

# 縦磁界印加同軸線路形マイクロ波プラズマCVD装置 の開発と成膜機構の研究

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# 目 次

|             | Page |
|-------------|------|
| I はしがき      | 1    |
| II 研究発表     | 2    |
| 1 学会誌、国際会議等 | 2    |
| 2 口頭発表      | 3    |
| III 研究成果    | 6    |
| 1 研究の背景     | 6    |
| 2 研究目的      | 9    |
| 3 研究成果概要    | 9    |
| IV 添付論文     | 12   |

## 1. はしがき

本研究は同軸線路形マイクロ波放電管に放電管軸方向（マイクロ波電界方向）と平行に直流磁界を印加して、プラズマの横方向への拡散を抑えることにより、電離電圧が高く放電しにくいガス、あるいは放電しにくいような低ガス圧において、プラズマCVD用の安定な高密度プラズマを作ることにある。ここで、膜堆積を行う堆積室内には直流磁界が漏れないようにして、等方的プラズマを作ること、またマイクロ波電力も漏れないようにして、静かな空間的アフターブロープラズマを作る必要がある。

本報告書は以上を目的として、平成7年－8年度の2年間にわたり行われた、装置の開発研究において得られた成果をまとめたものである。

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平成7年度                      1, 0 0 0    千円

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### Ⅲ 研究成果

#### 1 研究の背景

太陽電池はクリーンなエネルギー源として話題に上ってから久しいが、未だに十分な実用化段階に至っていない。その最大のネックは、低価格で大面積の良質な水素化アモルファスシリコン ( $a-Si:H$ ) 膜の作製技術が確立していないことにある。その作製法の主流は高周波 (RF) 放電を用いた化学気相堆積であるが、近年ではマイクロ波放電を用いる方法が多くなり、マイクロ波プラズマ CVD 法の研究が盛んに行われている。私は以前より二重管式同軸線路形マイクロ波プラズマ CVD 装置を開発し [1]、マイクロ波プラズマを用いた  $a-Si:H$  膜や窒化シリコン ( $SiN$ ) 膜の作製研究を行ってきた。これは、電子レンジの普及に伴いマイクロ波発振器が低価格となることを見越すと共に、空間的均一性のよい、高電子温度、高電子密度のプラズマを容易に得られること、そして無電極放電であるため純粋なプラズマが得られることを着目したことによる [2][3]。

また、本マイクロ波プラズマ CVD 方式の特徴は、マイクロ波の波長が短いことを生かして、キャビティー構造を用いて、マイクロ波電力を所定の空間に閉じ込めることによりマイクロ波電力の注入されている放電プラズマを所定の空間内にのみ発生できることにある。この装置により初めて、

$a-Si:H$  膜を放電プラズマの外で作製できるようになった [1][4]。

すなわち、放電プラズマに接続された膜堆積室にはプラズマの拡散と流れによって空間的な分離によって作られた、エネルギー注入のないプラズマ (空間的アフターグロープラズマ) が作られている。この空間的アフターグロープラズマ内で成膜することにより、プラズマ照射による基板あるいは膜表面加熱、そして膜への損傷を防ぐことが可能となった。ここではプラズマによる基板加熱がないので、高分子材料 (いわゆるプラスチック) のような低融



点物質上にも a-Si:H 膜が作製可能であることを示した[5]。

また、以前に行われた重点領域研究「反応性プラズマの制御」の研究計画「マイクロ波プラズマの発生法とその構造の制御」において、マイクロ波プラズマパラメータの空間分布を克明に測定し、これに基づき、プラズマの発生機構、およびプラズマの閉じ込め機構について明らかにしてきた[6][7]。さらに薄膜を作製する際に用いられる、膜堆積を行う所の反応性プラズマ (Ar/SiH<sub>4</sub> プラズマおよび N<sub>2</sub>/SiH<sub>4</sub> プラズマ) 中でのプローブ測定法を世界に先駆け、新たに考案し、この測定を可能とならしめ、膜を堆積している時の反応性プラズマパラメータ (電子温度、電子密度、プラズマ空間電位 等) の空間分布を始めて測定した[7][8][9]。さらに、基板に印加した DC バイアス電圧によるイオン衝撃エネルギーの制御性を明らかにした。すなわち、基板に流入するイオン流の単位面積、単位時間当たりの密度 (イオンフラックス密度) を一定としたとき、イオン衝撃エネルギーはイオンの加速電圧となり、基板上のプラズマのシース電圧となるわけであるが、これを始めて測定し、基板面積をパラメータとして、印加した DC バイアス電圧とシース電圧との関係を明らかにしたものである[10][11]。このような制御されたプラズマを用いて薄膜の作製研究を行い、ラジカルを低速で基板に軟着陸させることにより、低温で高品質な薄膜を作製できることを示してきた[12][13]。以上のような研究成果が本研究の背景となるものである。

これまでの私の研究は無磁界であることを特徴の一つとしてきた。他方、有磁界型のプラズマ CVD においてはマイクロ波電界と直流磁界を直交させることにより、電子サイクロトロン共鳴 (ECR) 効果を用い、高エネルギー電子を作り、SiH<sub>4</sub> を解離させることを目的としてきた。しかしながら、ECR 法ではプラズマが空間的に不均一であること、共鳴を用いるのでプラズマの安定性が悪いこと、かつ低ガス圧のみでしか ECR 効果が得られないこと、そして磁力線が基板位置までのびるので基板前で異方性プラズマとなるので、成膜に適さないこと、等の欠点を持つことが分かってきた。これら

の点をふまえて、新たなプラズマ作製法として本研究を立案した。

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## 2 研究目的

本研究目的は、直流磁界を用いて空間的に均一なプラズマを、種々のガス（放電し易いガスから放電しにくいガス）において、高いガス圧から低いガス圧にわたって安定に発生できる、プラズマCVD用の新しいプラズマ発生装置を開発することにある。その設計方針は、マイクロ波電力と直流磁界を所定の空間に閉じ込めて、その空間からプラズマと活性種を膜堆積室内に流入させマイクロ波電力のない、低温で静かな空間的アフターグロープラズマ内で、かつ磁力線の影響のない等方的プラズマ内で、成膜を可能とすることにある。これにより、より高品質なシリコン系薄膜（a-Si:HおよびSiN膜等）を作製することを目的とする。

## 3 研究成果概要

平成7年度には比較的放電しやすいArガスとN<sub>2</sub>ガスを用い、主として放電実験を行い、従来無磁界では放電が不安定となり、電子密度が低下してしまうような、低ガス圧でも安定で、かつ高電子密度のプラズマが得られることを明らかにした。さらに、比較的放電しにくいH<sub>2</sub>ガスにおいても同様の実験を行い、H<sub>2</sub>ガスにおいても安定で、かつ高電子密度のプラズマが得られるという見込みを得て、目的の前半を達成した。

平成8年度には、主として膜堆積に注目して実験を行い、Arガス、N<sub>2</sub>ガスを用いた場合には無磁界の場合と比較して、膜質を劣化させることなく、より高速な膜堆積の行えることを明らかにした。さらに、H<sub>2</sub>ガスの場合には、無磁界では電子密度が低いため、a-Si:H膜の堆積速度はかなり遅いものであったが、約1400ガウスの磁界印加により、安定でかつ高電子密度のプラズマが得られることを示し、7 Å/sという高速の膜堆積が行える

ことを明らかにし、目的の後半を達成した。

その詳細はその添付論文に記載されているが、無磁界時と有磁界時とを比較して、添付論文に従って、以下にその概要をまとめる。

〔1〕無磁界時における放電の安定性をArガスとN<sub>2</sub>ガスにおいて調べた。ここで、ArガスとN<sub>2</sub>ガスは本研究でいうところの放電し易いガスに相当する。さらに、安定な放電時における電子温度電子密度及びプラズマの空間電位等のプラズマパラメータを測定し、プラズマの均一性について検討し、CVD用のプラズマとして十分に均一なプラズマが得られることを明らかにした。またイオン衝撃効果について検討を加え、イオン衝撃効果の内、堆積中の膜表面加熱効果が、基板加熱効果と同様の膜質改善効果を持つことを明らかにした。しかしながら、イオン衝撃効果の内のイオン打ち込み効果により、膜質は総合的に悪くなることを明らかにした。添付論文〔15〕〔16〕〔17〕参照。

〔2〕イオン衝撃エネルギーは膜表面に流入するイオンフラックス密度を一定にしたとき、膜表面のシース電圧に比例する。そこで、基板に印加するDCバイアスを変えシース電圧を測定し、イオン衝撃エネルギーが膜質に与える効果を明らかにすると共に、基板をアースして、二重管の内管にDCバイアスを印加しても、ほぼ同時の効果の得られることを明らかにした。添付論文〔9〕〔13〕〔14〕参照。

〔3〕Arガス放電における直流磁界印加効果をプラズマパラメータの測定に基づき詳細に検討した。その結果、径方向、周方向に関するプラズマの均一性の良いこと、印加磁界強度によってはECR効果も表れるが、その効果は弱く、軸方向磁界は径方向へのプラズマの拡散を抑えプラズマを安定させる効果が強いことを明らかにした。添付論文〔11〕〔12〕参照。

〔４〕光ファイバーをセンサーとする極薄膜の高感度測定を開発して、極薄膜のエネルギーギャップ  $E_0$  を測定した。さらに、このセンサーにより成膜後の空気リーク時における膜質の変化を測定できることを明らかにした。また、膜成長時の膜質を測定し、成膜機構を検討しうる可能性を明らかにした。添付論文〔１〕〔２〕〔６〕〔１０〕参照。

〔５〕ＲＦバイアスを印加して、 $\text{SiN}$ 膜を作製し、 $\text{a-Si:H}$ 膜作製時におけるＤＣバイアス印加効果と同時の効果が得られることを明らかにした。添付論文〔７〕〔８〕参照。

〔６〕イオン衝撃効果には、成長中の膜表面加熱効果と、成長中に膜中にイオンを打ち込み膜組成を変えるようなイオン打ち込み効果があることを明らかにすると共にその分離に成功した。添付論文〔５〕参照。

〔７〕直流磁界を印加した場合の $\text{N}_2$ プラズマについて詳細に測定した。また直流磁界印加により、 $\text{SiN}$ 膜の膜質を劣化させることなく、無磁界時より、より高速な膜堆積を行うことができることを明らかにした。添付論文〔３〕〔４〕参照。

〔８〕 $\text{H}_2$ ガス放電においては無磁界時に十分密度の高いプラズマが作製できず、 $\text{a-Si:H}$ の堆積速度は遅いものであったが、軸方向磁界印加により、プラズマの径方向への拡散が抑えられ、ＣＶＤに必要な十分高密度なプラズマが得られることを明らかにした。その結果、 $\text{H}_2$ プラズマを用いて、 $7 \text{ \AA/s}$ という高速堆積ができることを明らかにした。

#### IV 添付論文

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# In situ measurement of the optical constant of ultra thin films using optical fiber sensor.

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## ABSTRACT

We use an optical fiber sensor whose part of clad is removed for the optical constant of ultra thin film measurement. The sensitivity of the sensor is increased by decreasing the diameter of the optical fiber and / or increasing the length of the film deposited part. The result of the *in situ* measurement method of change of a-Si:H ultra thin films by oxidation with passage of time by leaking from vacuum to atmospheric air is shown. We use an optical fiber sensor whose length of the film deposited part is 100 mm, diameter of the core is 110  $\mu\text{m}$  and the core material is silica. a-Si:H film with approximately 10 nm in thickness is deposited on the core of the optical fiber sensor. The oxidation saturates in approximately 600 s. The larger attenuation of transmitted light at the long wavelengths from 685 to 800 nm is observed. This phenomenon is maybe due to the change of defects by relaxation

Keywords; Fiber Sensor, Waveguide Sensor, In Situ Measurement, Oxidation, Ultra Thin Film, a-Si:H

## 1. INTRODUCTION

We have studied a method to measure the dependence of the light transmittance on the plasma chemical vapor deposition (CVD) film thickness for the measurement of the optical constants of thin films<sup>1,2,3</sup>. The films are deposited on an optical fiber whose part of the clad is removed or on a slab optical waveguide as a sensor. During the deposition of films in the plasma CVD system, the transmitted light which goes through the sensor decreases exponentially with periodic oscillation corresponding to the increase of film thickness. The reason is that the electric field strength concentrates periodically in the film. By removing the oscillation mathematically, we determined the optical energy gap<sup>1</sup>. Then, we also determined the refractive index from the value of the first valley in the oscillation or the period of the oscillation<sup>2,3</sup>. In our new method, we have been able to measure the optical energy gap of the ultra thin a-Si:H film with approximately 20 nm in thickness which is about 1/40 comparing with what in the conventional method and the refractive index of the ultra thin film with approximately 10 nm in thickness<sup>1,2</sup>. A film thickness of approximately 1  $\mu\text{m}$  was need to obtain sufficient interaction between a film and light in the conventional method[4]. As compared with this, the measurement of the ultra thin films mentioned above is possible in our method because the length of interaction takes long sufficiently toward the propagation direction of light. The same thing is able to correspond in the measurement using the optical fiber whose part of clad is removed as a sensor. By increasing the sensitivity of these optical waveguided type sensors, the change of many physical quantities which have not been measured before could be measured *in situ*.

On the other hand in thin film fabrication, the change of the films just after a leak by atmospheric air was not measured when fabrications were finished. The measurement of the surface oxidation layer of thin films was usually obtained by executing the etching of the surface and measurement of the X-ray photoelectron spectroscopy alternatively after leaking by atmospheric air and putting the films out of a fabrication chamber. Therefore, the film surface oxidation progress measurement of change in elapsed time after the leak from vacuum to atmospheric air is not completed.

In this report, using the high sensitivity optical fiber sensor obtained from results of investigation by increasing the sensitivity of the optical fiber sensor, we show an *in situ* measurement method of change of a film quality with passage of time just after leaking a-Si:H ultra thin films to atmospheric air.



## 2. INVESTIGATION OF HIGH SENSITIVITY OF THE OPTICAL WAVEGUIDE SENSOR IN SIMULATION

Conditions of increasing the sensitivity of the optical waveguide sensor are clarified in the four-layer slab waveguide simulation. The four-layer slab waveguide consists of air, film, waveguide and air. The length of the part on which the film is deposited is  $l$  [mm], and the thickness of the optical waveguide is  $t$  [ $\mu\text{m}$ ]. Transmittance dependence on deposited film thickness of the four-layer slab waveguide is obtained from solutions of an eigenvalue equation<sup>4</sup>. A wavelength  $\lambda$  is 632.8 nm, the refractive index of air  $n_0$  is  $1 - j0$ , the refractive index of deposited a film  $n_f$  is  $2.88 - j0.029$  and the refractive index of an optical waveguide  $n_w$  is  $1.457 - j0$ . The value of  $n_f$  is a typical value of a-Si:H, and the value of  $n_w$  is that of fused silica. The waveguided mode is the TE mode, and the mode number is 100.

Figure 1 and 2 show the calculation results using the values mentioned above.

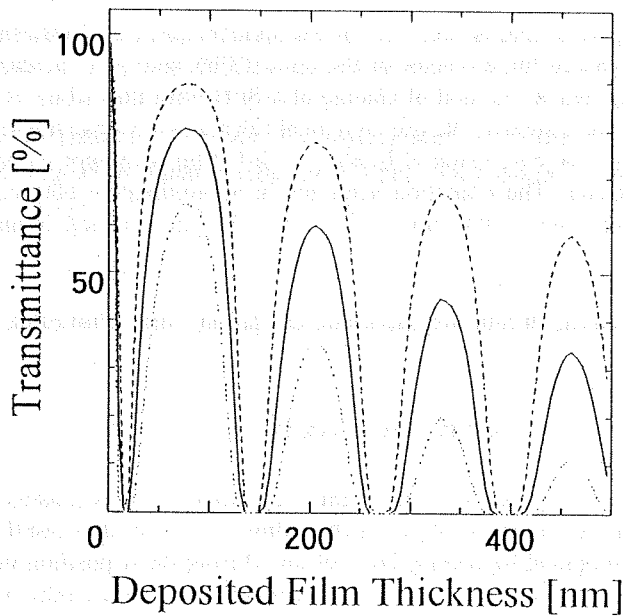


Fig. 1. Transmittance dependence on deposited film thickness at  $l = 50, 100$  and  $200$  mm when  $t = 100$   $\mu\text{m}$ .

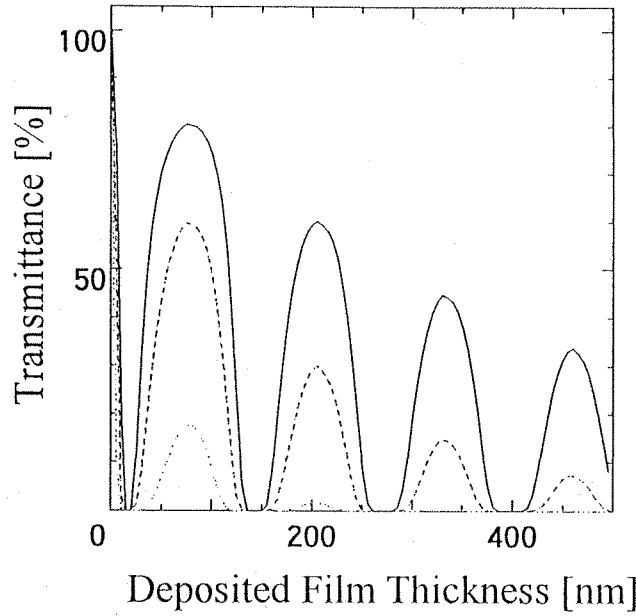


Fig. 2. Transmittance dependence on deposited film thickness at  $t = 100, 150$  and  $200 \mu\text{m}$  when  $l = 100 \text{ mm}$ .

Figure 1 shows the results at  $l = 50, 100$  and  $200 \text{ mm}$  when  $t = 100 \mu\text{m}$ , and Fig. 2. shows the results at  $t = 100, 150$  and  $200 \mu\text{m}$  when  $l = 100 \text{ mm}$ . It is clarified that transmittance has periodic oscillation. The reason of the oscillation is that the electric field concentrates periodically in the film layer which has large absorption coefficient<sup>1</sup>. It is clarified that transmittance decreases when the value of  $l$  increases from Fig. 1. Also, it is clarified that transmittance decreases when the value of  $t$  decreases from Fig. 2. Absorption increases when  $l$  increases. Ratio of light without interaction with a deposited film and the whole waveguided light decreases when  $t$  decreases. From these phenomena, the equivalent absorption coefficient of the entire four-layer slab waveguide increases. Consequently, even if the absorption coefficient of the deposited film is small the sufficient absorption for measuring can be obtained and the sensitivity of the sensor increases. The same conclusion is derived for the another mode numbers, another wavelengths and the TM mode. The same tendency was confirmed in experiments<sup>1</sup>. Therefore, to increase the sensitivity of the slab waveguide sensor, we need increase  $l$  and / or decrease  $t$ . However, the waveguided light is absorbed too much when  $l$  increases or  $t$  decreases too much. Therefore, the upper limit of  $l$  and the lower limit of  $t$  exist depending on the absorption coefficient of deposited films, the sensitivity of a detector and the proceedings of the noise reduction.

### 3. INVESTIGATION OF HIGH SENSITIVITY OF OPTICAL FIBER SENSOR IN EXPERIMENT

Conditions of increasing the sensitivity of the optical waveguide sensor are clarified in experiment. The optical fiber sensor and its setup in fabrication chamber are shown.

Fig. 3. Details of the optical fiber sensor.

Figure 3 shows the optical fiber sensor structure. This is a step index type optical fiber with silica core and polymer clad. The clad is removed for deposition of a-Si:H films. The length of the clad removed part is  $l$  [mm] and its diameter of the core is  $\phi$  [ $\mu\text{m}$ ].

Our experimental setup - the double-tubed coaxial-line-type microwave plasma CVD system is shown in Fig. 4<sup>5</sup>. As shown in Fig. 4, a-Si:H is fabricated from  $\text{SiH}_4$  by using Ar plasma flowing from the bottom side of the system.

Fig. 4. Experimental setup, with our optical fiber sensor.

The optical fiber sensor is set on the substrate table in this chamber. The input port of the optical fiber is connected with a halogen lamp

light source and the output port is connected with a spectrum analyzer.

Fig. 5. Transmittance dependence on deposited a-Si:H film thickness at  $\lambda = 650$  nm using the optical fiber sensors.

Figure 5 shows transmittance dependence on deposited a-Si:H film thickness at  $\lambda = 650$  nm using the optical fiber sensors. By comparing the data of the  $l = 50$  mm and  $\phi = 110$   $\mu$ m sensor with the data of the  $l = 100$  mm and  $\phi = 110$   $\mu$ m sensor, it is clarified that transmittance decreases when  $l$  is large in Fig. 5. Also, by comparing the data of the  $l = 100$  mm and  $\phi = 200$   $\mu$ m sensor with the data of the  $l = 100$  mm and  $\phi = 110$   $\mu$ m sensor, it is clarified that transmittance decreases when  $\phi$  is small. The values of the film thickness where the peaks of the periodic oscillations of transmittance appear are different among the sensors because we consider that the refractive indexes of the deposited film are different as depositions are not at same time. Especially, the different film thickness of the peaks between the sensors of  $\phi = 110$   $\mu$ m and  $200$   $\mu$ m course that the refractive indexes of core are different as the makers of the fibers are different, we consider. The same conclusion was derived for 400 through 800 nm in wavelength in our measurement.

Increasing  $l$  corresponds to increasing  $l$  of the optical waveguide sensor. It is considered that decreasing  $\phi$  corresponds to decreasing  $t$  of the optical waveguide sensor. Therefore, it is clarified that to increase the sensitivity of the optical fiber sensor, we need increase  $l$  and / or decrease  $\phi$ .

#### 4. CHANGE OF LIGHT TRANSMITTANCE AFTER LEAK

Transmitted light is measured in about 10 minutes after the fabrication. Using the optical fiber sensor, whose length of the film deposited part  $l$  is 100 mm and diameter of the core  $\phi$  is 110  $\mu$ m, a-Si:H film with approximately 10 nm in thickness is fabricated on the optical fiber sensor. The film change by oxidation is measured *in situ*. The period to take the leak of the CVD chamber from vacuum to atmospheric air is approximately 20 s.

Fig. 6. Transmittance spectra in experiment using the optical fiber sensor.

Figure 6 shows transmitted light spectra. In Fig. 6, the upper data is the spectrum of the sensor without the film. The middle data is the spectrum after depositing a-Si:H of approximately 10 nm in thickness and letting it stand in approximately 30 minutes in vacuum, namely, the spectrum before the leak. The lower data is the spectrum at 680 s after leaking the chamber. The attenuation between the upper spectrum and the middle spectrum means the absorption by a-Si:H, the interference and the scattering of transmitted light. The attenuation between the middle spectrum and the lower spectrum means the change of transmittance by the leak.

Fig. 7. Transmittance change with passage of time.

Figure 7 shows the change of light transmittance through the optical fiber sensor with passage of time at wavelengths of 800, 750, 700 and 685 nm. From Fig. 7, it is clarified that the transmittance at every wavelength decreases after leaking the CVD system and it saturates in approximately 600 s.

It is considered that the film is changed by oxidation and the oxidation saturates around 600 s from Fig. 7. By comparing the rate of the change of transmittance among the wavelengths, it is clarified that the large rate of the change occurs at long wavelengths. It was reported that defects are changed by relaxation by the bias light in the region of  $0.8 \text{ eV} < h\nu < 1.8 \text{ eV}$  ( $\lambda = 690 \text{ nm} \sim 1.55 \text{ } \mu\text{m}$ ) for a-Si:H because of the shift of the quasi-Fermi-level to the conduction band or an increase in the concentration of dangling-bond centers  $D^-$ <sup>6,7</sup>. The result in this experiment in Fig. 6 shows the similar tendency to the dependence of the absorption coefficient on energy owing to the change of defects described in above references. We consider that the similar phenomena occur by oxidation in the high energy side of the Urbach tail region ( $1.5 \text{ eV} < h\nu < 1.8 \text{ eV}$  corresponding to  $690 \text{ nm} < \lambda < 800 \text{ nm}$ ).

#### 5. CONCLUSIONS

Using the optical waveguide as a sensor, it was shown that the sensitivity increases by increasing  $l$  and / or decreasing  $t$  in

the four-layer slab optical waveguide simulation. Using the optical fiber as a sensor, we found the experimental results consisted with the above theoretical analysis of the slab optical waveguide. The *in situ* measurement of the physics quantity which has not measured before was shown with the high sensitive sensor. Concretely, the *in situ* measurement of the change of the film quality due to the oxidation can be completed with the high sensitive optical fiber sensor.

## **6. ACKNOWLEDGMENT**

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# Refractive Index Measurement of Silicon Thin Films Using Slab Optical Waveguides

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Measurement of the real part of the refractive index ( $n'_f$ ) of silicon thin films using a slab optical waveguide (SOW) is discussed. Upon deposition of thin films on a SOW, the transmittance decreases with periodic oscillation owing to the multiple reflection. It is clarified from a simulation of a four-layer SOW that the period of oscillation is reduced when  $n'_f$  increases. In this paper, we discuss a method of determining the  $n'_f$  from correspondence of the minimum film thickness ( $d_0$ ) in which the oscillation valley appears as a calculation result of transmittance for the TE<sub>0</sub> mode to  $d_0$  in an experiment in which the refractive index and sizes of SOW are known without considering higher modes or the TM mode. Good agreement is observed in comparison of the result of the measurement with that of the ellipsometer at a wavelength of 632.8 nm. Therefore, it can be shown that the distributions of  $n'_f$  of a-Si:H and SiN thin films at wavelengths from 400 to 800 nm are obtained in the same manner. In order to achieve higher accuracy of the measurement, a SOW with a larger refractive index is used.

KEYWORDS: optical fiber sensor, refractive index, slab optical waveguide, a-Si:H, SiN, thin film, MPCVD

## 1. Introduction

Sensors which use optical fibers such as temperature sensors,<sup>1)</sup> pressure sensors<sup>2)</sup> and gas sensors,<sup>3)</sup> have been actively developed, and optical functional devices by which a metal or semiconductor film is fabricated on an optical waveguide have been studied.<sup>4-7)</sup> The phenomenon in which the combinations of light with a film on a waveguide differ between the TE and TM modes according to the fabricated film thickness is applied to the realized waveguide type TE/TM mode filters. The extinction ratio of the transmitted light of the TE and TM modes is 34 dB for metal film fabrication.<sup>5)</sup> The extinction ratio with hydrogenated amorphous silicon (a-Si:H) is 30 dB.<sup>6)</sup> The extinction ratio with silicon nitride (SiN) is 27 dB.<sup>7)</sup> An optical energy gap ( $E_g$ ) measurement of a-Si:H with approximately 20 nm has been performed with the dependence of transmittance on the deposited film thickness by depositing semiconductor films on a slab optical waveguide (SOW) used as a sensor.<sup>8)</sup> In this study, it was clarified that the transmittance decreases with periodic oscillation. We propose a new measurement method for the real part of the refractive index ( $n'_f$ ) of silicon thin films such as a-Si:H and SiN on SOW from the minimum film thickness ( $d_0$ ) at which the valley of the oscillation appears. The refractive index of thin films can be measured using interference fringes by perpendicularly irradiating light onto a film or by using ellipsometry. In the method using interference fringes, the refractive index is obtained from the interval of the fringes appearing in the dependence of transmittance on the wavelength.<sup>9)</sup> In the ellipsometry method, the refractive index is obtained from the reflection coefficients and the relative phases of the *p* and *s* waves.<sup>10)</sup> A film thickness of approximately 1 μm is needed to obtain sufficiently narrow interval fringes for the method using the interference fringes. On the other hand, in our method, the refractive index can be determined below 20 nm in thickness. Furthermore, this method is not influenced by the atmosphere because films are deposited on a SOW sensor which is in a fabrication chamber. While light is absorbed and scattered in plasma for the ellipsometry

method because light goes through plasma, there is an advantage in this method in that absorption by plasma does not exist using light which goes through the SOW.

In this report, it is shown by a simulation of a four-layer SOW that the value of the film thickness at a peak in the dependence of the effective absorption coefficient ( $\alpha_m$ ) for the mode number *m* on the film thickness (*d*) is changed by  $n'_f$ . The peaks match the valleys appearing in the dependence of transmittance on *d*. A method to obtain  $n'_f$  from the correspondence of  $d_0$  of a calculated result to  $d_0$  of an experimental result, by changing  $n'_f$  in the simulation for the TE<sub>0</sub> mode is shown. Distributions of  $n'_f$  from 400 to 800 nm in wavelength for three films with different  $n'_f$  are shown.

## 2. Dependence of $\alpha_m$ on *d* in the Four-layer SOW Simulation

Figure 1 shows the structure of the four-layer SOW. The SOW consists of air, film, optical waveguide and air. The thickness of the deposited film is defined as *d* nm, the length of the part on which the film is deposited is defined as *l* mm, and the thickness of the SOW is defined as *t* μm. The refractive index of air  $n_0$  is  $1 - j0$ , the refractive index of film  $n_f$  is  $n'_f - jn''_f$ , and the refractive index of optical waveguide  $n_w$  is  $n'_w - jn''_w$ . The guided light is in the direction of *z*. The effective refractive index of the four-layer SOW  $N_m$  which is  $N'_m - jN''_m$  and the profile of the electric field distribution for the guided mode of the mode number *m* are obtained from solutions of an

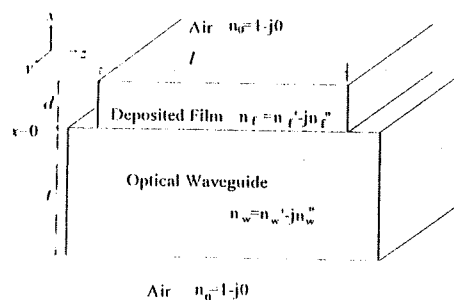


Fig. 1. Structure of the four-layer SOW.

eigenvalue equation for a transversely guided mode.<sup>11)</sup>

We obtain the dependence of  $\alpha_m$  on  $d$  in the four-layer SOW at a wavelength of 632.8 nm.  $N'_m$  and  $N''_m$  are obtained by the four-layer SOW simulation.  $\alpha_m$  is obtained with  $N''_m$  using

$$\alpha_m = 4\pi/\lambda \cdot N''_m, \quad (1)$$

where  $\lambda$  is the wavelength.

The material of the SOW is fused silica and that of the films is  $\alpha$ -Si:H in the simulation. The constant values used in the simulation are as follows.  $n_f$  is 4.0 - j0.1 at 632.8 nm. The value of  $n'_f$  is almost the highest one measured by the conventional ellipsometer for  $\alpha$ -Si:H films with a thickness of 1  $\mu$ m which are fabricated by a double-tubed coaxial-line type microwave plasma chemical vapor deposition (MPCVD) system.<sup>7)</sup> The value of  $n''_f$  is almost the highest one calculated with the absorption coefficient obtained from the ultraviolet-visible spectroscopy spectrum for the same  $\alpha$ -Si:H films. The value of  $n'_w$  is 1.457 at 632.8 nm when the material is fused silica, and  $n''_w$  is null because  $l$  is short enough.  $l$  is 100  $\mu$ m. The maximum mode number of the four-layer SOW is 335 for both the TE mode and the TM mode with the values set in this section.

### 2.1 Dependence of $\alpha_m$ on $d$ for the TE<sub>0</sub> mode and the TM<sub>0</sub> mode

Figure 2 shows the dependences of  $\alpha_m$  on  $d$  for the TE<sub>0</sub> and TM<sub>0</sub> modes. It is clarified that  $\alpha_m$  has periodic peaks in both the TE<sub>0</sub> mode and the TM<sub>0</sub> mode. The field strength is enlarged when the number of antinodes of the field increases one by one at each constant film thickness from the calculation of the field distribution. At this moment,  $\alpha_m$  exhibits a peak because the field distribution concentrates in the film.<sup>8)</sup>

### 2.2 Dependence of $\alpha_m$ on $d$ with $n'_f$

For the TE<sub>0</sub> mode, Fig. 3 shows the dependence of  $\alpha_m$  on  $d$  with  $n'_f = 2.0, 3.0$  and 4.0. It is clarified that the period of the  $\alpha_m$  peaks increases when  $n'_f$  becomes small. Figure 4 shows the profile of the field distribution around the film at  $d = 300$  nm with  $n'_f = 2.0, 3.0$  and 4.0 for the TE<sub>300</sub> mode. The wave vector  $k_i$  in a material with the

real part of the refractive index  $n'_i$  is expressed as

$$|k_i| = 2\pi/\lambda \cdot n'_i. \quad (2)$$

Because  $n'_f > n'_w$ , the wave vector component ( $k_{fx}$ ) in the direction of  $x$  in the film is smaller than that ( $k_{wx}$ ) in the SOW. From Fig. 4, it is clarified that the period of the amplitude of the field distribution decreases at the same value of  $d$ .  $\alpha_m$  reaches peaks with increasing  $d$  when the number of antinodes in the film increases. Therefore, when the period of the field amplitude decreases, namely, when  $n'_f$  enlarges, the period of  $\alpha_m$  peaks becomes smaller. The same conclusion is derived for the TM mode qualitatively.

As mentioned above, by depositing a silicon film on a SOW whose refractive index and sizes are known,  $n'_f$  is measured from the thickness in which the peaks of  $\alpha_m$  are obtained, or, in which the valleys of transmittance are obtained in the dependence on  $d$ .

### 2.3 Dependence of $\alpha_m$ on $d$ for the mode number $m$

Figure 5 shows the dependence of  $\alpha_m$  on  $d$  when the mode numbers  $m$  of the TE mode are 0, 10 and 100. It is clarified that the values of  $d$  with which  $\alpha_m$  peaks are almost the same even if  $m$  changes. Furthermore,

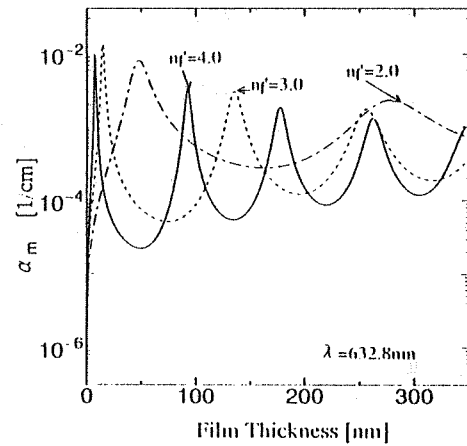


Fig. 3. Dependence of  $\alpha_m$  on  $d$  for the TE<sub>0</sub> mode at  $n'_f = 2.0, 3.0$  and 4.0.

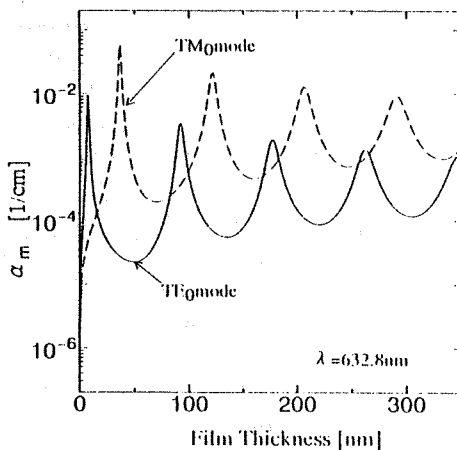


Fig. 2. Dependence of  $\alpha_m$  on  $d$  for the TE<sub>0</sub> and TM<sub>0</sub> modes.

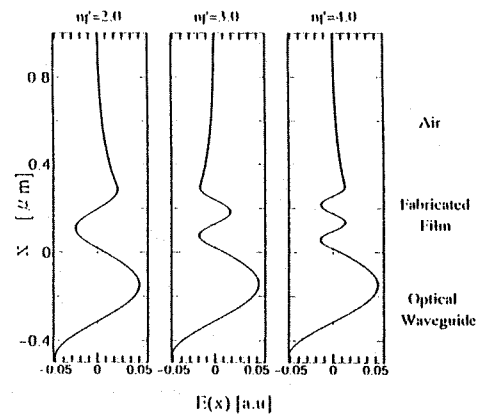


Fig. 4. Field strength distributions for the TE<sub>300</sub> mode at  $n'_f = 2.0, 3.0$  and 4.0 around a film of 300 nm in thickness and  $\lambda = 632.8$  nm.

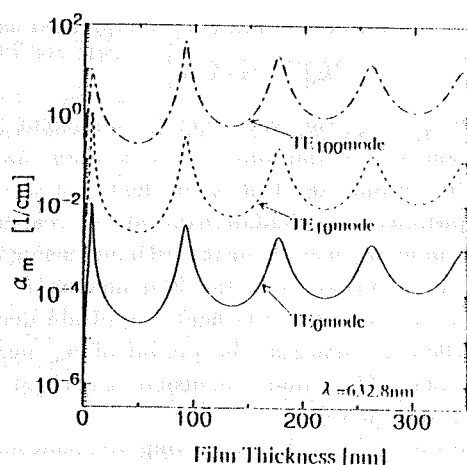


Fig. 5. Dependences of  $\alpha_m$  on  $d$  for the  $TE_0$ ,  $TE_{10}$  and  $TE_{100}$  modes.

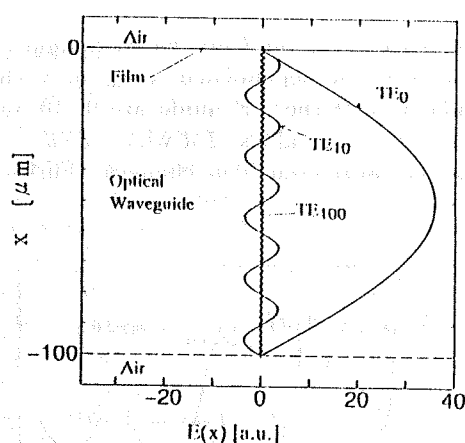


Fig. 6. Field strength distributions for the  $TE_0$ ,  $TE_{10}$  and  $TE_{100}$  modes at  $\lambda = 632.8$  nm.

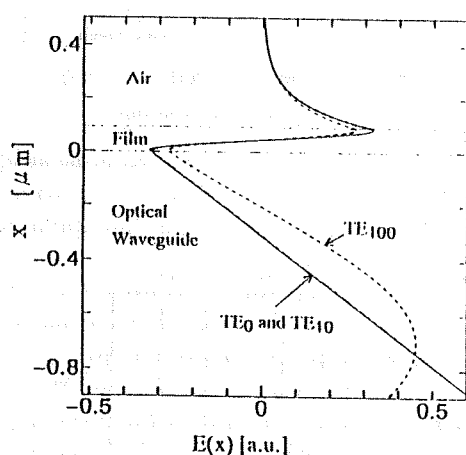


Fig. 7. Field strength distributions for the  $TE_0$ ,  $TE_{10}$  and  $TE_{100}$  modes around a film of 92 nm in thickness and  $\lambda = 632.8$  nm.

the value of  $\alpha_m$  increases for higher  $m$ .  $\alpha_m$  reaches a second peak at  $d = 92$  nm. In this case, Fig. 6 shows the profiles of the field distribution at  $m$  of 0, 10 and 100 for the TE mode. The profiles of the field distribution around the film are shown in Fig. 7, since the film is very thin compared with the SOW. From Fig. 6, it

is clarified that the maximum relative field strength in the SOW is smaller at the higher value of  $m$ . The maximum field strength is 35.85 in the  $TE_0$  mode, 3.587 in the  $TE_{10}$  mode and 0.4584 in the  $TE_{100}$  mode. It is clarified that the energy distribution in the SOW becomes smaller at a higher value of  $m$ . On the other hand, it is clarified that the field distributions are almost the same in the film even if  $m$  is high in Fig. 7. Therefore, the ratio of absorption increases for higher  $m$ .  $\alpha_m$  increases when the field distribution is smaller in the SOW and is almost the same in the film, because  $\alpha_m$  means the equivalent absorption coefficient for the entire four-layer SOW. The same conclusion is derived for the TM mode qualitatively.

#### 2.4. $d$ at which the first peak of $\alpha_m$ is obtained

For the case when  $n'_t$  is 2.0, 3.0 and 4.0 and  $n''_t$  is 0.01, 0.05 and 0.1, the film thicknesses ( $d_0$ ) at which the first peak appearing in the dependence of  $\alpha_m$  on  $d$  is obtained are shown in Table I for the TE mode of the mode number 0 and the maximum mode number of the potential guided light. The ranges of  $n'_t$  and  $n''_t$  cover that of the silicon thin films fabricated using our MPCVD.  $d_0$  becomes smaller when  $n'_t$  enlarges, from Table I. Furthermore,  $d_0$  hardly changes even if  $n''_t$  enlarges at  $n'_t = 3.0$  and 4.0. However, when  $n''_t$  is 0.1, compared with  $n''_t = 0.01$  and 0.05 at  $n'_t = 2.0$ ,  $d_0$  becomes smaller by approximately 0.5 nm. This means that the value of  $n'_t$  must be considered for the film whose  $n'_t$  is small enough and  $n''_t$  is approximately 0.1. Next, the difference of  $d_0$  becomes appreciable as determined by comparison of the mode number of 335 with that of 0. Therefore, consideration for the higher mode number is also needed.

Table II shows the same calculation as Table I for the TM mode. The same conclusions are derived for the TM mode as for the TE mode.  $d_0$  cannot be recognized at  $n'_t = 2.0$  and  $m = 335$  because the dependence of  $\alpha_m$  on  $d$  becomes broad and the peaks disappear. The Brewster angle exists at the bound between the SOW and the film since the TM mode is the light of the  $p$  polarization. Reflection at the bound is less when the incident angle of light approaches the Brewster angle. In this case, the peaks of the dependence of  $\alpha_m$  on  $d$  cannot be recognized. This result is agreed for the whole TM mode. In the same way, because the reflection at the bound between the SOW and the film is less when the value of the real part of the refractive index of SOW and that of the film become the same, such as  $n'_t = 2.0$ , many modes in which the peaks of the dependence of  $\alpha_m$  on  $d$

Table I.  $d_0$  variation with  $n'_t$  and the  $TE_0$  mode at  $n''_w = 1.457$ ,  $t = 100$   $\mu$ m and  $\lambda = 632.8$  nm.

| $n'_t$<br>$n''_t$ | 2.0    |            | 3.0    |            | 4.0    |            |
|-------------------|--------|------------|--------|------------|--------|------------|
|                   | $TE_0$ | $TE_{335}$ | $TE_0$ | $TE_{335}$ | $TE_0$ | $TE_{335}$ |
| 0.01              | 48.5   | 42.0       | 14.8   | 14.2       | 7.5    | 7.4        |
| 0.05              | 48.3   | 41.9       | 14.8   | 14.2       | 7.5    | 7.4        |
| 0.1               | 48.0   | 41.7       | 14.7   | 14.2       | 7.5    | 7.4        |

Table II.  $d_0$  variation with  $n'_t$  and the  $\text{TM}_0$  mode at  $n''_w = 1.457$ ,  $t = 100 \mu\text{m}$  and  $\lambda = 632.8 \text{ nm}$ .

| $n'_t$<br>$n''_t$ | 2.0           |                   | 3.0           |                   | 4.0           |                   |
|-------------------|---------------|-------------------|---------------|-------------------|---------------|-------------------|
|                   | $\text{TE}_0$ | $\text{TE}_{335}$ | $\text{TE}_0$ | $\text{TE}_{335}$ | $\text{TE}_0$ | $\text{TE}_{335}$ |
| 0.01              | 92.6          | ---               | 50.1          | 75.3              | 36.7          | 52.6              |
| 0.05              | 92.4          | ---               | 50.1          | 75.4              | 36.7          | 52.6              |
| 0.1               | 91.7          | ---               | 50.1          | 75.4              | 36.7          | 52.6              |

cannot be recognized exist around the Brewster angle.

### 3. Measurement of $n'_t$

We consider the first valley appearing in the dependence of transmittance on  $d$ . The SOW is set as the sensor in the MPCVD chamber. A double-tubed coaxial-line type MPCVD system<sup>7)</sup> is used for fabrication on the SOW sensor. Figure 8 shows the detail of the sensor. The material of the SOW is fused silica (T-4040, Toshiba Ceramics).  $t$  is  $170 \mu\text{m}$  and  $l$  is  $15 \text{ mm}$ . The width of the part of the SOW on which the film is deposited,  $w$ , is  $18 \text{ mm}$ . A halogen lamp light is guided as input beams, and then output beam spectra are observed. Intensities of the spectrum from  $400$  to  $800 \text{ nm}$  are measured during the deposition. During one scan of measurement of the spectrum,  $d$  is regarded as constant because the spectrum is measured at  $0.5 \text{ s}$  per scan while the deposition rate of the films is very low at  $0.05 \text{ nm/s}$ . The changes in  $d$  are recorded using a crystal-oscillation-type thickness monitor, and then the thickness of the film on a Si substrate placed close to the SOW is measured using a needle-tactual-type thickness meter after the deposition. The change of  $d$  during the deposition is obtained by correcting the values of the crystal-oscillation-type thickness monitor with the value of the needle-tactual-type thickness meter. For further details, readers may refer to ref. 8.  $\alpha\text{-Si:H}$ ,  $\text{Si}_3\text{N}_4$  and silicon rich SiN which has optical characteristics intermediate between those of the former two materials are used as films. For details of the fabrications, readers may refer to refs. 7, 12, 13, 14, and 15. Sample #1 is the  $\alpha\text{-Si:H}$  film, #2 is the silicon rich SiN film and #3 is the  $\text{Si}_3\text{N}_4$  film. For comparison, the value of  $n'_t$  is obtained from measurement of the film on the Si substrate placed close to the sensor by the ellipsometer. Further,  $n''_t$  is obtained from the ultraviolet visible spectroscopy spectrum of the film on a fused silica substrate placed close to the sensor.

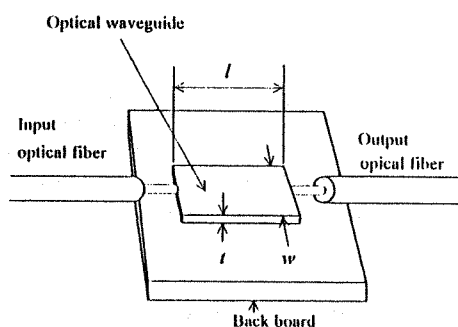


Fig. 8. Details of the SOW sensor.

We pointed out in §2.4 that the value of  $n''_t$  must be considered for a film whose  $n'_t$  is smaller such as approximately 2.0 and whose  $n''_t$  is larger such as approximately 0.1. For  $\text{Si}_3\text{N}_4$ , the absorption caused by the electron transition across the energy band does not exist in the visible light region (from  $400$  to  $800 \text{ nm}$ ) in which it is clarified that  $E_g$  is approximately  $5 \text{ eV}$ . Therefore, although the value of  $n'_t$  of  $\text{Si}_3\text{N}_4$  is approximately 2.0 through the visible light region,  $n''_t$  is regarded as 0. As clarified in Tables I and II, the value of  $n''_t$  does not influence the value of  $d_0$  in the region of our discussion, because the values of  $n'_t$  are from approximately 3 to 4 for the other two films. Therefore, for the three films discussed in this report,  $n''_t$  can be any value from 0.01 to 0.1. We take the value of 0.029 which is obtained from the ultraviolet-visible spectroscopy spectrum for Sample #2 at  $632.8 \text{ nm}$ .

#### 3.1 Dependence of transmittance on $d$

By the four-layer SOW simulation, the dependences of  $\alpha_m$  on  $d$  are obtained for all the mode numbers of the potential guided light. The dependence of the transmittance  $T_m$  on  $d$  for each mode is calculated using

$$T_m = \exp(-\alpha_m \cdot l). \quad (3)$$

This procedure is performed for the TE and TM modes.

The incident light is smaller for higher modes according to the Gaussian distribution because the incident light from the light source is the Gaussian beam. Therefore, the coefficient  $G_m$  which is weighted for the mode number  $m$  is given as

$$G_m = \exp(-C \cdot m^2/M^2), \quad (4)$$

where  $M$  is the mode number of the maximum of the potential guided light.  $C$  is a constant. The value of  $M$  obtained from calculation is 569 for both the TE mode and the TM mode for  $t = 170 \mu\text{m}$ .

The transmittance is defined as  $T_{\text{TE}}$  and  $T_{\text{TM}}$  to which the transmittance of the  $\text{TE}_m$  and  $\text{TM}_m$  modes are added as they are weighted for the mode number from 0 to  $M$  in

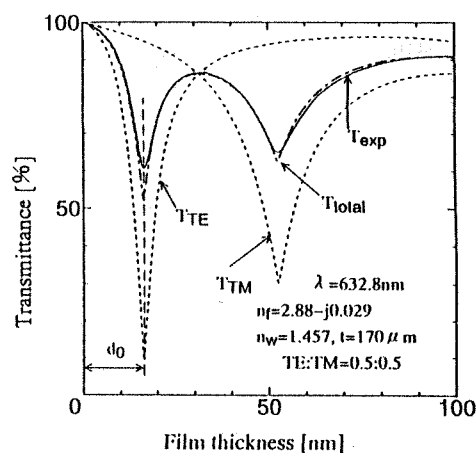


Fig. 9. Dependence of transmittance on  $d$ .  $T_{\text{exp}}$ : experimental values for sample #2;  $T_{\text{TE}}$  and  $T_{\text{TM}}$ : transmittance weighted by the mode number, by associating the mode number with the Gaussian distribution;  $T_{\text{total}}$ : total transmittance of  $T_{\text{TE}}$  and  $T_{\text{TM}}$  as 0.5:0.5.



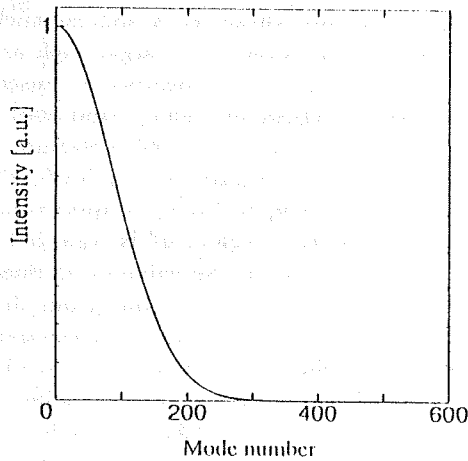


Fig. 10. Profile of the existence ratio of the transmittance weighted with the Gaussian distribution for the mode number.

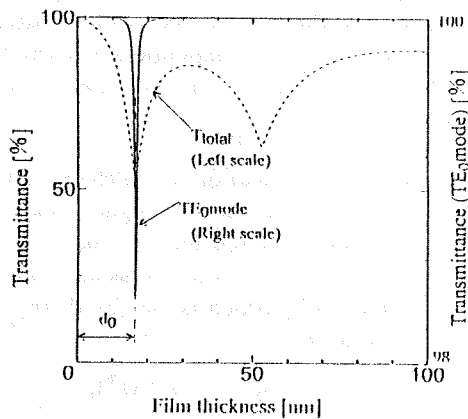


Fig. 11. Dependence of transmittance on  $d$ .  $T_{\text{total}}$ : total transmittance of  $T_{\text{TE}}$  and  $T_{\text{TM}}$  as 0.5:0.5;  $\text{TE}_0$  mode: transmittance for the  $\text{TE}_0$  mode.

accordance with the Gaussian distribution.  $T_{\text{TE}}$  and  $T_{\text{TM}}$  are shown as broken curves and the total transmittance  $T_{\text{total}}$  is shown as a dash-dotted curve when the existence ratio between  $T_{\text{TE}}$  and  $T_{\text{TM}}$  is assumed to be 0.5:0.5 for the addition of  $T_{\text{TE}}$  and  $T_{\text{TM}} = 1$  in Fig. 9.  $C$  is  $0.5 \times 10^{-10}$ , by fitting of  $T_{\text{total}}$  to the transmittance  $T_{\text{exp}}$ , which is shown as the solid curve in Fig. 9 as the experimental result for Sample #2 at a wavelength of 632.8 nm. The profile of the existence ratio of the transmittance which is weighted with the Gaussian distribution for the mode number is shown in Fig. 10.

The first peak of  $\alpha_m$  (refer to Figs. 2 and 5) is the first valley of  $T_{\text{exp}}$ , at which the value of the thickness is  $d_0$ . It is clarified that  $d_0$  is the first valley of the TE mode from Fig. 9. The value of  $d_0$  in  $T_{\text{exp}}$  is 16.3 nm.

From Tables I and II, the change of the value of  $d_0$  is small through the mode numbers for the TE mode compared with the TM mode. Hence the error by misreading is smaller for the TE mode. In addition,  $d_0$  of  $T_{\text{TE}}$  is smaller than that of  $T_{\text{TM}}$ ; namely, the second valley of  $T_{\text{total}}$  in Fig. 9.  $n'_t$  for the thinner films can also be determined by considering the TE mode. Therefore, we obtain  $n'_t$  from the value of  $d_0$  for the TE mode.

Figure 11 shows  $T_{\text{total}}$  and the transmittance for the

Table III.  $n'_t$  from  $d_0$  for the  $\text{TE}_0$  mode, by the calculation and  $n'_t$  by ellipsometry, at  $\lambda = 632.8$  nm.

| Sample # | $\text{TE}_0$ | Ellipsometer |
|----------|---------------|--------------|
| 1        | 3.45          | 3.49         |
| 2        | 2.88          | 2.89         |
| 3        | 1.80          | 1.81         |

$\text{TE}_0$  mode. It is clarified that  $d_0$  corresponds to the first valley of the  $\text{TE}_0$  mode from Fig. 11. From the calculation, it is confirmed that the values of  $d_0$  of the transmittance for the  $\text{TE}_0$  mode,  $T_{\text{TE}}$  and  $T_{\text{total}}$  correspond by the digit of 0.1 nm. Therefore, it is clarified that only the  $\text{TE}_0$  mode has to be taken into account without considering higher modes. In this manner, the value of  $n'_t$  is 2.88.

Table III shows the values of  $n'_t$  determined using this method and the ellipsometer. The values determined using this method agree with those determined using the ellipsometer.

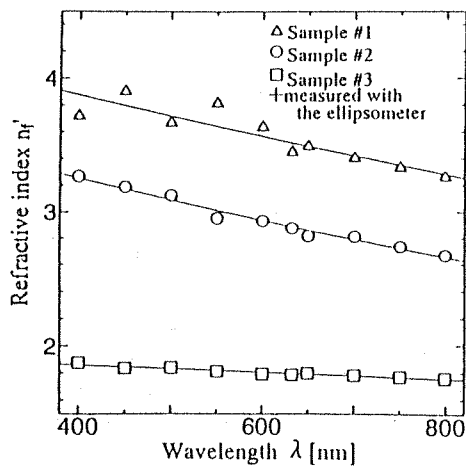
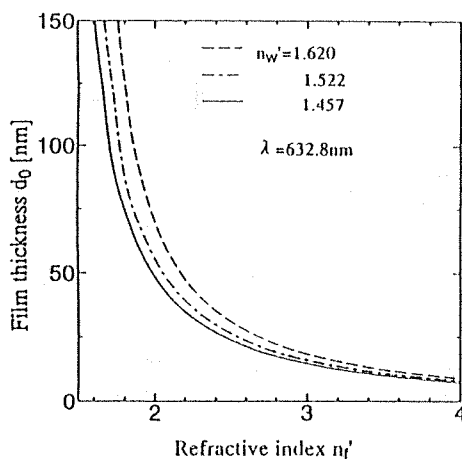
#### 4. Distribution of the Refractive Index

From correspondence of the value of  $d_0$  of the calculation for the  $\text{TE}_0$  mode to the value of  $d_0$  of the experiment,  $n'_t$  is obtained for the wavelength at every 50 nm between 400 nm and 800 nm. Figure 12 shows the measurement results for the three films which have different  $n'_t$ . The continuous values of the refractive index of the SOW are calculated by interpolating a quadratic function in the discontinuous values of the official refractive index data of T-4040. The measurement results of the film on the Si substrate placed close to the sensor with the ellipsometer at 632.8 nm, namely, the values in Table III, are also shown as + plots in Fig. 12.

From Fig. 12, it is clarified that the amount of fluctuation is especially large under 550 nm in Sample #1, while the amount of fluctuation is small in Samples #2 and #3. Figure 13 shows the dependence of  $d_0$  on  $n'_t$  obtained by the four-layer SOW simulation. The solid curve is the result at a value of  $n'_w$  of 1.457 used for the experiments in this section. It is clarified from Fig. 13 that the error of  $n'_t$  becomes large when  $n'_t$  enlarges because the accuracy of  $d_0$  by reading is constant. In the experiments, it is considered that the amount of fluctuation is large for the shorter wavelengths in Sample #1 as shown in Fig. 12 because the significant value of  $d_0$  is the digit of 1/10 nanometer. The dependences of  $d_0$  on  $n'_t$  are also shown in Fig. 13, when the values of  $n'_w$  are 1.522 (borosilicate glass) and 1.620 (bisphenol Z polycarbonate<sup>16)</sup>). It is clarified that the error caused by misreading at a large  $n'_t$  becomes smaller by using the smaller difference between  $n'_w$  and  $n'_t$ . Therefore, in this situation, the amount of fluctuation of  $n'_t$  is smaller when a SOW with a large  $n'_w$  is applied.

#### 5. Conclusions

The transmittance of light guided through the SOW oscillates periodically with deposition of a silicon film on the SOW. The period of the oscillation becomes smaller when  $n'_t$  enlarges. Therefore, it was shown that the value

Fig. 12. Distributions of  $n'_f$ .Fig. 13. Dependence of  $d_0$  on  $n'_f$ . Broken curve: at  $n'_w = 1.620$ ; dash-dotted curve: at  $n'_w = 1.522$ ; solid curve: at  $n'_w = 1.457$ .

of  $n'_f$  can be measured by depositing a silicon thin film on a SOW whose refractive index and sizes are known. The peaks of  $\alpha_m$  obtained from the calculation by considering all the modes of the four-layer SOW simulation, namely, the minimum film thickness  $d_0$  by which the valleys appearing in the dependence of transmittance on  $d$  is given, correspond to  $d_0$  for the  $TE_0$  mode above a digit of 0.1 nm. Therefore, without considering the higher TE

modes or the TM mode, it was clarified that  $n'_f$  with a thickness of 16.3 nm can be measured from the correspondence of the calculation result of the transmittance for the  $TE_0$  mode only to the experimental value of the first valley appearing in the dependence of transmittance on  $d$ . Good agreement was obtained in comparison of the result of this method with that of the ellipsometry at a wavelength of 632.8 nm. Moreover, it was shown that the distributions of  $n'_f$  of silicon films are obtained at wavelengths of 400 to 800 nm. It was shown that the error caused by misreading  $d_0$  can be reduced by using a SOW with a larger  $n'_w$ . As a result, the amount of fluctuation of  $n'_f$  can be reduced.

#### Acknowledgement

This work was supported by a Waseda University Grant for Special Research Projects in 1996 and by a Grant-in-Aid for Scientific Research from the Ministry of Education, Science, Sports and Culture.

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## Fabrication of SiN Film by Using Coaxial Line Type MPCVD System with a Longitudinal Magnetic Field

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A double tubed coaxial line type MPCVD (Microwave Plasma Chemical Vapor Deposition) system with a longitudinal magnetic field has been developed for high quality SiN film deposition. The deposition rate of the film was increased because of the confinement and the enhancement of the microwave plasma due to the electrical and magnetic interaction. The experimental results and discussion are reported

### 1. Introduction

SiN films have been widely used in integrated circuits as inter layer insulator, gate insulator etc. In order to deposit high quality SiN films with a reasonable deposition rate under low substrate temperature a double tubed coaxial line type MPCVD (Microwave Plasma Chemical Vapor Deposition) system with a longitudinal magnetic field has been developed. [1-4]

The plasma density could be increased and uniformed by the electrical and magnetic interaction. The magnetic field confines the plasma ions and electrons, depresses their diffusion from the center part to the wall of the discharge tube. Then a strong uniform and stable plasma could be remained during the deposition time. Therefore the dissociation of the source gas (SiH<sub>4</sub>) and the deposition rate of SiN film could be increased comparing with those parameters without the magnetic field.

The experimental system, conditions, results and discussion are reported.

### 2. Experiment

The experimental system is shown as in Fig.1. The SiH<sub>4</sub> gas was mixed with N<sub>2</sub> plasma and dissociated on the end of the inner tube. The distance from the end of the discharge tube to the end of the inner tube is defined as  $z$ . The  $z$  could be  $-1.0 \pm 1$  cm in our experiment.

A longitudinal magnetic field was applied on the microwave plasma by setting a coil with a current  $I$  on the cylindrical cavity in this system. A strong, uniform and stable plasma blew off into the deposition chamber. The high quality SiN film was deposited on the substrate. The distance between the substrate and the end of the discharge tube was 10 cm.

The experimental conditions are shown as in table 1

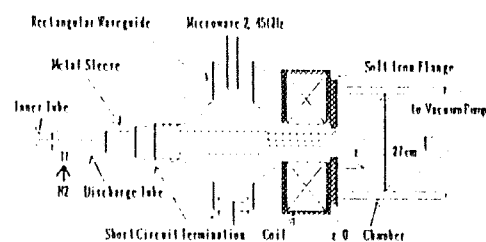


Fig. 1. Experimental Apparatus

Table 1 Experimental conditions

|   |                 |
|---|-----------------|
| microwave input power                           | 200 W           |
| microwave reflection power                      | 20 W            |
| N <sub>2</sub> gas flux rate                    | 115 ml/min      |
| SiH <sub>4</sub> gas flux rate                  | 5 ml/min        |
| chamber pressure                                | 3.4 mtorr       |
| current in the coil                             | 0-15 A          |
| magnetic flux density at the center of the coil | 0-2637 Gauss    |
| position of the inner tube $z$                  | $-1.0 \pm 1$ cm |
| temperature of the substrate                    | R.T.            |

The plasma parameters like electron density and temperature were measured by a single probe. [5] The SiN film thickness and the deposition rate were measured and calculated by a needle thickness monitor. The film refractive index was measured by an ellipsometer. Other characteristics like the contents of N-H bonds, Si-H bonds and Si-N bonds were measured and calculated by the infrared absorption spectrum. The dangling bond density was measured by the electron spin resonance spectrum. The optical energy gap was measured by the UV absorption spectrum.

### 3. Experimental results and discussion

Fig. 2 shows the dependence of the electron density on the magnetic field at  $z=1$  cm. The electron density was increased with increasing of the magnetic field rapidly from about 600 Gauss to about 1000 Gauss because of the electrical and magnetic

interaction. The magnetic field confined the plasma ions and electrons, depressed their diffusion from the center part to the wall of the discharge tube. Then a strong uniform and stable plasma could be remained during the deposition time while the magnetic field kept around 1000 Gauss<sup>3)</sup>. The electron density saturated when the magnetic field was over 1000 Gauss.

Fig.3 Shows the dissociation of the source gas SiH<sub>4</sub> vs. magnetic field. It is clear that when the magnetic field was kept around 1000 Gauss, the source gas was dissociated in the confined and enhanced plasma much more than that without the magnetic field. Therefore the SiN film deposition rate would be much high as shown in Fig. 4 in above mentioned confined and enhanced plasma.

All the characteristics of the film deposited in this new system with the longitudinal magnetic field, like refractive index, the contents of N-H bonds, Si-H bonds and Si-N bonds, the dangling bond density and the optical energy gap did not change much comparing with those without the magnetic field. But the deposition rate could be increased much more.

The further detail is being investigated and will be reported later.

#### Aknowlegement:

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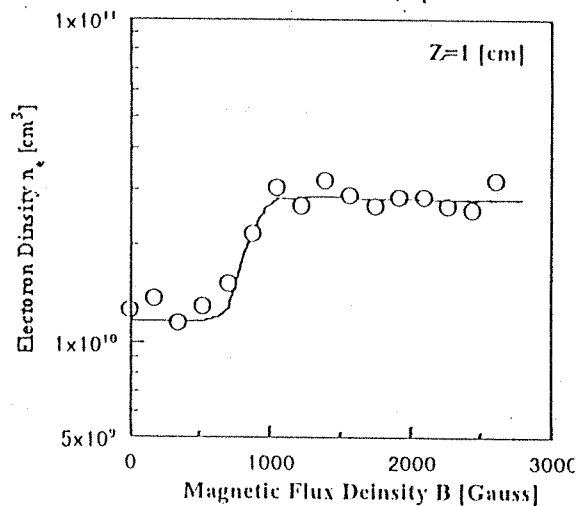


Fig2. Dependence of electron density on magnetic flux density

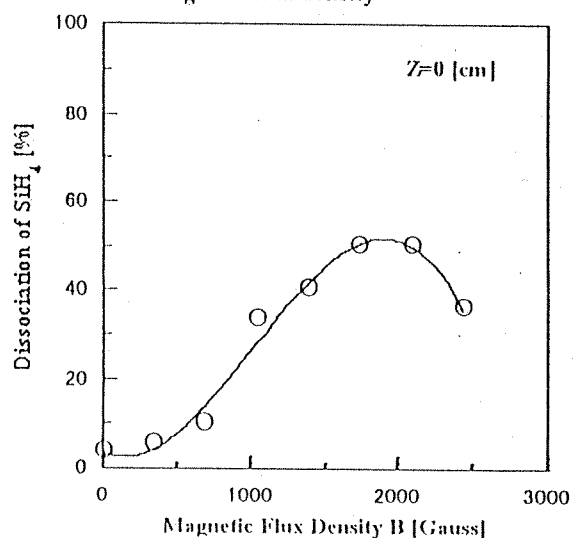


Fig 3. Dependence of dissociation of SiH<sub>4</sub> on magnetic flux density

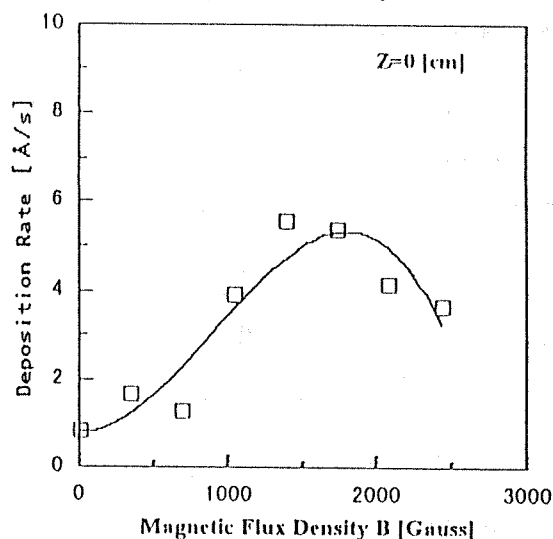


Fig-4 Dependence of deposition rate on magnetic flux density

# Influence of Longitudinal Magnetic Field Applied to Coaxial Line Type Microwave Plasma(IV)

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In the double tubed coaxial line type microwave plasma chemical vapor deposition system, a magnetic field along the gas flow is applied to the plasma, and the effects of applying longitudinal magnetic field to the plasma is considered. The spatial distributions of electron density in the discharge area are measured by a single probe method. It is determined that radial distribution of electron density at the discharge area is uniform, and the plasma inside of the discharge area extends keeping the density constant to the vicinity of the place where plasma blows off into the deposition chamber. Therefore, uniform and stable plasma which is proper for CVD system is generated by applying a magnetic field.

## 1. Introduction

In the double tubed coaxial line type microwave plasma chemical vapor deposition system, in order to generate the stable plasma in a wider range of gas pressure and with various kinds of gases, a magnetic field along the gas flow (longitudinal magnetic field) is applied to the discharge area, and the effects of applying longitudinal magnetic field to plasma have been considered by a single probe method. The plasma parameters of  $N_2$  plasma have been measured in the deposition chamber and the effects of applying a magnetic field have been considered. And it was determined that the stability of the plasma is improved<sup>[1]</sup> and electron density can be increased by a few times with magnetic field over about 1000Gauss in the vicinity of the place plasma blows off into the deposition chamber<sup>[2]</sup>. In this report, the spatial distribution of plasma parameters in the radial and axial direction in the discharge area are measured by the single probe method and the effects of applying such a magnetic field are considered.

## 2. Experiment

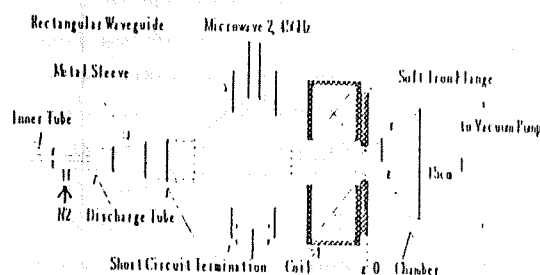


Fig. 1. Experimental Apparatus

Figure 1 shows experimental setup. The coil is set up around the discharge area, and a magnetic field along the gas flow is applied. Spatial distribution of electron

density in the discharge area is measured by single probe method and the effect of applying such a magnetic field is considered. The axial distance from the end of the discharge tube is defined as  $z$  and the radial distance from the center axis of the discharge tube is defined as  $r$ . The details of this system was reported in our previous work<sup>[1]</sup>.

The experimental conditions are shown in Table I. An experimental condition in which a good quality of SiN thin film is fabricated when magnetic field is 0Gauss and  $SiH_4$  gas flows in the inner tube is used. Single probe method is used in the measurement. The probe is a round plate which is 1mm in diameter. The surface of the probe is set up perpendicularly to the magnetic field so that the influence of the magnetic field on the probe I-V characteristic is minimized. Points of the measurement are every 5mm between  $z = -15mm$  and  $z = 5mm$ , and at each  $z$   $r = 0, 4, 8mm$ .

Table I. Experimental Condition

|  |             |
|--|-------------|
| Discharge Gas                              | $N_2$       |
| $N_2$ Gas Flow Rate                        | 50ml/min    |
| Microwave Input Power                      | 150W        |
| Microwave Reflective Power                 | 45W         |
| Gas Pressure in Chamber                    | 4.0mTorr    |
| Coil Current                               | 0~6A        |
| Magnetic Field (at the center of the coil) | 0~1986Gauss |
| Position of Inner Tube End                 | $z = -20mm$ |

## 3. Result and Discussion

Figure 2 shows the dependence of the electron density on magnetic field at  $z = 5mm$ . It is shown that electron density increases with increasing magnetic field from about 600Gauss to about 1000Gauss. Because the diffusion of the plasma toward the wall of the discharge tube is depressed, therefore, the decay of the plasma on the wall are depressed. The electron density saturates over

about 1000Gauss. Therefore, by applying a magnetic field over about 1000Gauss, electron density can be increased by a few times in the vicinity of the place the plasma blows off into the deposition chamber. And it can be said that those plasma is proper for CVD system because it is possible to fabricate films at a high rate. Figure 3 and 4 show the dependences of the electron density on magnetic field at  $z = 0, -10$ mm. Figure 2, 3 and 4 show electron density under about 600Gauss at  $z = 0$  or 5mm are lower than that at  $z = -10$ mm, but over about 1000Gauss those electron densities are almost the same. The reason is as following. At  $z = -10$ mm electron density is high and stable regardless of magnetic flux density and doesn't fluctuate so much(as shown in Fig.4). On the contrary, at  $z = 0$ mm electron density is low and unstable, and fluctuates when magnetic flux density is under about 600Gauss (as shown in Fig.3), and the same tendency is shown at  $z = 5$ mm. Those fluctuation are suppressed by applying a magnetic field.

Figure 5 shows the dependence of electron density on  $r$ . The saturated value of the electron density vs. magnetic field are averaged when magnetic field is over about 1000Gauss. At each  $z$ , radial distribution of electron density is not the shape like as described as  $J_0$  Bessel function but the shape like as trapezoid. Because the discharge is done by the microwave that propagates plasma as the fundamental mode of coaxial line. It means uniform plasma in radial direction can be generated.

The further details including the tendency of electron temperature will be reported later.

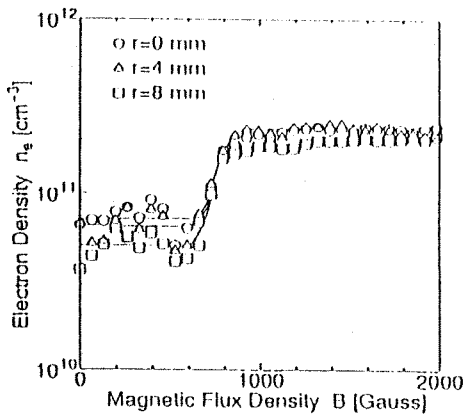


Fig. 2. Dependence of Electron Density on Magnetic Field ( $z = 5$ mm)

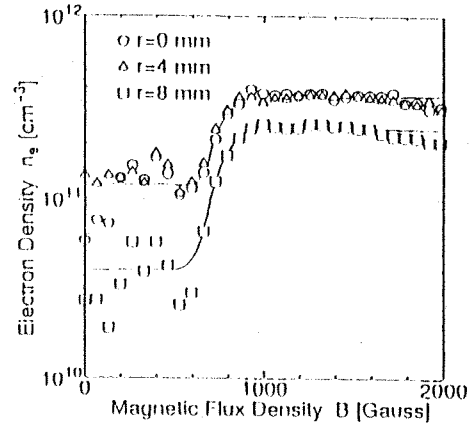


Fig. 3. Dependence of Electron Density on Magnetic Field ( $z = 0$ mm)

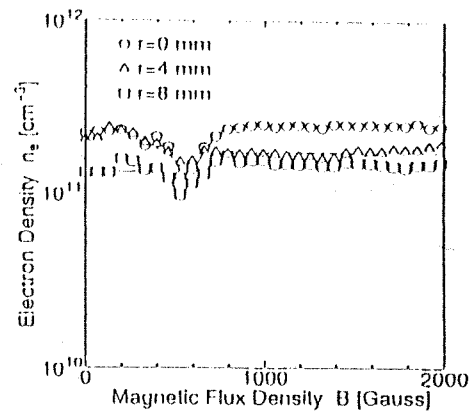


Fig. 4. Dependence of Electron Density on Magnetic Field ( $z = -10$ mm)

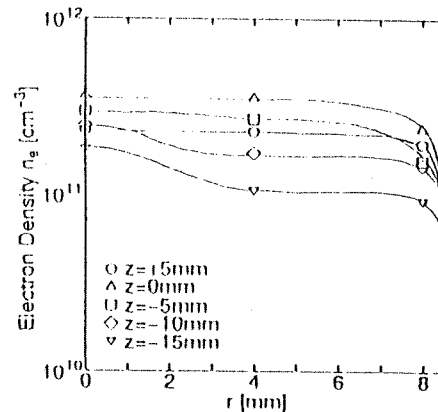


Fig. 5. Dependence of Electron Density on  $r$  ( $B \geq 993$  Gauss)

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# Separation of Film Surface Heating Effect and Ion Implanting Effect

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Generally in a plasma CVD method, a substrate table is placed in the discharge plasma and films are fabricated under the ion bombardment. We have studied influences of the ion bombardment on a-Si:H films and clarified that an ion bombardment has a film surface heating effect and other effects (ion implanting effect) in films [1]. Even if the ion bombardment is increased, it is impossible to discuss whether film properties become good or not. In this paper, the film surface heating effect and the ion implanting effect of the ion bombardment are separately studied and discussed.

## 1. Introduction

We have developed the double tubed coaxial line type microwave plasma CVD (MPCVD) system to deposit a-Si:H films. In this paper, in order to study the ion implanting effects on a-Si:H films the dependence of the film properties on sheath voltage ( $V_{sh}$ ) without heating substrate table and the dependence of the film properties on the substrate temperature ( $T_s$ ) without the ion bombardment are measured [2]. The dependence of film properties on  $T_s$  is equivalent to that on the film surface heated by the ion bombardment effect. By subtracting the dependence of film properties on  $T_s$  from the dependence of film properties on  $V_{sh}$ , the ion implanting effect is left. Hence we try to put two axes together from the two figures of the dependence of Si concentration on  $T_s$  and  $V_{sh}$ , then the Si concentration in the film seems to be influenced by only the film surface heating effect. In the dependence of other film properties, two axes are put together in the same way and the film surface ion bombardment heating effect and the ion implanting effect have been separated.

## 2. Experiment

Figure 1 shows the configuration of the MPCVD system. The axial distance from the discharge tube end is defined as  $z$ . The substrate table area is  $40 \text{ cm}^2$  and is placed at  $z=10 \text{ cm}$ . Ar gas flow rate is  $110 \text{ ml/min}$  and  $\text{SiH}_4$  gas flow rate is  $30 \text{ ml/min}$ . When DC substrate bias voltage ( $V_{dc}$ ) is varied from  $+40 \text{ V}$  to  $-80 \text{ V}$ ,  $V_{sh}$  can be controlled from  $0 \text{ V}$  to  $-95 \text{ V}$ . The dependence of  $V_{sh}$  on  $V_{dc}$  has been measured by single probe method. The probe of  $0.05 \text{ cm}$  in diameter and  $1 \text{ cm}$  in length is used. The

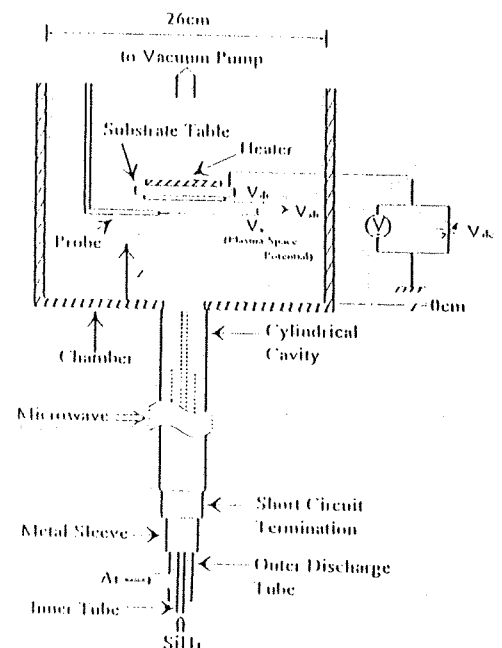


Fig. 1. Configuration of the MPCVD system

measurement was performed at  $z=9$  cm. In the case of the film property dependence measurement on  $T_s$ ,  $V_{sh}$  is 0 V (namely  $V_{dc}$  is +40 V) and  $T_s$  is varied from R.T. to 250 °C.

### 3.Result and Discussion

The dependence of Si concentration on  $T_s$  (at  $V_{sh}=0$  V) and the dependence of Si concentration on  $V_{sh}$  (at  $T_s=30$  °C) are shown in Fig.2. In this figure the Si concentration at  $V_{sh} = 0$  V and that at  $T_s = 30$  °C must be the same because they are deposited at the same condition. Because the ion implanting dose not change the Si concentration of the film, considering only the film surface heating effect, we can adjust the unit of  $T_s$  axis to fit the Si concentration at  $T_s = 250$  °C to that at  $V_{sh} = -95$  V. By this way a linear relationship between  $T_s$  and  $V_{sh}$  is obtained as following experience equation.

$$T_s = -2.3158 V_{sh} + 30$$

After two axes are put together in this way, the dependence of two other a-SiH film properties on  $T_s$  and  $V_{sh}$  is shown in Fig.3 and Fig.4. The arrows in Fig.3 and Fig.4, namely the difference of two curves, shows the amount of the ion implanting effect. The dependence of SiH concentration on  $T_s$  and  $V_{sh}$  is shown in Fig.3. From the figure the concentration of SiH bond increases by the ion implanting effect in the range of  $V_{sh} < -40$  V because the hydrogen ions accelerated by  $V_{sh}$  are implanted in film. The dependence of dangling bond density on  $T_s$  and  $V_{sh}$  is shown in Fig.4. From the figure dangling bond density increases by the ion implanting effect because the Ar ions are implanted and cut bonds in film.

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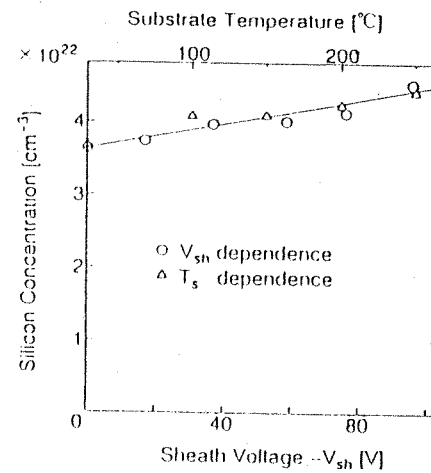


Fig.2. Dependence of Si concentration on  $T_s$  and  $V_{sh}$

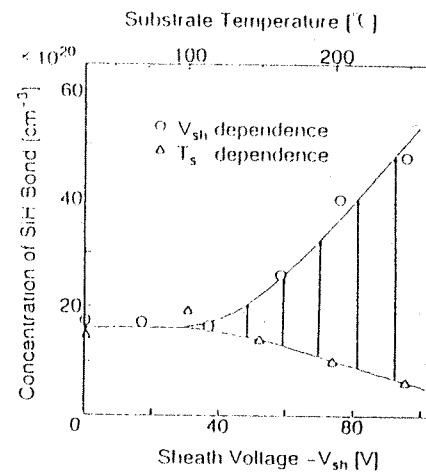


Fig.3. Dependence of SiH concentration on  $T_s$  and  $V_{sh}$

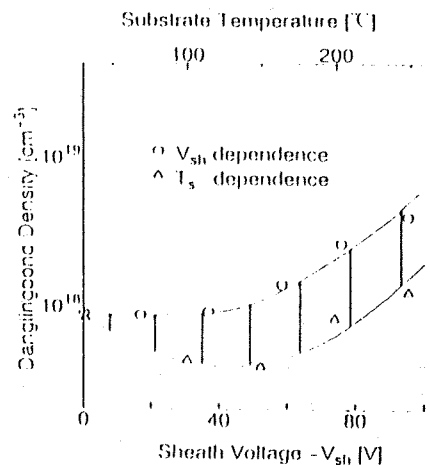


Fig.4. Dependence of dangling bond density on  $T_s$  and  $V_{sh}$



# In situ Measurement of Change of Ultra Thin Films in Elapsed Time Using Optical Fiber Sensors

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An *in situ* measurement method of change of ultra thin a-Si:H films with passage of time by leaking from vacuum to atmospheric air will be shown. a-Si:H film with approximately 10 nm in thickness is deposited on the core of an optical fiber sensor whose part of the clad is removed. The film is changed by oxidation and the oxidation saturates in approximately 600 s. The larger attenuation of translated light maybe due to the change of defects by relaxation at the long wavelengths from 685 to 800 nm is observed.

## 1. Introduction

In thin film fabrication, the change of the films just after a leak by atmospheric air was not measured when fabrications were finished. The measurement of the surface oxidation layer of thin films was usually obtained by executing the etching of the surface and measurement of the X-ray photoelectron spectroscopy alternatively after leaking by atmospheric air and putting the films out of a fabrication chamber. In this case, the film surface oxidation progress measurement of change in elapsed time after the leak from vacuum to atmospheric air is not completed.

We have studied a method to measure the dependence of the light transmittance on the film thickness with depositing films on an optical fiber whose part of the clad is removed as a sensor for the measurement of the optical constants of ultra thin films deposited with the Plasma CVD. During the deposition of films in the plasma CVD system, the transmitted light which goes through the sensor decreases exponentially with periodic oscillation corresponding to the increase of film thickness. The reason is that the electric field strength concentrates periodically in the film. By removing the oscillation mathematically, we determined the optical energy gap[1]. Then, we also determined the refractive index from the value of the first valley in the oscillation or the period of the oscillation[2,3]. In our new method, we have been able to measure the optical energy gap of the ultra thin a-Si:H film with approximately 20 nm in thickness which is about 1/40 comparing with what in the conventional method and the refractive index of the ultra thin a-Si:H film with approximately 10 nm in thickness[1,2]. The sensitivity of the sensor is increased more by decreasing the diameter of the optical fiber and / or

increasing the length of the film deposited part.

In this report, using this optical fiber sensor in the a-Si:H fabrication, we show an *in situ* measurement method of change of ultra thin films with passage of time just after the leak of atmospheric air.

## 2. Experimental Setup and the Optical Fiber Sensor

### Our experimental setup - the double-tubed coaxial-line-type microwave plasma CVD

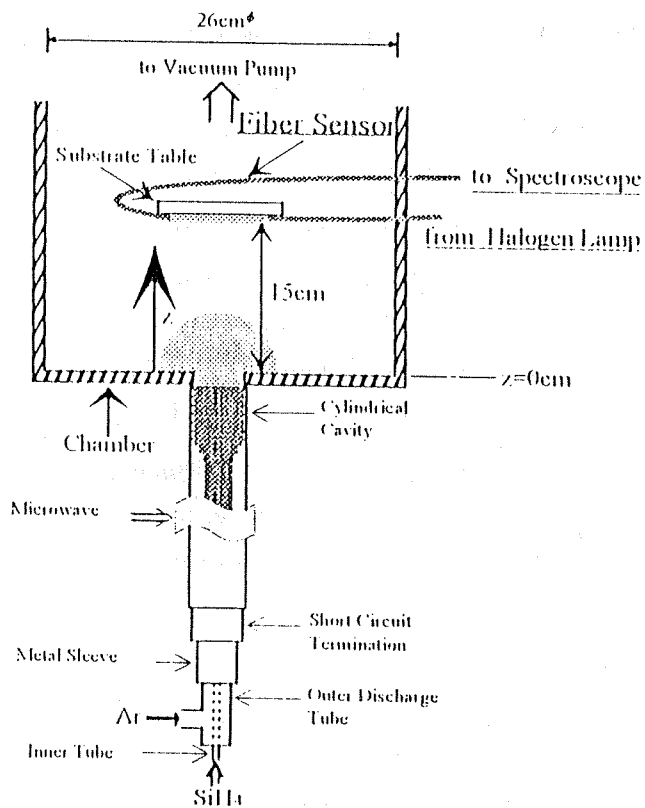


Fig. 1. Experimental setup, with our optical fiber sensor.

system is shown in Fig. 1[4]. As shown in Fig. 1, a-Si:H is fabricated from  $\text{SiH}_4$  by using Ar plasma flowing from the bottom side of the system.

The optical fiber sensor is set on the substrate table in this chamber. The input port of the optical fiber is connected with a halogen lamp light source and the output port is connected with a spectrum analyzer. Transmitted light is measured in about 10 minutes after the fabrication.

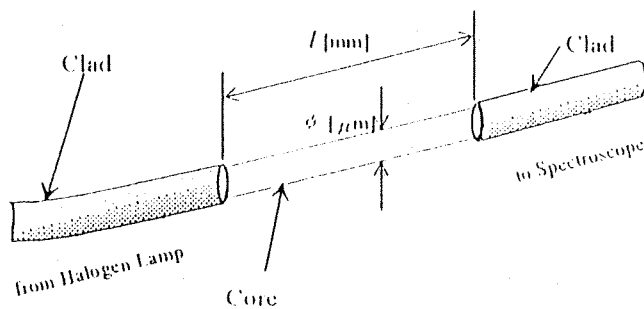


Fig. 2. Details of the optical fiber sensor.

Figure 2 shows the optical fiber sensor structure. This is a step index type optical fiber with silica core and polymer clad. The clad is removed for deposition of a-Si:H films. The length of the clad removed part is  $l$  [mm] and its diameter of the core is  $\phi$  [ $\mu\text{m}$ ].

### 3. Result and Discussion

Using the optical fiber sensor, whose length of the film deposited part  $l$  is 100 nm and diameter of the core  $\phi$  is 110  $\mu\text{m}$ , a-Si:H film with approximately 10 nm in thickness is fabricated on the optical fiber sensor. The film change by oxidation is measured *in situ*. The period to take the leak of the CVD chamber from vacuum to atmospheric air is approximately 20 s.

Figure 3 shows the change of light transmittance through the optical fiber sensor with passage of time at wavelengths of 800, 750, 700 and 685 nm. From Fig. 3, it is clarified that the transmittance at every wavelength decreases after leaking the CVD system and it saturates in approximately 600 s. It is considered that the film is changed by oxidation and the oxidation saturates around 600 s. By comparing the rate of the change of transmittance among the wavelengths, it is clarified that the large rate of the change occurs at long wavelengths. It was reported that defects are changed by relaxation by the bias light in the region of 0.8 eV

$< h\nu < 1.8$  eV for a-Si:H because of the shift of the quasi-Fermi-level to the conduction band or an increase in the concentration of dangling-bond centers D $^-$ [5,6]. The result in this experiment shows the similar tendency to the dependence of the absorption coefficient on energy owing to the change of defects described in above references. We consider that the similar phenomena occur by oxidation in the high energy side of the Urbach tail region ( $1.5$  eV  $< h\nu < 1.8$  eV). The more specific discussion will report at the presentation.

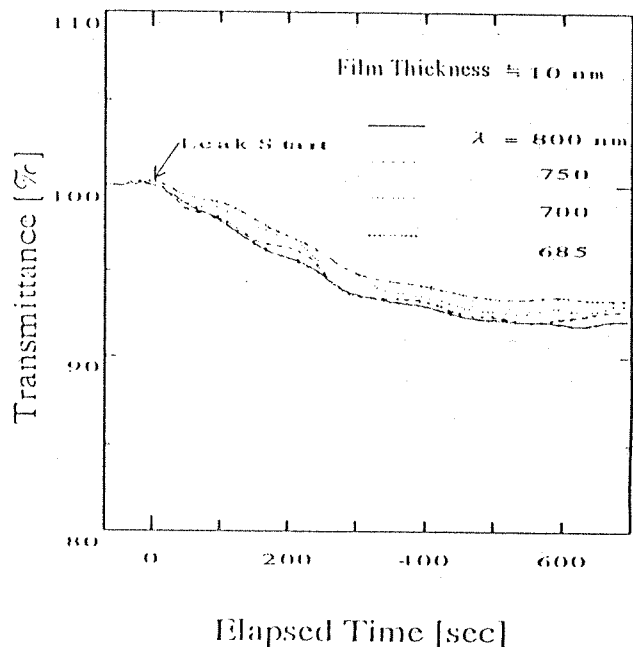


Fig. 3. Transmittance change with passage of time.

### Acknowledgment

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# 二重管式同軸線路形マイクロ波プラズマCVDにおける N<sub>2</sub>/SiH<sub>4</sub>プラズマのパラメータの空間分布

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Spatial Distribution of Plasma Parameter in N<sub>2</sub>/SiH<sub>4</sub> Plasma  
in Double Tubed Coaxial Line Type Microwave Plasma CVD System  
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We have confirmed the new method of probe measurement in N<sub>2</sub>/SiH<sub>4</sub> plasma. Using this method, we have measured the spatial distribution of plasma parameters such as electron temperature  $T_e$ , electron density  $n_e$ , plasma space potential  $V_s$ , floating potential  $V_f$  and sheath voltage  $V_s-V_f$  with varying the gas flow rate of SiH<sub>4</sub> in the chamber of the double tubed coaxial line type microwave plasma CVD (MPCVD) system. In this paper, we report the spatial distribution of these plasma parameters in the chamber of this MPCVD system. And it is cleared that the plasma is very uniform in the chamber.

キーワード: マイクロ波プラズマ、プラズマパラメータ、シングルプローブ法、イオンボンバードメント、空間的アフターグロープラズマ

## 1. まえがき

プラズマを用いた化学気相堆積 (CVD) 法の研究は現在盛んに行われており、水素化アモルファスシリコン (a-Si:H) 膜や窒化シリコン (SiN) 膜をはじめ各種の薄膜の作製に用いられている。一般に良く用いられている高周波プラズマCVD法では、電力が供給されているプラズマ (放電プラズマ) 内で膜を作製しているため、膜表面は常にイオン衝撃にさらされているという問題が生じる。そこで筆者らは、イオン衝撃を抑えるために、マイクロ波を円筒キャビティ内に閉じ込めて、堆積室内には電力注入のないプラズマ (空間的アフターグロープラズマ) を生成できる二重管式同軸線路形マイクロ波プラズマCVD装置の研究開発を行ってきた<sup>1)</sup>。また、本装置におけるプラズマは、イオンがマイクロ波の電界に追従できないためにイオン温度の低いコールドプラズマとなる。このような特長を持つ本装置の堆積室内においては、前述の空間的アフターグロープラズマ中で、またコールドプラズマ中で成膜が行われるので、膜表面へのイオンボンバードの少ない良質な a-Si:H 膜や SiN 膜が作製されることが期待できる。また、イオンボンバードがないことで膜表面が加熱されないため、低融点物質上に膜を堆積させることができる<sup>2)</sup>。

また、多くの研究機関で行われているプラズマCVD法に関する研究は、ガス流量、ガス圧、電力などの外部から

単独に直接制御可能な外部的プラズマパラメータを変化させて作製した膜の電子材料としての性質や、その応用上の良否について論じている。しかしながら、このような外部的プラズマパラメータは、装置の寸法や構造によって、その最適値が異なるので、これに基づいて、本質的な成膜機構を議論、解明することはできない。すなわち、電子温度、電子密度、プラズマ空間電位などの、外部から単独に直接制御できない内部的プラズマパラメータを測定し、これに基づいて、成膜機構を検討しなければならない。

このような内部的プラズマパラメータの測定には、ラングミュア・プローブ法が簡便かつ空間的分解能にすぐれた方法として知られている。しかしながら、シラン系ラジカルを含む反応性プラズマ中におけるプローブ測定では、プローブ上に膜が堆積して、その影響がプローブ電流電圧特性 ( $I_p-V_p$  特性) に現れる。そこで、正常な測定を行うためには、新たな工夫を要する。筆者等はこれまでに、導電性膜である、良質な a-Si:H 膜を堆積させることができる Ar/SiH<sub>4</sub> プラズマ中で、正常なプローブ測定を可能とする測定条件とその方法を明らかにしてきた<sup>3)</sup>。その上で、二重管式同軸線路形マイクロ波プラズマCVD装置の堆積室内での Ar/SiH<sub>4</sub> プラズマ中のプラズマパラメータの空間分布を測定により明らかにした<sup>4)</sup>。

また、絶縁性膜である SiN 膜を堆積させることができる N<sub>2</sub>/SiH<sub>4</sub> プラズマ中において従来のプローブ法によ

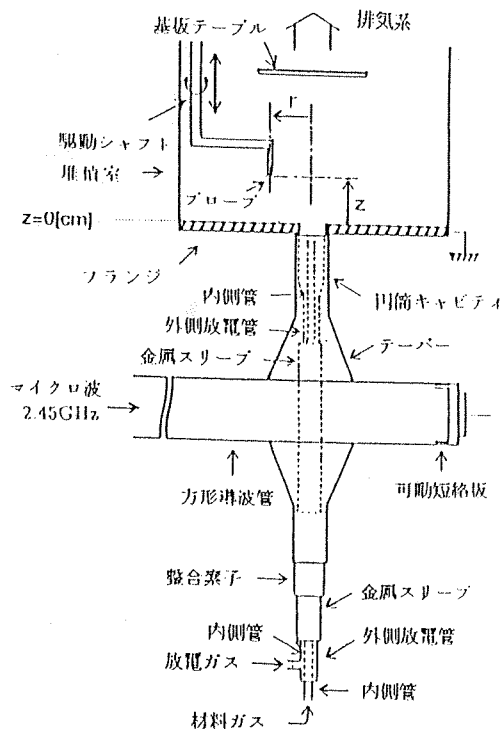


図1 二重管式同軸線路形マイクロ波プラズマCVD装置

Fig.1 Double Tubed Coaxial Line Type Microwave Plasma CVD System

り測定を行う場合、 $N_2/SiH_4$ プラズマ中における測定と同様にプローブ表面に $SiN$ 膜が堆積してしまうため、正常な $I_p-V_p$ 特性が得られないという問題が生じる。この問題を解決するために当研究室では、 $N_2/SiH_4$ プラズマ中での新しいプローブ測定法について明らかにしてきた<sup>(15)</sup>。本論文では、この方法を用いて、同装置の堆積室内における $N_2/SiH_4$ プラズマ中の電子温度、電子密度、プラズマ空間電位などのプラズマパラメータの空間分布を、 $SiH_4$ ガス流量を変化させて測定した結果について報告することを目的とする。

## 2. 実験

実験には、図1に示す二重管式同軸線路形マイクロ波プラズマCVD装置<sup>(14)(17)</sup>を用いた。プラズマ生成条件として、マイクロ波電力を270[W]一定とした。外側放電管には放電ガスとして $N_2$ ガスを流し、ガス流量は140[ml/min]と一定とした。内側管には材料ガスとして $SiH_4$ ガスを流し、ガス流量は0~50[ml/min]まで変化させた。また比較のために、内側管に $SiH_4$ ガスの代わりに $N_2$ ガスを流し、ガス流量を0~50[ml/min]まで変化させた。なお、ガス流量の測定時の圧力は1[atm]とした。堆積室内のガス圧は、

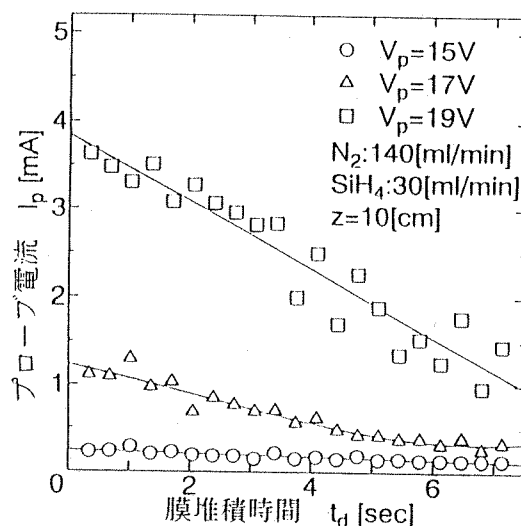


図2  $N_2/SiH_4$ プラズマ中でのプローブ電流の膜堆積時間依存性

Fig.2 Dependence of Probe Current on Film Deposition Time in  $N_2/SiH_4$  Plasma

内側管に流すガス流量によって、3.3~4.3[mTorr]まで直線的に変化した。

本装置の堆積室は、内直径26[cm]の円筒形である。放電管端、すなわち堆積室のフランジの内壁面の位置から堆積室の軸方向への距離を $z$ 、中心軸からの径方向への距離を $r$ と定義した(図1参照)。測定位置は、 $z$ は1.5~25[cm]の範囲で、 $r$ は0~10[cm]の範囲で変化させている。なお、内管端位置はチャンパー内に挿入されておらず、 $z=-1.4$ [cm]の点とした。

## 3. プローブ測定法

前述のように、 $N_2/SiH_4$ プラズマのプローブ測定では、プローブ上に $SiN$ 膜が堆積するため、正常な $I_p-V_p$ 特性を得ることは単純にはできない。そこで、筆者等は $N_2/SiH_4$ プラズマ中では図2のようにプローブ電流が膜堆積時間 $t_d$ とともに直線的に減少する領域があることに着目し、直線外挿をすることにより、膜が堆積していない場合( $t_d=0$ )に得られる正常な $I_p-V_p$ 特性を得ることができることを明らかにしてきた<sup>(14)</sup>。

すなわち、 $N_2/SiH_4$ プラズマを発生させて、放電開始から一定時間間隔(340[ms])で $I_p-V_p$ 特性を短時間(10[ms])で測定する。取り込んだ $I_p-V_p$ 特性から、あるプローブ電圧におけるプローブ電流の放電時間 $t_d$ 依存性を求める(図2参照)。この図を用いて、放電時間に対するプローブ電流 $I_p$ の減少が直線となる領域より最小自乗法を用いて、放電時間が0秒での、すなわちプローブ上に膜が堆積していないときの正常なプローブ電流値 $I_{p0}$ を算出する。これを異なるプローブ電圧についても行い、正常な $I_{p0}-V_p$ 特性を得る。

さらに、プローブ上に堆積した厚さ45 [nm] のSiN膜が、プローブに-200 [V] の負バイアスを印加して、電子温度が13,000 [K]、電子密度が $5.0 \times 10^9$  [cm<sup>-3</sup>] の純N<sub>2</sub>プラズマ中で約220秒間イオン bombard を行えば除去できることを明らかにしている<sup>13)</sup>。そこで、一連のプローブ測定ごとに、この条件でプローブ上に堆積したSiN膜の除去を行うことにより、同じプローブを繰り返し用いている。

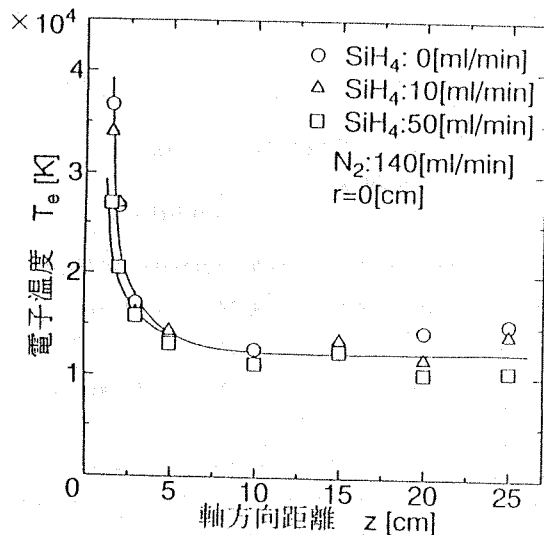


図3 電子温度のz依存性

Fig. 3 Dependence of Electron Temperature on z

## 4. 測定結果および考察

### 4. 1 電子温度T<sub>e</sub>の空間分布

図3に中心軸上 ( $r=0$  [cm]) の電子温度T<sub>e</sub>の軸方向距離z依存性を示す。SiH<sub>4</sub>ガス流量がいずれの場合も、T<sub>e</sub>はzの増加に対して、放電管端 ( $z=0$  [cm]) 付近で急激に減少した後、 $z>5$  [cm] ではほぼ一定となる。T<sub>e</sub>の高い放電管端付近では、内側管を通して流したSiH<sub>4</sub>分子または外側放電管を通して流出するN<sub>2</sub>分子と電子との、電離や解離をとまう非弾性衝突周波数が高く、T<sub>e</sub>の減少割合が大きい。放電管端から離れT<sub>e</sub>が低下すると、非弾性衝突断面積が小さくなるので、非弾性衝突周波数が減少し、T<sub>e</sub>の減少割合は小さくなる。従って、SiH<sub>4</sub>ガス流量を大きくすると高温部 ( $z<5$  [cm]) でT<sub>e</sub>の減少は、よりすみやかに起こることになる。また低温部 ( $z>5$  [cm]) では、SiH<sub>4</sub>ガス流量を大きくしてもT<sub>e</sub>はほとんど変化しない。

図4にT<sub>e</sub>の径方向距離r依存性を示す。T<sub>e</sub>はrの増加に対して、 $z=3$  [cm] では少し減少するが、 $z=10$  [cm] ではほぼ一定となる。また、SiH<sub>4</sub>ガスを増加させてもこ

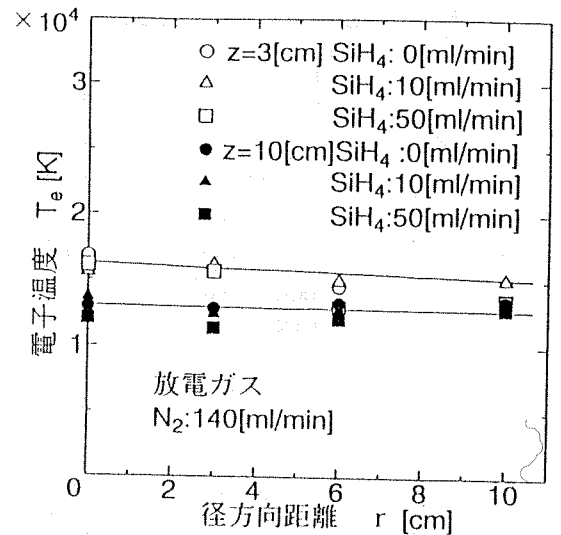


図4 電子温度のr依存性

Fig. 4 Dependence of Electron Temperature on r

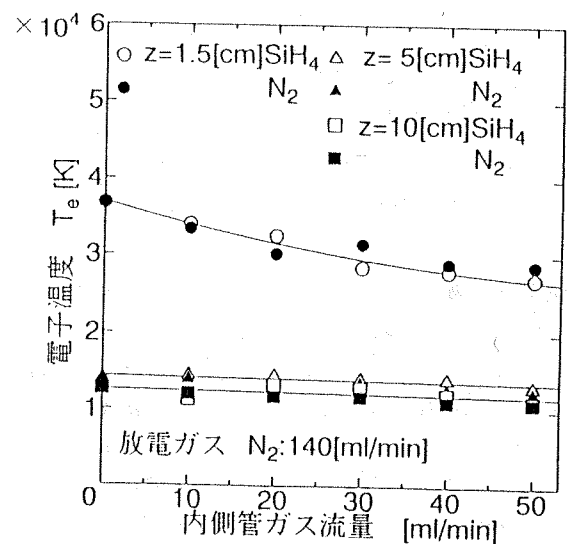


図5 電子温度の内側管ガス流量依存性

Fig. 5 Dependence of Electron Temperature on Gas Flow Rate of Inner Tube

の傾向はほとんど変化しない。図3、4より、 $z>10$  [cm] の空間では、z、r方向にT<sub>e</sub>は均一であることが分かる。

図5にT<sub>e</sub>のSiH<sub>4</sub>ガス流量依存性を○ ( $z=1.5$  [cm])、△ ( $z=5$  [cm])、□ ( $z=10$  [cm]) プロットで示す。T<sub>e</sub>は、前述のように放電管端付近の $z=1.5$  [cm] (T<sub>e</sub>の高い領域) ではSiH<sub>4</sub>ガス流量の増加にともない減少するが、 $z>5$  [cm] (T<sub>e</sub>の低い領域) ではSiH<sub>4</sub>ガス流量を増加してもほぼ一定となっている。このことより、図3において $z<5$  [cm] では2本の曲線とし、 $z>5$  [cm] では1本の曲線としてある。したがって、SiH<sub>4</sub>分子の解離のほとんどは、 $z<5$  [cm] のT<sub>e</sub>の高い領域で行われていること

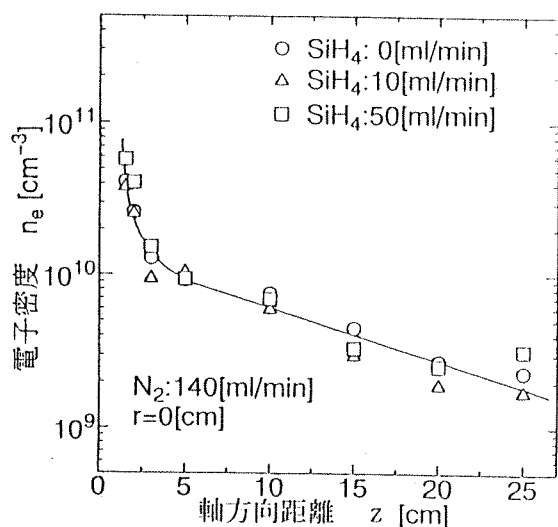


図6 電子密度の  $z$  依存性

Fig. 6 Dependence of Electron Density on  $z$

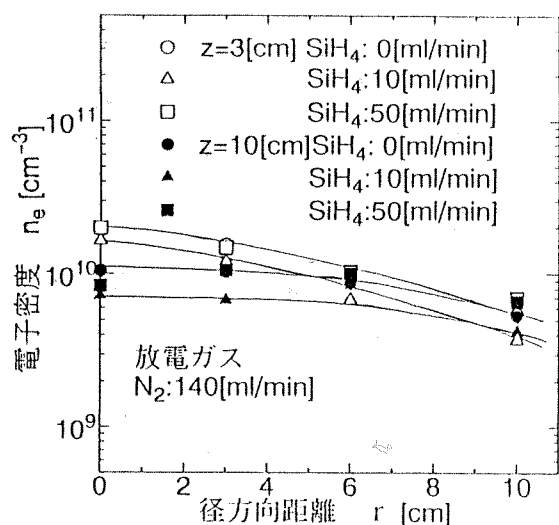


図7 電子密度の  $r$  依存性

Fig. 7 Dependence of Electron Density on  $r$

が分かる。また、内側管に  $N_2$  ガス (● ( $z = 1.5$  [cm])、▲ ( $z = 5$  [cm])、■ ( $z = 10$  [cm]) プロット) を流して同様の測定を行った。図5から明らかなように両ガスにおいてほとんど変化がないことから、堆積室内において電子を冷却する効果は  $SiH_4$  と  $N_2$  では大きな違いはないことが分かる。

#### 4. 2 電子密度 $n_e$ の空間分布

図6に電子密度  $n_e$  の  $z$  依存性を示す。 $SiH_4$  ガス流量がいずれの場合も、 $n_e$  は  $z$  の増加に対して、放電管端付近で急激に減少した後、 $z > 5$  [cm] では、指数関数的に減少する。また  $SiH_4$  ガス流量を変化させても  $n_e$  はほとんど変化しないことがわかる。

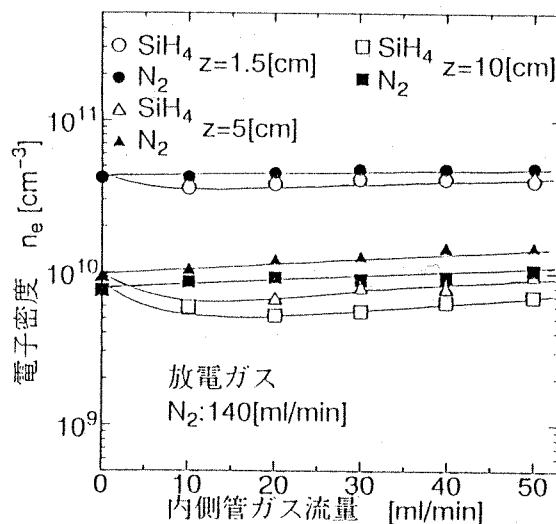


図8 電子密度の内側管ガス流量依存性

Fig. 8 Dependence of Electron Density on Gas Flow Rate of Inner Tube

図7に  $n_e$  の  $r$  依存性を示す。 $SiH_4$  ガス流量がいずれの場合も  $n_e$  は  $r$  の増加に対して、 $z = 3$  [cm] では減少するが、 $z$  が増加するほど  $r$  方向の均一性は良くなり、 $z = 10$  [cm] ではほぼ均一となる。

図8に  $n_e$  の内側管ガス流量依存性を示す。内側管に放電ガスと同じ  $N_2$  を流したときは、 $z$  がいずれの場合にも  $n_e$  は  $N_2$  ガス流量の増加に対してわずかに増加するが大きな変化はない (黒プロット)。内側管に  $SiH_4$  ガスを流すと、 $z$  がいずれの場合にも  $n_e$  はいったん減少するが、その後  $SiH_4$  ガス流量を増加させるとわずかに増加する (白プロット)。しかしながら図6で述べたのと同様に、 $SiH_4$  ガス流量を変化させても  $n_e$  は全体としては大きな変化はない。

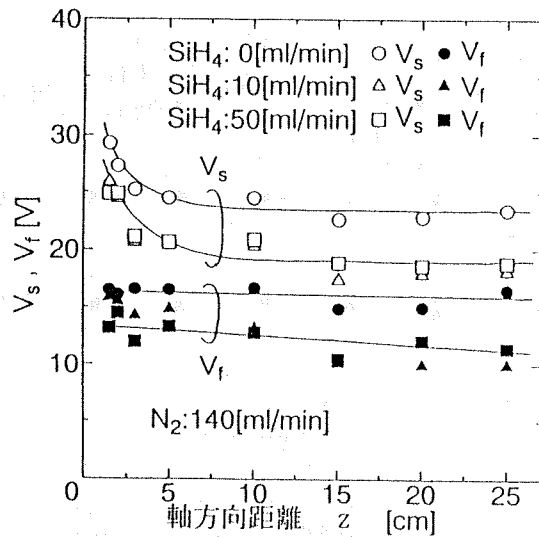
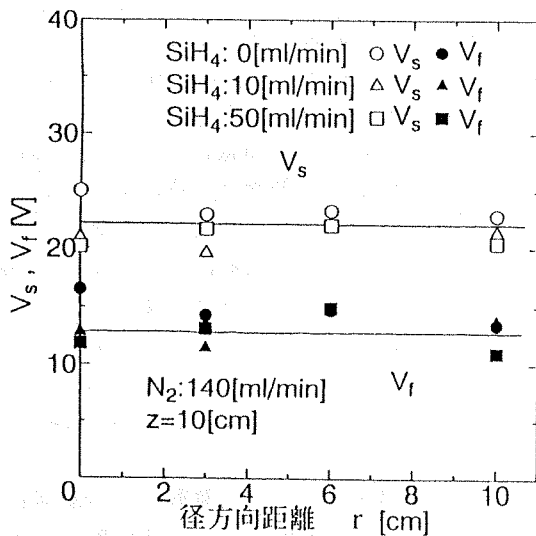
#### 4. 3 空間電位 $V$ 、および浮動電位 $V_f$ の空間分布

図9にプラズマ空間電位  $V$ 、および浮動電位  $V_f$  の  $z$  依存性を示す。 $V_f$  は、 $z$  の増加に対して放電管端付近で急激に減少した後、 $z > 5$  [cm] で緩やかに減少する。 $V$  は  $z$  の増加に対して、全領域で緩やかに減少する。

図10に  $V$ 、および  $V_f$  の  $z = 10$  [cm] における  $r$  依存性を示す。 $V$ 、および  $V_f$  は  $r$  方向にほぼ均一となることがわかる。

図11 (a)、(b) にそれぞれ  $z = 1.5$  [cm]、10 [cm] のときのプラズマ空間電位  $V$ 、及び浮動電位  $V_f$  の内側管ガス流量依存性を示す。 $V$ 、および  $V_f$  は、 $SiH_4$  ガスを加えることによって減少するが、 $SiH_4$  ガス流量を10 [ml/min] 以上に増加させても、ほとんど変化しない。また、内側管に  $N_2$  ガスを流した場合には、全領域でほとんど変化しない。

プラズマ中で成膜を行う際、基板を絶縁したときに基板とプラズマの間にできるシース電圧は、空間電位と浮動電位の差  $V - V_f$  で与えられる。なお、 $SiN$  膜のような絶

図9 空間電位・浮動電位の  $z$  依存性Fig. 9 Dependence of Space Potential and Floating Potential on  $z$ 図10 空間電位・浮動電位の  $r$  依存性Fig. 10 Dependence of Space Potential and Floating Potential on  $r$ 

線性の膜の場合には基板をアースしておいても成膜中の膜表面は絶縁状態にあることになる。従って、イオンは、このシース電圧によって加速され、膜に衝撃を与える。

図12に $V_s$ 、 $V_f$ の $z$ 依存性を示す。 $V_s$ 、 $V_f$ は $z$ の増加に対して放電管端付近で急激に減少した後、 $z > 5$  [cm]ではほぼ一定となる。また、 $\text{SiH}_4$ ガス流量を変化させても、ほとんど変化しない。さらに、 $z \geq 10$  [cm]においては、 $V_s$ 、 $V_f$ は $r$ 方向に均一であることも確認している。これらの結果から、 $V_s$ 、 $V_f$ は $\text{SiH}_4$ ガス流量にかかわらず、 $z > 10$  [cm]の空間で $z$ 、 $r$ 方向に均一であることが分かる。すなわち、この空間では、膜に与えられるイオン衝撃エネルギーは全膜面上で均一であることが分かる。また、

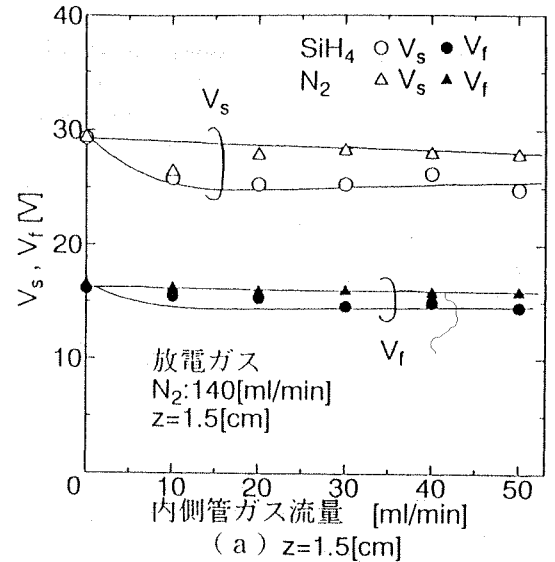
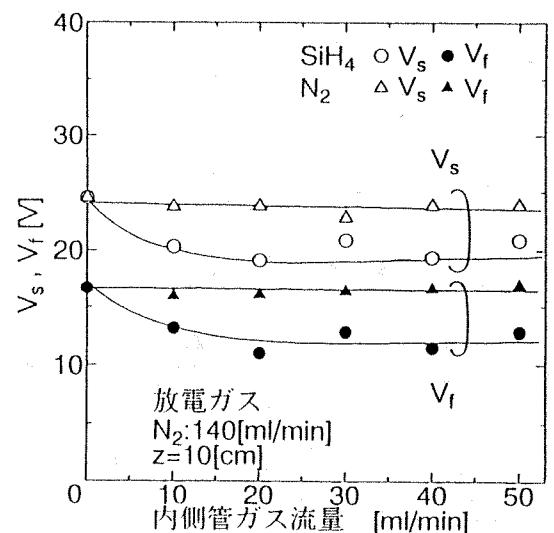
図11 空間電位・浮動電位の内側管ガス流量依存性 (b)  $z=10$  [cm]

Fig. 11 Dependence of Space Potential and Floating Potential on Gas Flow Rate of Inner Tube

$z > 10$  [cm]の空間では、図4、7の結果も合わせて考えると、内部的プラズマパラメータが $r$ 方向に均一となるので、均一なSiN膜が作製できると考えられる。さらに、図6の結果を考慮すると、基板位置を $z$ 方向に変化することにより、イオン衝撃エネルギーは変化させずに、電子密度のみを変化させて、すなわち衝撃を与えるイオンの数のみを変化させて成膜することが可能といえる。

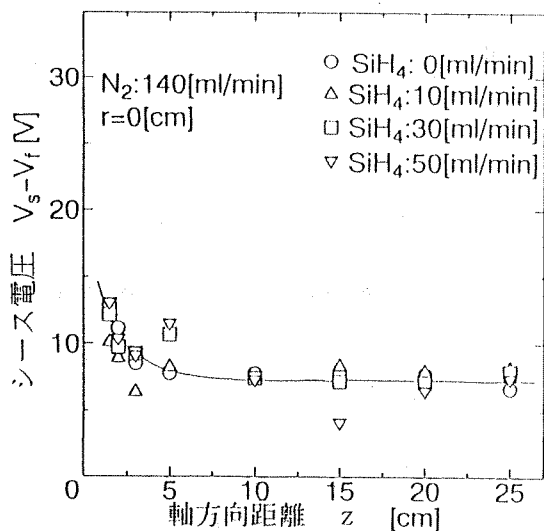


図 12 シース電圧の  $z$  依存性

Fig. 12 Dependence of Sheath Voltage on  $z$

## 5. まとめ

二重管式同軸線路形マイクロ波プラズマCVD装置の堆積室内における $N_2/SiH_4$ プラズマのプラズマパラメータを $SiH_4$ ガス流量を変化させて、シングルプローブ法により測定した。その結果、以下のことを明らかにした。

1. 電子温度は、 $z$ の増加に対して放電管端付近で急激に減少した後、 $z > 5$  [cm] でほぼ一定となる。また、 $r$ の増加に対しては、 $z = 3$  [cm] で緩やかに減少し、 $z = 10$  [cm] では一定となる。すなわち、 $z > 10$  [cm] では電子温度は空間的に均一であると考えてよいことが明らかとなった。

2. 電子温度は、 $SiH_4$ ガス流量の増加に対して、放電管端付近では減少するが、 $z > 5$  [cm] の空間では、ほとんど変化しない。これは、電子温度の高い放電管端付近では、 $SiH_4$ が解離されて電子の冷却効果が大いだが、電子温度の低い $z > 5$  [cm] の空間では、非弾性衝突周波数が減少し電子がほとんど冷却されなくなるためである。

3. 電子密度は、 $z$ の増加に対して放電管端付近で急激に減少した後、 $z > 5$  [cm] で指数関数的に減少する。また、電子密度は $r$ の増加に対して減少するが、 $z$ が増加するにしたがい、 $r$ 方向の均一性はよくなり、 $z > 10$  [cm] では $r$ 方向にほぼ均一となる。

4. 基板を絶縁したときのシース電圧 $V_s - V_f$ は、 $z > 10$  [cm] で空間的に一定となる。また、 $SiH_4$ ガス流量を変化させてもほとんど変化しない。すなわち、成膜中に膜に与えられるイオン衝撃エネルギーは、 $z > 10$  [cm]

では、 $SiH_4$ 流量によらず、かつ、空間的に一定であることが明らかになった。また、この時衝撃エネルギーは約7.5 [eV]であることを明らかにした。

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# RF バイアス印加同軸線路形マイクロ波プラズマ CVD による SiN 膜の低温作製

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Fabrication of SiN Films at Low Temperature Using RF Biased Coaxial-Line  
Type Microwave Plasma CVD

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あらまし イオン衝撃が SiN 膜の特性に及ぼす影響を検討することを目的とする。本研究では、イオン衝撃効果を検討するのに適している 2 重管式同軸線路形マイクロ波プラズマ CVD 装置を用い、基板に印加する RF バイアスを変化させて、基板に入射するイオン密度を一定にしてイオン衝撃エネルギーのみを変化させた。RF バイアスを増加させると、膜密度は増加し水素含有量は減少したが、ダングリングボンド密度は増加した。前者はイオン衝撃により成膜中の膜表面が加熱されるためであり、後者は  $N^+$  イオン衝撃により  $N^+$  イオンが膜中に打ち込まれ結合が切られるためである。また、基板温度を比較的低温である  $200^{\circ}\text{C}$  に上昇させて、かつ、RF バイアスを  $-175\text{ V}$  印加して成膜を行った結果、イオン衝撃による膜表面加熱と基板加熱の重畳効果により、膜密度が  $3\text{ g/cm}^3$ 、水素含有量が  $9\text{ at.}\%$  となった。更に、基板を  $200^{\circ}\text{C}$  に加熱することにより  $N^+$  イオン衝撃のイオン打込みによるダングリングボンド密度の増加を抑制できた。また、本  $N_2/\text{SiH}_4$  プラズマにおいて、室温で成膜した場合に、RF バイアスが  $-70\sim-80\text{ V}$  で膜表面温度が約  $200^{\circ}\text{C}$  となっていることを明らかにした。

キーワード マイクロ波プラズマ CVD, SiN 膜, RF バイアス, イオン衝撃効果, 膜表面加熱効果

## 1. ま え が き

窒化シリコン (SiN) 膜は、半導体デバイスの集積回路において、層間絶縁膜、ゲート絶縁膜、最終保護膜などに幅広く用いられており、その作製法には、熱 CVD 法、高周波プラズマ CVD 法、マイクロ波プラズマ CVD 法、電子サイクロトロン共鳴マイクロ波プラズマ CVD 法などがある。しかし、近年半導体デバイスプロセスにおいて薄膜の低温作製が要求されており、熱 CVD 法では  $900^{\circ}\text{C}$  と高温を必要とし、低温で薄膜を作製することができないことから、プラズマ CVD 法の研究が盛んに行われている。その中で、イオン衝撃下で成膜することにより低温で良質な膜が作製できるとの報告がなされている [1], [2]。しかしながら、イオン衝撃効果についての詳しい報告はない。これは、高周波プラズマ CVD 法では基板が放電プラズマ中に置かれており、イオン衝撃を変化させる (すなわち RF バイアスを変化させる) と電子温度、電子密度などの他

のプラズマパラメータも大きく変化してしまい、イオン衝撃効果について検討するには適さないこと、また電子サイクロトロン共鳴マイクロ波プラズマ CVD 法では、膜質が良くなる理由として、適度なイオン衝撃がもともとあるとしているので、イオン衝撃効果そのものを検討するには適さないためと考えられる。

一方、我々が研究開発を進めてきている 2 重管式同軸線路形マイクロ波プラズマ CVD 装置は、マイクロ波の波長が短いことを生かしてマイクロ波および放電プラズマを所定の空間に閉じ込めることができるので、基板をマイクロ波電力の注入のない、電子温度の低い空間的アフターグロープラズマ中に設置することができる [3], [4]。これにより、イオン衝撃がかなり少ない状態で成膜することができる [3], [5]~[7]。

本研究ではイオン衝撃が SiN 膜の特性に及ぼす影響について検討を行うことを目的とする。イオン衝撃効果は基板に流入するイオン密度と基板前面のシース電圧の積で表される。そこで本研究では、まずイオン密度を変化させないで、基板前面のシース電圧のみを変化させることが可能であることを示す。そして、シース電圧 (RF バイアス) のみを変化させることにより

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SiN 膜を作製し、SiN 膜作製時におけるイオン衝撃効果について検討することとした。なお、SiN 膜は絶縁膜であるので、直流バイアス法ではチャージアップが起こり、バイアスを印加したことになるので、RF バイアス法を用いた [8], [9]。なお、成膜中の基板温度は室温と 200°C とした。

## 2. 成膜装置および成膜条件

図 1 に成膜に用いた RF バイアス印加 2 重管式同軸線路形マイクロ波プラズマ CVD (MPCVD) 装置の概略図を示す。本装置は、2 重管式同軸線路形 MPCVD 装置に RF バイアス印加装置を取り付けたものである。まず、2 重管式同軸線路形 MPCVD 装置について説明する。放電管は 2 重管構造となっており、溶融石英製の外側放電管 (outer discharge tube) に純  $N_2$  ガスを流して、マイクロ波により電離させ窒素プラズマを生成する。そして、ステンレス製の内側管 (inner tube) を用いて  $SiH_4$  ガスを放電管端まで導き、窒素プラズマ中に混入することにより  $SiH_4$  ガスを解離させている。窒素およびシラン系ラジカルは堆積室 (deposition chamber) 内に輸送され、基板 (substrate) 上に SiN 膜を形成する。本装置ではマイクロ波は円筒キャビティ (cylindrical cavity) 内に閉じ込められているので、ここにマイクロ波電力が注入されている放電

プラズマが生じる。そして、堆積室内にはマイクロ波の電力注入のない空間的アフターグロープラズマを生成することができる [3], [4]。この空間的アフターグロープラズマ中に基板を設置することにより、イオン衝撃がかなり少ない状態で SiN 膜を作製することができる [3], [5]~[7]。2 重管式同軸線路形マイクロ波プラズマ CVD 装置の詳細は文献 [10] を参照して頂きたい。

次に、RF バイアス印加装置について説明する。周波数 21.0 MHz の高周波は、整合回路 (matching circuit) を通して、内直径 25.4 cm の堆積室内に導入され、堆積室とは電気的に絶縁してある大きさ 4.5 cm × 11.0 cm のステンレス製の基板テーブル (substrate table) に印加される。このように、RF バイアスを印加する基板テーブルを放電プラズマ領域外、すなわち空間的アフターグロープラズマ領域内に設置することにより、基板に高周波電力を印加しても、放電プラズマの状態を変化させずに基板に RF バイアスを印加することができる [8], [9]。RF バイアスとは、基板に高周波電力を印加したとき、基板に生じる自己バイアスである。基板テーブルの電位の測定には、整合回路の出力端に取り付けたオシロスコープ (oscilloscope) により行った。印加する高周波の周波数が低いとイオンが高周波に追従可能となるため、高周波電圧がイオン衝撃効果に影響する [11]。しかし、ここで用いた高周波の周波数は 21.0 MHz であり、イオンは高周波電界に追従できないために、イオンは RF バイアスのみによって膜表面で加速され膜表面に入射することになる。

次に、SiN 膜の作製条件を示す。マイクロ波電力を 270 W とした。 $N_2$  ガス流量および  $SiH_4$  ガス流量をそれぞれ 140 ml/min, 15 ml/min とした。このときの堆積室内のガス圧は 3.9 mTorr となった。基板位置は放電管端から 10 cm の位置に固定した。基板温度は室温と 200°C とした。基板加熱にはカーボンヒータ (carbon heater) を用いた。印加した高周波の電力を 0 W から約 70 W まで増加させることにより、基板電位を +4 V から -175 V まで変化できた。我々はこれまでに純窒素プラズマにおいて RF バイアスを変化させて、RF バイアスがプラズマに与える影響について電気単針法および発光分光分析を用いて検討を行ってきた。但し、実験条件は、 $SiH_4$  ガス流量を 0 ml/min とし、基板温度は室温で、他の条件は SiN 膜の作製条件と同じとした。その結果、RF バイアスを印加しても基板近傍 (放電管端から 9 cm 離れた点) で電気探針のイオン飽和

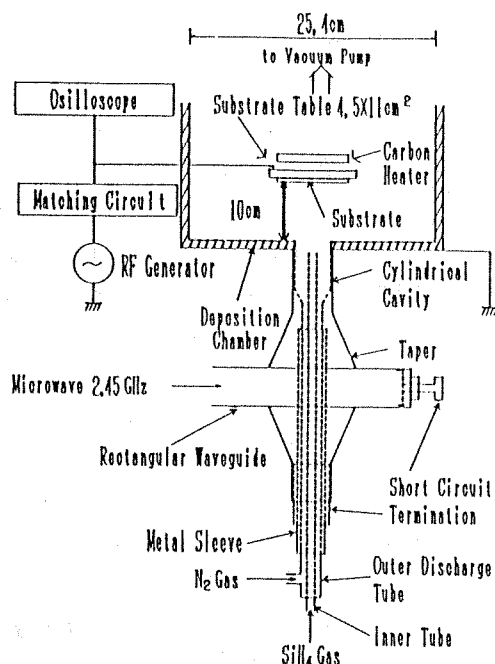


図 1 実験装置概略図  
Fig. 1 Schematic diagram of experiment system.

電流が変化していないことから、イオン密度、すなわち電子密度が RF バイアスを印加しても変化していないことを明らかにしてきた [12]。また、このことと基板近傍でラジカルの発光強度が RF バイアスを印加するとわずかに変化していることから、基板近傍で電子温度はわずかに増加するが、その増加割合は 4% 以下であるので、空間的アフターグロープラズマの状態は RF バイアスを印加してもほとんど変化していないことを明らかにしてきた [12]。N<sub>2</sub>/SiH<sub>4</sub> プラズマにおいても、同様と考えられる。すなわち、基板に RF バイアスを印加することにより、マイクロ波放電により生成された空間的アフターグロープラズマの状態をほぼ変化させずに、基板前面のシース電圧のみを変化させることができる。シース電圧とは基板前面のシース端でのプラズマ空間電位と基板電位との差であり、この電圧によりイオンが加速される。前述のように空間的アフターグロープラズマ中では、基板をフローにしたとき、シース電圧はかなり小さいと考えられるので、RF バイアスにより、イオンが加速されるものとして以後、検討を進めることにする。

膜厚測定には触針式膜厚計を用いた。屈折率測定には波長 632.8 nm の光源のエリプソメータを用いた。赤外吸収分光スペクトルと膜厚より、N-H 結合、Si-H 結合、Si-N 結合のストレッチングモードの積分吸収強度を求め、それぞれの赤外吸収強度に比例係数  $2.8 \times 10^{20} \text{ cm}^{-2}$  [13],  $1.4 \times 10^{20} \text{ cm}^{-2}$  [14],  $9.2 \times 10^{18} \text{ cm}^{-2}$  [15] を掛けることにより、N-H 結合の形で含まれる水素含有量、Si-H 結合の形で含まれる水素含有量、窒素含有量を求めた。全水素含有量は N-H 結合の形で含まれる水素含有量と Si-H 結合の形で含まれる水素含有量の和として求めた。電子スピン共鳴スペクトルと膜厚より、ダングリングボンド密度を求めた。屈折率と窒素含有量を用いて、Lorentz-Lorenz の関係式より Si/N 比、膜密度、Si 含有量を求めた [16], [17]。紫外可視吸収スペクトルと膜厚より、光学エネルギーギャップを求めた [18]。

### 3. 実験結果および考察

図 2 に堆積速度の RF バイアス依存性を示す。図から、堆積速度は RF バイアスを増加させると、いずれの基板温度においても減少することがわかる。これは、後述するが、イオン衝撃により、成膜中の膜表面が加熱され、膜がち密になったことと、膜がスパッタリングを受けたためである。また、基板温度を室温から

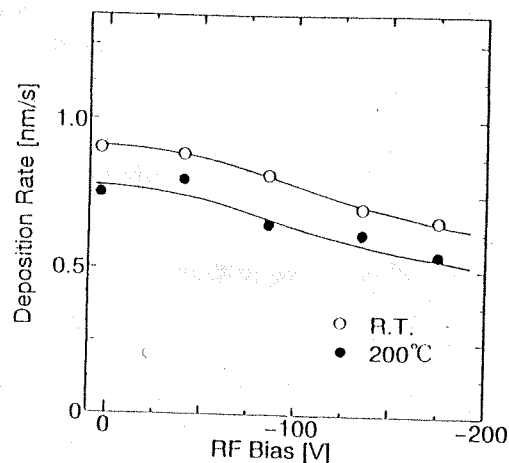


図 2 堆積速度の RF バイアス依存性  
Fig. 2 Dependence of deposition rate on RF bias.

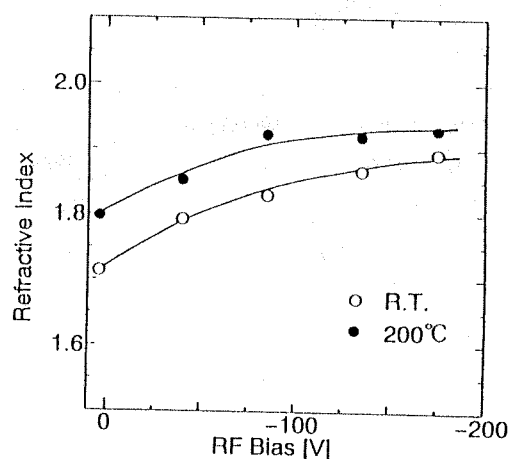


図 3 屈折率の RF バイアス依存性  
Fig. 3 Dependence of refractive index on RF bias.

200°C に上昇させると、膜表面反応が促進されて膜がよりち密になるので、堆積速度は減少する。

図 3 に屈折率の RF バイアス依存性を示す。図から、屈折率は RF バイアスを増加させると、いずれの基板温度においても増加することがわかる。また、基板温度を増加させると屈折率は増加する。これは、膜密度の増加が主な原因である。なお、基板温度を 200°C で RF バイアスを -175 V 印加すると、屈折率は熱 CVD 法で作製した膜の値 (2.0~2.1) [17] に近づくことがわかる。

図 4 に水素含有量の RF バイアス依存性を示す。図から、N-H 結合、Si-H 結合の形で含まれる水素含有量は RF バイアスを増加させると、いずれの基板温度においても減少することがわかる。RF バイアスを印加すると、膜表面に入射するイオンが加速され膜表面の原子と衝突して格子振動を起こして、膜表面が加熱

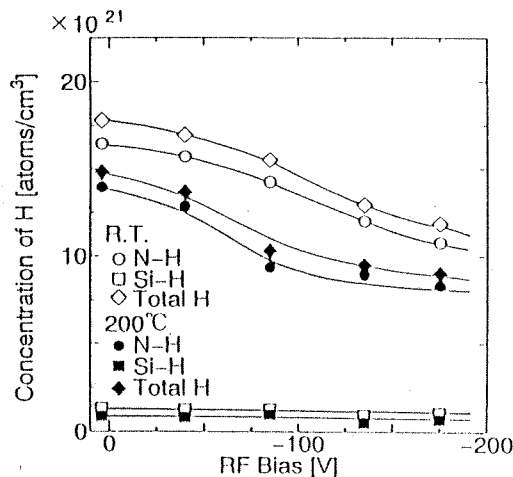


図 4 水素含有量の RF バイアス依存性  
Fig. 4 Dependence of concentration of H on RF bias.

される(膜表面加熱効果)。これにより、膜表面での反応が促進されるので、水素が脱離して、膜中に取り込まれる水素量は減少する。また、図から、基板温度を 200°C に加熱すると、更に膜の表面反応が促進され、N-H 結合、Si-H 結合の形で含まれる水素含有量は減少していることがわかる。また、基板温度を 200°C で RF バイアスを -175 V 印加すると、イオン衝撃による膜表面加熱と基板加熱の重畳効果により、膜中の全水素原子数は、膜の全原子数に対して 9% まで減少し、熱 CVD 法で作製した膜の値 (4~7%) [19] とほぼ同程度までに水素含有量を低減できることがわかる。

図 5 にダングリングボンド密度の RF バイアス依存性を示す。図から、RF バイアスを増加させるに従い、どの基板温度においてもダングリングボンド密度は増加することがわかる。RF バイアスを増加すると、膜の表面加熱により基板温度を上昇させたときと同様に、膜表面反応が促進されてダングリングボンド密度が減少するとも考えられるが、実際には増加した。これは窒素系イオンが膜表面に打ち込まれ結合が切られるためである [20]。マスマススペクトルメータによる分析によると、 $N_2^+$  イオンは  $N^+$  イオンの 14 倍あるが、膜に打ち込まれるのは質量の軽いほうの  $N^+$  イオンが主と考えられる(このことについては後に更に検討を加える)。また、図から、基板温度を 200°C に上昇させることにより、膜の表面反応が促進されダングリングボンド密度は減少していることがわかる。基板温度が室温で RF バイアスを増加させるとダングリングボンド密度が増加してしまっただが、基板温度を 200°C に上昇させることにより、イオン衝撃によるダングリングボン

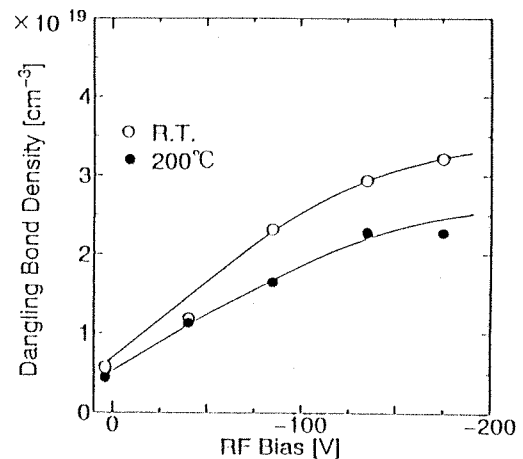


図 5 ダングリングボンド密度の RF バイアス依存性  
Fig. 5 Dependence of dangling bond density on RF bias.

ド密度の増加を抑制できることがわかる。しかしながら、熱 CVD 法で作製した膜のダングリングボンド密度は  $4 \times 10^{15} \sim 1 \times 10^{16} \text{ cm}^{-3}$  [21] 程度であり、本装置で作製した膜の値より小さい。また、いずれの基板温度においても RF バイアスを増加させると、ダングリングボンド密度は増加する。従って、ダングリングボンド密度の小さい膜を作製するには、イオン衝撃を避けて成膜する必要がある。

図 6 に窒素含有量、シリコン含有量の RF バイアス依存性を示す。図から、RF バイアスを増加させると、どの基板温度においても窒素含有量、シリコン含有量は増加することがわかる。これは、RF バイアスを増加させるに従い、基板温度を上昇させたときと同様な効果(膜表面加熱効果)が生じて、膜の表面反応が促進されて、ち密な膜となったためである。また、図から、基板温度を 200°C に加熱すると、膜の表面反応が更に促進され、室温の場合より窒素含有量、シリコン含有量が増加することがわかる。窒素含有量の増加割合はシリコン含有量の増加割合より大きい。マスマススペクトルメータによる分析によると窒素系イオンとシラン系イオンとはほぼ同量である。しかしながら、前述のように、質量の軽い  $N^+$  イオンは膜に打ち込まれて膜中に残るので、窒素含有量の増加割合が大きくなると考えられる。

また、本実験による窒素含有量、シリコン含有量が一番大きい基板温度が 200°C で RF バイアスを -175 V 印加して作製した膜を熱 CVD 法で作製した膜と比較すると、窒素含有量は  $5.7 \times 10^{22} \text{ atoms/cm}^3$  で熱 CVD 法で作製した膜の値 ( $5.3 \times 10^{22} \text{ atoms/cm}^3$ ) [21]

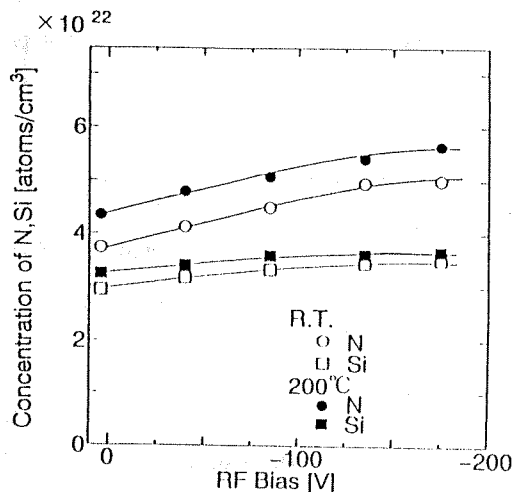


図 6 窒素含有量、シリコン含有量の RF バイアス依存性  
Fig. 6 Dependence of concentration of N and Si on RF bias.

より大きい。これは、イオン衝撃による  $N^+$  イオンの打込みによると考えられる。一方、シリコン含有量は  $3.7 \times 10^{22}$  atoms/cm<sup>3</sup> で熱 CVD 法で作製した膜の値 ( $4.0 \times 10^{22}$  atoms/cm<sup>3</sup>) [21] に近づいている。これは、イオン衝撃による膜表面加熱効果により膜が緻密化したためと考えられる。

図 7 に堆積速度とシリコン含有量の積の RF バイアス依存性を示す。図から、RF バイアスを増加させると堆積速度とシリコン含有量の積、すなわち単位時間単位面積当たりに膜となるシリコン原子数は、RF バイアスを増加させると減少することがわかる。これはイオン衝撃によりスパッタリングを生ずるためと考えられる。ここで、シラン系イオンが膜に衝突して Si をスパッタしたとしても、そのイオン中の Si が膜として残るので、結果的にスパッタリングは起きないことになる。しかしながら、ほぼ同質量の  $N_2^+$  イオンは Si のスパッタリングを生ずることになる。

図 8 に堆積速度と窒素含有量の積の RF バイアス依存性を示す。図から、RF バイアスを増加させても堆積速度と窒素含有量の積、すなわち、単位時間単位面積当たりに膜となる窒素の原子数は、RF バイアスを増加させてもほぼ一定であることがわかる。シリコンの原子の場合と同様に、単位時間単位面積当たりに膜となる窒素の原子数も、イオン衝撃によるスパッタリングにより減少するとも考えられるが、実際にはほぼ一定であった。これは、前述のように、窒素系イオン(主として  $N^+$  イオン) が膜中に打ち込まれる分だけ減少が抑えられることによると考えられる。すなわち、イ

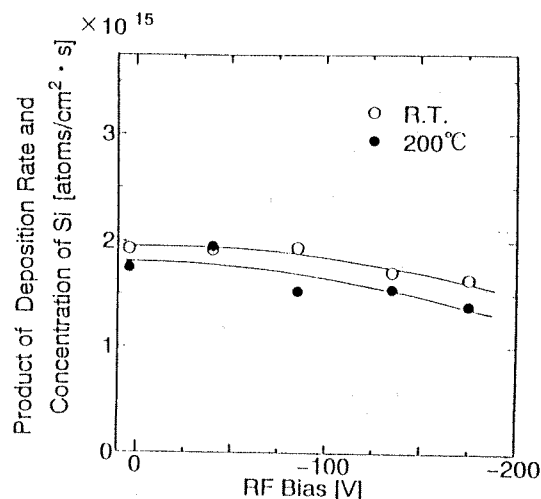


図 7 堆積速度とシリコン含有量の積の RF バイアス依存性  
Fig. 7 Dependence of product of deposition rate and concentration of Si on RF bias.

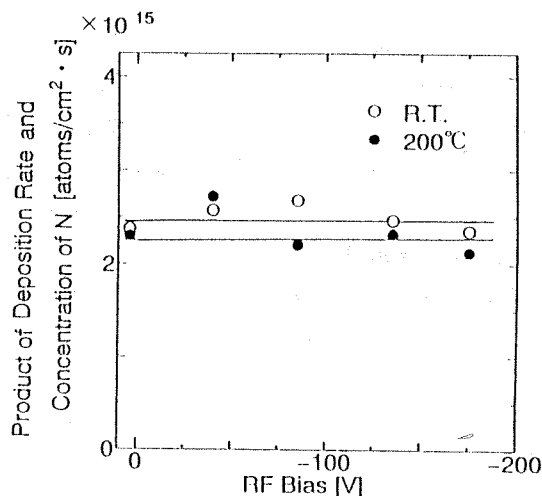


図 8 堆積速度と窒素含有量の積の RF バイアス依存性  
Fig. 8 Dependence of product of deposition rate and concentration of N on RF bias.

オンラジカルより中性ラジカルが多いことを考慮すると、シラン系イオンは膜表面加熱効果に寄与し、 $N_2^+$  イオンは膜表面加熱効果と Si のスパッタリングに寄与する。また、 $N^+$  イオンは膜中に打ち込まれ、膜の窒素含有量を増加する効果があるが、膜中の結合を切り、ダングリングボンド密度を増加させる効果もあることになる。

図 9 に Si/N 比の RF バイアス依存性を示す。図から、RF バイアスを増加させると、どの基板温度においても Si/N 比は減少することがわかる。これは、イオン衝撃により膜表面の温度が上昇したために薄膜形成に寄与するシラン系ラジカルと窒素系ラジカルの付着確

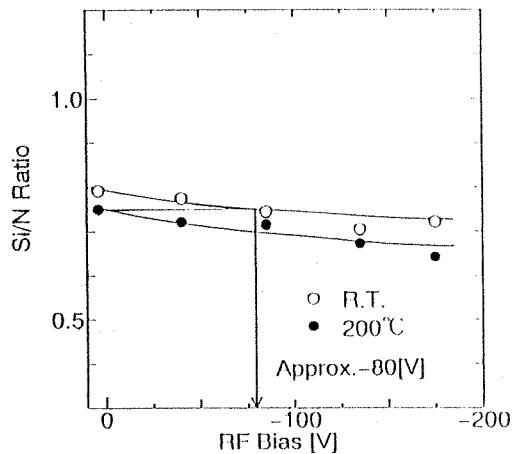


図 9 Si/N 比の RF バイアス依存性  
Fig. 9 Dependence of Si/N ratio on RF bias.

率の比が温度により変化したため [16] と、窒素系イオンがイオン衝撃により膜表面に、より多く打ち込まれるためである。また、図から、基板温度を上昇させると、Si/N 比は減少していることがわかる。これは薄膜形成に寄与するシラン系ラジカルと窒素系ラジカルの付着確率が温度により異なることを示すものである [16]。また、RF バイアス印加により、窒素リッチな膜となることが示されている。

基板温度が室温で RF バイアスが約 -80 V で作製した膜の Si/N 比と基板温度が 200°C で RF バイアスがほぼ 0 V で作製した膜の Si/N 比が一致することから、イオン衝撃による膜表面加熱効果により、基板温度が室温で RF バイアスが約 -80 V のとき、膜表面温度が約 200°C となっていると考えられる。

図 10 に膜密度の RF バイアス依存性を示す。図から、RF バイアスを増加させると、どの基板温度においても膜密度は増加することがわかる。これは、RF バイアスを増加させると、基板温度を上昇させたときと同様に成膜中の表面での構造緩和が促進されたためである。この膜密度の増加が、図 2 で堆積速度が RF バイアスの増加に対して減少した主な理由である。また、基板温度を 200°C にすると、更に膜の構造緩和が促進され、膜密度が増加する。基板温度が 200°C で RF バイアスがほぼ 0 V の場合の膜密度は、基板温度が室温で RF バイアスが約 -70 V の場合の膜密度と一致する。従って、この場合、RF バイアスが約 -70 V で、膜表面温度が約 200°C となっていると考えられる。図 9 における同様の考察では RF バイアスが約 -80 V で約 200°C になっているが、実験誤差を考えれば両者は良く一致しているといえる。イオン衝撃効果には膜表面加

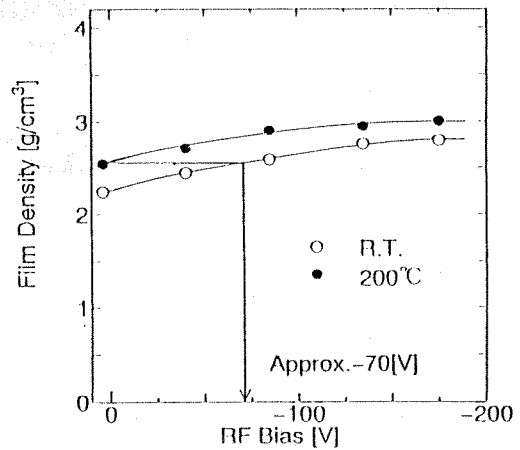


図 10 膜密度の RF バイアス依存性  
Fig. 10 Dependence of film density on RF bias.

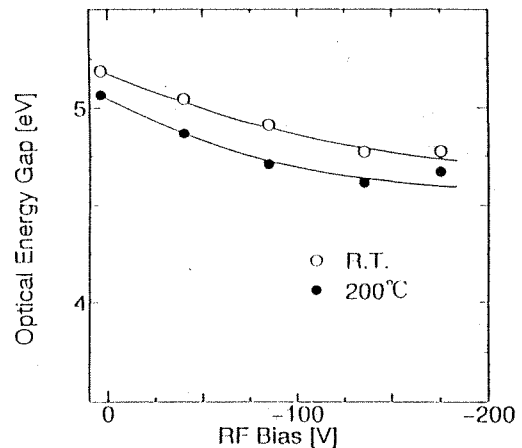


図 11 光学エネルギーギャップの RF バイアス依存性  
Fig. 11 Dependence of optical energy gap on RF bias.

熱効果ばかりでなく、イオン打込み効果、スパッタリング効果などがあるが、膜表面加熱効果について言えば、この場合 RF バイアスが -70 ~ -80 V で膜表面が約 200°C となっていると考えてよいことになる。

基板温度を 200°C で RF バイアスを -175 V 印加すると、イオン衝撃による膜表面加熱効果と基板加熱の効果が重畳するので、膜密度は 3.0 g/cm³ となり、非常に密な膜となっており、熱 CVD 法で作製した膜の膜密度 (2.8 ~ 3.1 g/cm³) [17] と同程度の値となることがわかる。

図 11 に光学エネルギーギャップの RF バイアス依存性を示す。図から、RF バイアスを増加させると、どの基板温度においても光学エネルギーギャップは減少することがわかる。また、基板温度を上昇させると光学エネルギーギャップは減少することがわかる。熱

CVD 法では光学エネルギーギャップは約 5.1 eV であり, 本装置で室温で成膜した場合とほぼ一致している。RF バイアスを印加すると最小で 4.7 eV とやや低下する。しかしながら, 電子サイクロトロン共鳴マイクロ波プラズマ CVD で成膜した場合 3 eV 程度のものもあり [22], 本実験における値の減少割合は小さいといえる。

#### 4. む す び

2 重管式同軸線路形マイクロ波プラズマ CVD 装置を用いて, 基板に RF バイアスを印加することにより基板に入射するイオン密度を一定にしてイオン衝撃エネルギー (RF バイアス) のみを変化させて, SiN 膜を作製して以下のことを明らかにした。

(1) RF バイアスを増加させることにより, 水素含有量は減少し, 膜密度は増加する。これは, イオン衝撃による膜表面加熱効果のためである。

(2) シラン系イオンは膜表面加熱効果に寄与し,  $N_2$  イオンは膜表面加熱効果と Si のスパッタリングに寄与する。また,  $N^+$  イオンは膜中に打ち込まれ, 窒素含有量を増加する効果があるが, 膜中の結合を切り, ダングリングボンド密度を増加させる効果もある。

(3) 基板温度を比較的低温である 200°C に上昇させて, かつ, RF バイアスを -175 V 印加することにより, 堆積速度 0.55 nm/s, 屈折率 1.93, 水素含有量 9 atomic%, 膜密度 3.0 g/cm<sup>3</sup> の膜が作製できた。

(4) 膜表面加熱効果はイオンの種類および密度によって変化するものであるが, 本  $N_2/SiH_4$  プラズマ (電子温度約 12,000 K, 電子密度約  $5 \times 10^{19}$  cm<sup>-3</sup>) [23] では, 基板を加熱しないで室温で成膜した場合に, RF バイアスが -70 ~ -80 V で膜表面温度が約 200°C となるという, 結果を得た。

今後, 窒素ガスとシランガス流量を変化させて, 同様な実験を行い, 最適条件を明らかにすると共に, 電子温度, 電子密度等の内部的プラズマパラメータの詳細な測定を行い, 堆積機構について検討を進める。また, 本 SiN 膜が半導体デバイス作製に適応できるかどうかを検討するため, 電気的特性も測定する予定である。

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## Dependence of Plasma Parameters on Electric Potential of Electrode in Microwave Plasma

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### SUMMARY

The authors have been studying the double-tubed coaxial line-type microwave plasma chemical vapor deposition (MPCVD). The discharge tube of the present MPCVD is a dual-tube structure made of a fused quartz outer discharge tube and stainless steel inner tube. The authors have discovered that the ion bombardment energy can be controlled without varying the electron densities and temperature by changing the potential of the substrate placed in a spatial after-glow plasma. In the present research, it is found that the ion bombardment energy can also be controlled by changing the potential of the inner tube placed in the discharge plasma. However, the electron densities and temperature have exhibited a tendency different from the one when the substrate potential is varied. Hence, a theoretical calculation has been carried out on the electron densities and temperature based on Maxwell-Boltzmann distribution. It is found that a different tendency can be explained from the fact that the electrons successively vanish on the deposition chamber wall from the higher-energy side as the plasma spatial potential is reduced from about 13 V to 4 V so that the electron velocity distribution is modified.

**Key words:** Substrate potential; inner tube potential; ion collision; plasma parameters; Maxwell-Boltzmann distribution.

### 1. Introduction

Hydrogenized amorphous silicon (a-Si:H) films are used as the electronic and photonic materials for thin-film transistors and solar cells. The plasma chemical vapor deposition (CVD) method often is used for fabrication of the a-Si:H film since the method can be used for a large surface area and is a low-temperature process. Although it is necessary to control the plasma in order to control the film quality, few studies on the plasma have been carried out. In the plasma CVD, the problem on the ion collision cannot be considered separately. We have developed a double-tube coaxial-line-type microwave plasma CVD (MPCVD) with which the film can be grown in a spatial after-glow plasma with less ion bombardments by trapping the discharge plasma in a specified region. They have been engaged in research on the ion bombardments [1-5]. In these studies, we have discovered that the ion bombardment energy can be controlled without changing the ion flux density incident on the substrate if the dc bias voltage applied to the substrate placed in the spatial after-glow plasma is varied [1].

In the present research, the plasma parameters are measured by varying the potential of the stainless inner tube placed in the discharge plasma in the MPCVD apparatus to find out if the ion bombardment energy can be controlled in the same way as varying the potential of the substrate placed in the spatial after-glow plasma. As

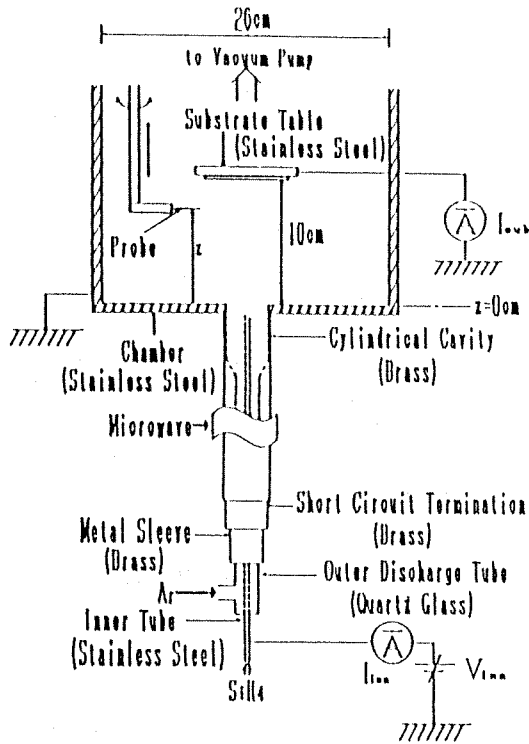


Fig. 1. Schematic diagram of experimental system.

a result, it is found that the ion bombardment energy can be controlled when the inner tube potential is varied. However, there is different tendency in the plasma parameters if the substrate potential is varied or if the inner tube potential is varied. Therefore, a theoretical study is carried out to find the reason for the difference.

## 2. Experiment

Figure 1 shows the schematic of the MPCVD equipment used in the experiment. The discharge section of the equipment is a dual-tube configuration made of a fused quartz outer discharge tube and a stainless inner tube. Ar gas flows in the outer discharge tube while  $\text{SiH}_4$  gas flows in the inner tube. The microwave at 2.45 GHz generated in a magnetron propagating in a rectangular waveguide is led to the metallic cylindrical cavity. In the cavity region, Ar gas is discharged by the microwave power.  $\text{SiH}_4$  gas is guided to the end of the discharge tube by the stainless inner tube and is mixed with Ar plasma where it collides with the particles of Ar plasma and is dissociated. In the present MPCVD equipment, the microwave power is confined within the cavity. Within the deposition chamber, a spatial after-glow plasma, in

which no microwave power is injected, is formed by the flow and diffusion. For the details of the present equipment, the readers are referred to [2], [3], and [4]. We have been carrying out research by changing the substrate potential with the inner tube and the deposition chamber wall grounded [1]. In the present research, however, the substrate and the deposition chamber wall are grounded and the inner tube potential is varied. Here, the inner tube potential is  $V_{inn}$ , the substrate potential is  $V_{sub}$ , the current flowing in the inner tube is  $I_{inn}$ , the current in the substrate is  $I_{sub}$ , and the distance along the axial direction from the end of the discharge tube is  $z$  (see Fig. 1).

The experimental conditions are described below. The microwave power is 150 W. The substrate is placed at  $z = 10$  cm. If  $V_{inn}$  exceeds  $\pm 40$  V, the glowing condition in the spatial after-glow plasma changes. Therefore, the dc discharge occurs between the inner tube and the deposition chamber wall and the power is injected into the plasma. Further, when  $V_{inn}$  exceeds  $-30$  V, the inner tube is sputtered by Ar ions and the metal atoms ejected from the stainless inner wall attach to the discharge tube so that the condition of the microwave discharge changes. Hence, in this research,  $V_{inn}$  was varied in the range between  $-30$  V and  $+40$  V where no dc discharge occurs and the inner tube is not sputtered. Then  $V_{sub}$  was 0 V. By means of the single-probe method, the measurement of the plasma parameters was carried out in the pure Ar plasma (Ar gas flow: 110 ml/min) and in the Ar/ $\text{SiH}_4$  plasma under the conditions identical to the time of fabrication of the a-Si:H film (Ar gas flow: 110 ml/min,  $\text{SiH}_4$  gas flow: 30 ml/min). A cylindrical probe with a diameter of 0.05 cm and a length of 0.3 cm was used. The measurement was carried out at the locations of  $z = 3, 5, 7$ , and  $9$  along the center axis of the deposition chamber.

The probe measurement in Ar/ $\text{SiH}_4$  plasma which is a reactive plasma cannot be carried out in a usual way because a film deposits on the surface of the probe. We have established the probe measurement method that can also be carried out in Ar/ $\text{SiH}_4$  plasma [5]. In the present research, this method is used for measurement in Ar/ $\text{SiH}_4$  plasma.

In this paper, the  $V_{sub}$  dependence of the electron density, electron temperature, plasma spatial potential, and  $I_{sub}$  was measured again in order to test repeatability. The results agreed well with those reported earlier. Also, the  $V_{sub}$  dependence of  $I_{inn}$  was not measured previously but was measured here for the first time.

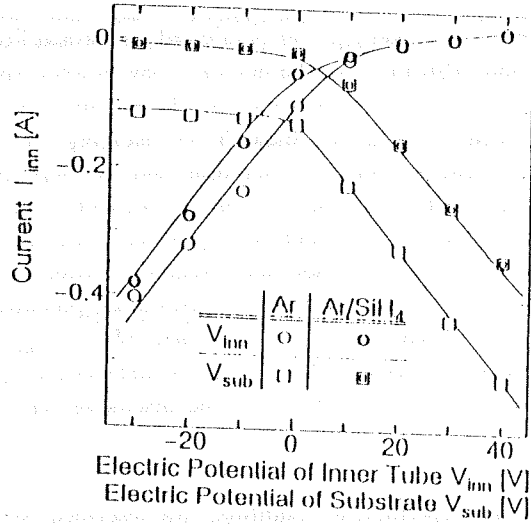


Fig. 2. Dependence of  $I_{inn}$  on  $V_{inn}$  and  $V_{sub}$ .

### 3. Results and Discussions

Figure 2 shows the  $V_{sub}$  dependence and  $V_{inn}$  dependence of  $I_{inn}$ . The electron current is taken positive. From the figure, it is found that  $I_{inn}$  changes little in the negative region of a varying  $V_{sub}$  and that it decreases rapidly in the positive region of  $V_{sub}$ . The reason why  $I_{inn}$  does not change in the negative region of  $V_{sub}$  is that the sheath voltage of the inner tube surface does not change. The reason why  $I_{inn}$  decreases rapidly in the positive region of  $V_{sub}$  is that the sheath voltage of the inner tube surface increases rapidly. On the other hand, when  $V_{inn}$  is varied,  $I_{inn}$  increases rapidly and then is saturated for an increasing  $V_{inn}$ . The reason why  $I_{inn}$  increases rapidly is that the sheath voltage of the inner tube surface decreases rapidly and  $I_{inn}$  is saturated because the variation of the sheath voltage of the inner tube surface decreases. From the figure, it is found that the  $V_{sub}$  dependence and the  $V_{inn}$  dependence of  $I_{inn}$  are almost symmetric.

Next, let us discuss the reason why  $I_{inn}$  increases in both cases as  $\text{SiH}_4$  gas is mixed. First, it is clear from the schematic of the equipment in Fig. 1 that the surface area of the inner tube is smaller than those of the inner wall of the deposition chamber and of the substrate table. The gas flow is upward in Fig. 1 as is the Ar plasma. When  $\text{SiH}_4$  gas is mixed, Ar ions are used for the dissociation of  $\text{SiH}_4$  and are decreased due to the charged transfer. As a result, the silan ions and hydrogen ions are increased. These ions, which are lighter in weight than the Ar ions, are carried upward by the gas flow and at

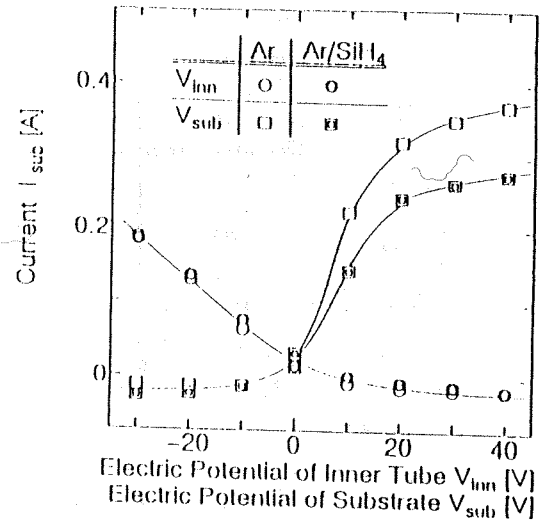


Fig. 3. Dependence of  $I_{sub}$  on  $V_{inn}$  and  $V_{sub}$ .

the same time are more likely to reach the inner wall of the deposition chamber and the substrate table by diffusion. Hence, the ion current in the inner tube is decreased while  $I_{inn}$  increases. However, if  $V_{inn}$  is varied to exceed about 15 V, the results with a mixed  $\text{SiH}_4$  gas coincide with those without it. This is because the ion current decreases so that the electron current is dominant, which does not depend on the type of ions.

Figure 3 shows the  $V_{sub}$  dependence and the  $V_{inn}$  dependence of  $I_{sub}$ . Similar to the case in Fig. 2, the electron current is positive in Fig. 3. As  $V_{sub}$  is increased,  $I_{sub}$  increases slowly for  $V_{sub}$  of less than -10 V while it increases rapidly in the region between -10 V and 20 V and then is saturated. On the other hand, when  $V_{inn}$  is increased  $I_{sub}$  decreases rapidly and then is constant. From the figure, it is found that the  $V_{sub}$  dependence and the  $V_{inn}$  dependence of  $I_{sub}$  are almost symmetric.

From Figs. 2 and 3, it is found that the ion bombardment energy can be controlled by varying the inner tube potential ( $V_{inn}$ ) as well as by that of the substrate potential ( $V_{sub}$ ).

Next, the results of the probe measurement are shown. Figure 4 depicts the  $V_{sub}$  dependence and the  $V_{inn}$  dependence of the plasma spatial potential ( $V_s$ ) at  $z = 3$  cm. When  $V_{sub}$  is increased,  $V_s$  increases slightly in the negative region of  $V_{sub}$  and increases rapidly in the positive region of  $V_{sub}$ . On the other hand,  $V_s$  increases rapidly if  $V_{inn}$  is increased. Similar results are obtained at other measurement locations.

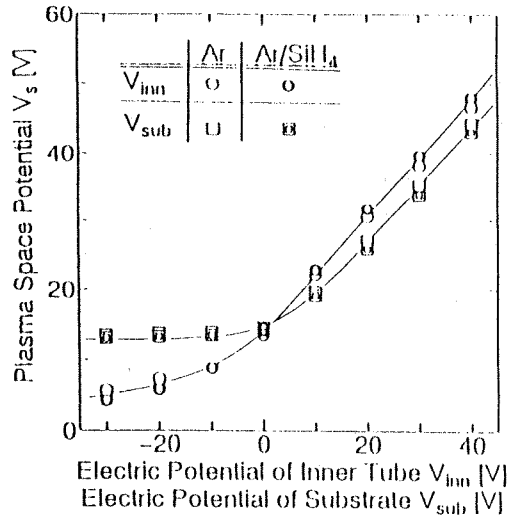


Fig. 4. Dependence of  $V_s$  on  $V_{inn}$  and  $V_{sub}$ .

When  $V_{sub}$  is negative, the decreasing gradient of  $V_s$  becomes smaller and the decrease is only up to about 13 V. On the other hand, if  $V_{inn}$  is negative,  $V_s$  continues decreasing up to about 4 V. This is because the inner tube is placed in the discharge plasma with high electron density and temperature so that  $V_{inn}$  affects  $V_s$  strongly, whereas the substrate is in the spatial after-glow plasma in which the electron density and temperature are low.

The sheath voltage ( $V_{sh, sub}$ ) on the surface of the substrate can be obtained by taking the difference between  $V_s$  and  $V_{sub}$  at the edge of the sheath. Since the sheath thickness is several millimeters, it is necessary to carry out the measurement at a location several millimeters from the substrate. However, since the gradient of  $V_s$  in the  $z$  direction is small, the value of  $V_s$  at the sheath edge can be approximated by the value of  $V_s$  at  $z = 9$  cm [1]. Hence, by taking the difference between  $V_s$  and  $V_{sub}$  at  $z = 9$  cm,  $V_{sh, sub}$  is derived. Figure 5 shows the results. Since  $V_{sub}$  is 0 V, the  $V_{inn}$  dependence of  $V_{sh, sub}$  is identical to the  $V_{inn}$  dependence of  $V_s$ . From the figure, it is found that  $V_{sh, sub}$  decreases as  $V_{sub}$  is increased. This result indicates that the ion bombardment energy decreases as  $V_{sub}$  is increased. On the other hand,  $V_{sh, sub}$  decreases as  $V_{inn}$  is decreased. This result indicates that the ion bombardment energy decreases as  $V_{inn}$  is decreased. From the above results, it is found that the ion bombardment energy can be controlled by changing  $V_{inn}$ .

The ion bombardment energy can be reduced to about 3 eV when  $V_{inn}$  is -30 V. When  $V_{sub}$  is +40 V,

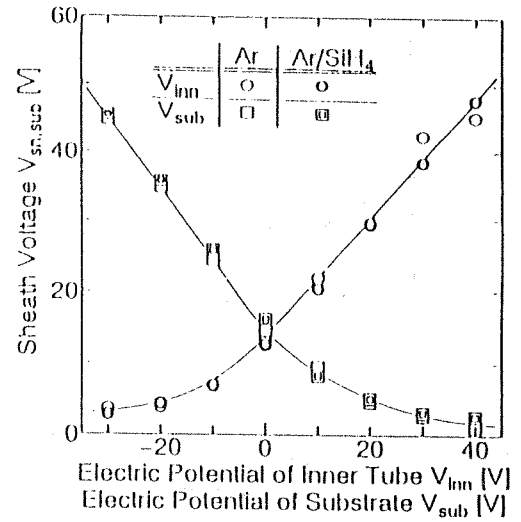


Fig. 5. Dependence of  $V_{sh, sub}$  on  $V_{inn}$  and  $V_{sub}$ .

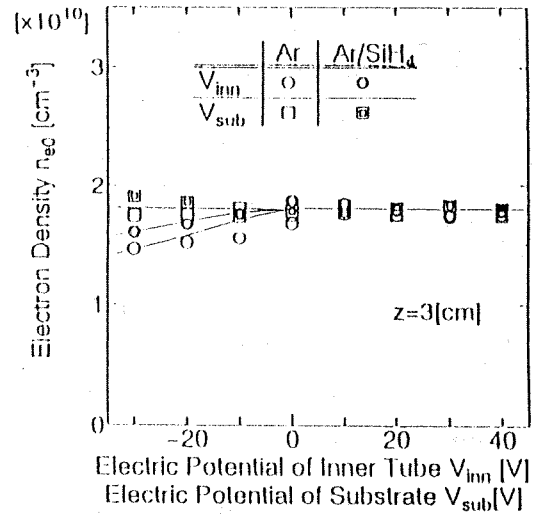


Fig. 6. Dependence of  $n_{co}$  on  $V_{inn}$  and  $V_{sub}$ .

the ion bombardment energy can be reduced to about 3 eV. However, the electric field that can repel the ions cannot be formed by varying  $V_{sub}$  or  $V_{inn}$ .

Figure 6 shows the  $V_{sub}$  dependence and the  $V_{inn}$  dependence of the electron density ( $n_{co}$ ) at  $z = 3$  cm. It is found from the figure that  $n_{co}$  does not change with  $V_{sub}$ . On the other hand, if  $V_{inn}$  is varied,  $n_{co}$  increases slightly as  $V_{inn}$  approaches 0 V from a negative value. There is no change for a positive  $V_{inn}$ . Similar results are obtained at other measurement locations.

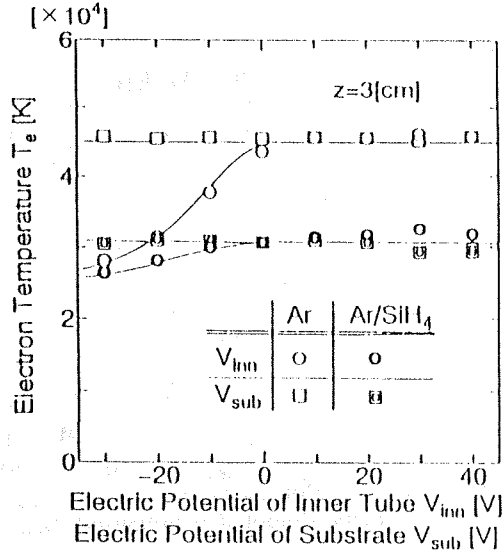


Fig. 7. Dependence of  $T_e$  on  $V_{inn}$  and  $V_{sub}$ .

Figure 7 shows the  $V_{sub}$  dependence and the  $V_{inn}$  dependence of the electron temperature ( $T_e$ ) at  $z = 3$  cm. From the figure, it is found that  $T_e$  does not change as  $V_{sub}$  is varied. On the other hand, if  $V_{inn}$  is varied,  $T_e$  increases as  $V_{inn}$  approaches 0 V from a negative value. No change is observed for a positive value of  $V_{inn}$ . The results are similar at other measurement locations.

It is found also from the figure that  $T_e$  of Ar/SiH<sub>4</sub> plasma is lower than  $T_e$  of the pure Ar plasma. This is due to the increases of nonelastic collision, the dissociation of SiH<sub>4</sub> because Ar/SiH<sub>4</sub> plasma is generated mixing Ar plasma with SiH<sub>4</sub> [5].

In the foregoing, it became clear that the potential ( $V_{inn}$ ) of the electrode in the discharge plasma and the potential ( $V_{sub}$ ) of the electrode in the spatial after-glow plasma have similar effects on  $V_s$ . On the other hand, it was found experimentally that  $n_{e0}$  and  $T_e$  do not change when  $V_{sub}$  is varied while they decrease as  $V_{inn}$  is increased in the negative direction in the negative region. The reason for the different tendencies will be discussed.

The velocity distribution of the electrons is, in general, Maxwell-Boltzmann:

$$n_e(v) = 4\pi n_{e0} \left( \frac{m_e}{2\pi k T_e} \right)^{3/2} v^2 \exp\left( -\frac{m_e v^2}{2k T_e} \right) \quad (1)$$

where  $k$  is Boltzmann's constant,  $m_e$  is the electron mass,  $T_e$  is the electron temperature,  $v$  is the electron velocity,

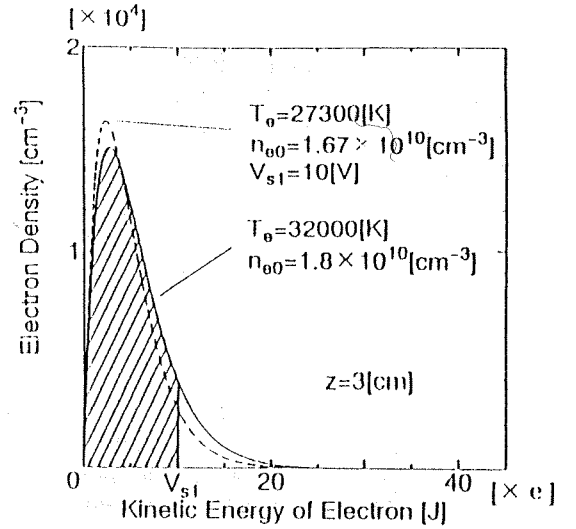


Fig. 8. Maxwell-Boltzmann's distribution.

$n_{e0}$  is the total electron density, and  $n_e(v)$  is the density of the electrons with a velocity of  $v$ . Since

$$\frac{1}{2} m_e v^2 = eV \quad (2)$$

Eq. (1) becomes

$$n_e(V) = 8\pi n_{e0} \left( \frac{m_e}{2\pi k T_e} \right)^{3/2} \frac{eV}{m_e} \exp\left( -\frac{eV}{k T_e} \right) \quad (3)$$

where  $e$  is the elementary charge and  $V$  is the voltage. If the sheath voltage or  $V_s$  of the wall surface of the deposition chamber is sufficiently large, most of the electrons are repelled back at the wall. As  $V_s$  is decreased, the electrons following Maxwell-Boltzmann distribution reach the wall of the deposition chamber successively in the order of higher-electron energy and vanish by recombination with ions at the wall surface.

The solid line in Fig. 8 is the velocity distribution of the electrons obtained by substitution of the experimental data of  $n_{e0}$  and  $T_e$  to Eq. (3) when  $V_s$  is sufficiently large ( $V_{inn} > 0$ ). The values at  $z = 3$  cm were used as the experimental data. Next, when  $V_s$  is decreased and is  $V_{s1}$  in the figure, the electrons with kinetic energy of less than  $eV_{s1}$  are repelled by the sheath voltage whereas other electrons with a larger kinetic energy can be separated from the sheath voltage and vanish at the wall of the deposition chamber. Hence, the electron density  $n'_{e0}$  when  $V_s$  is  $V_{s1}$  is the integration of the hatched region in Fig. 8 and is given by

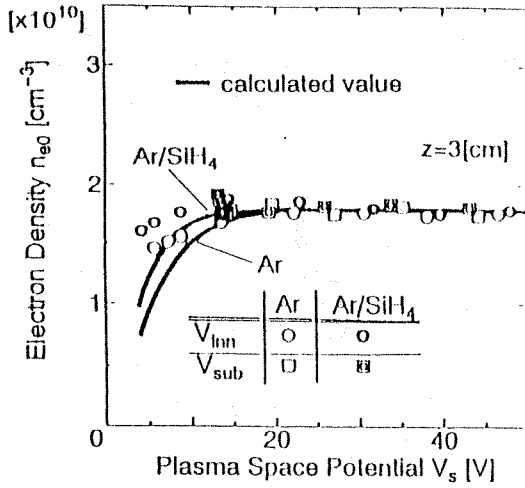


Fig. 9. Comparison of calculated values with experimental values of  $n_{e0}$ .

$$n'_{e0} = \int_0^{V_{s1}} n_e(V) dV \quad (4)$$

The electron group with the distribution of the hatched region in Fig. 8 is diffused while colliding with other particles and then becomes another Maxwell-Boltzmann distribution indicated by the dotted line in Fig. 8. Let  $T_e$  be the electron temperature of the redistribution. Then,  $n_e(V)'$  is given by

$$n_e(V)' = 8\pi n'_{e0} \left( \frac{m_e}{2\pi k T_e} \right)^{3/2} \frac{eV}{m_e} \exp\left( -\frac{eV}{k T_e} \right) \quad (5)$$

Then, the energy of the total electrons in the plasma is preserved. Hence,

$$\int_0^{V_{s1}} n_e(V) eV dV = \int_0^{\infty} n_e(V)' eV dV \quad (6)$$

holds. By solving Eq. (5) and Eq. (6) simultaneously,  $T_e$  can be obtained as a first-order approximation.

Figure 9 shows the comparison of the electron density derived from Eq. (4) with the experimental data. On the other hand, Fig. 10 shows the electron temperature derived by solving Eq. (5) and Eq. (6) simultaneously, compared with the experimental data. In both figures, it is found that the experimental findings that  $n_{e0}$  and  $T_e$  become small if  $V_s$  is small ( $V_{inn} < 0$ ) can be explained by the theory described above.

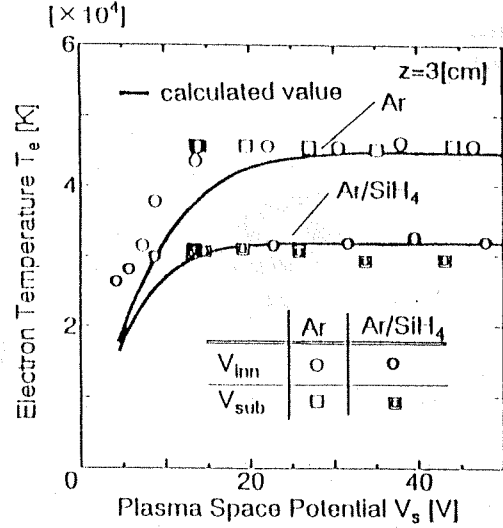


Fig. 10. Comparison of calculated values with experimental values of  $T_e$ .

In Figs. 9 and 10, the numerical and experimental results have the identical tendencies that  $n_{e0}$  and  $T_e$  decrease as  $V_s$  is decreased. The results of the theoretical calculations indicate that the reduction is larger. The reaction described above takes place only at the wall surface of the deposition chamber but not in the entire space of the deposition chamber. In the theoretical calculations, however, the calculation was under the assumption that the high-energy electrons in the entire space arrive at the wall of the deposition chamber where it then vanishes. Therefore, the numerical results are smaller than the experimental results. From the above results, when  $V_{sub}$  is varied, there is little change in  $n_{e0}$  and  $T_e$ . This is because  $V_s$  decreases only up to about 13 V with a negative value of  $V_{sub}$  (as shown in Fig. 4) and the extinction of the electrons at the wall of the deposition chamber is negligible so that the velocity distribution of the electrons does not change. On the other hand, if  $V_{inn}$  is varied,  $n_{e0}$  and  $T_e$  vary. This is because  $V_s$  decreases to about 4 V as  $V_{inn}$  is negative (as shown in Fig. 4) and the electrons on the higher-energy side vanish by a large amount so that the electron density decreases and the electron temperature is reduced.

#### 4. Conclusions

In a double-tubed coaxial-line microwave plasma CVD system, the plasma parameters were measured while the substrate potential ( $V_{sub}$ ) and the inner tube

potential ( $V_{inn}$ ) are varied. The following results can be reported.

(1) The plasma spatial potential ( $V_s$ ) increases slightly as  $V_{sub}$  is increased with a negative value and increases suddenly when  $V_{sub}$  is positive. When  $V_{inn}$  is increased,  $V_s$  increases rapidly. When  $V_{sub}$  is varied in the negative region,  $V_s$  decreases only to about 13 V. If  $V_{inn}$  is varied in the negative region,  $V_s$  decreases to about 4 V.

(2) When  $V_{sub}$  is increased, the ion bombardment energy can be reduced. When  $V_{inn}$  is decreased, the ion bombardment energy can be reduced.

(3) When  $V_{sub}$  is varied, the electron density ( $n_{e0}$ ) and the electron temperature ( $T_e$ ) do not change. If  $V_{inn}$  is increased in the negative direction,  $n_{e0}$  and  $T_e$  decrease.

(4) The variations of  $n_{e0}$  and  $T_e$  in item (3) can be explained from the fact that, if  $V_s$  is decreased, the electron density decreases due to extinction of the electrons with higher energy in Maxwell-Boltzmann distribution successively on the wall of the deposition chamber so that the average energy of the total electrons in the plasma decreases.

(5) As a method to control the ion bombardment energy, the one varying the substrate potential generally is used. When the substrate is grounded, or the substrate

happens to be grounded, the ion bombardment energy can still be controlled by varying the potential of another electrode (inner tube) in the microwave plasma.

$V_{sub}$  is varied in the fabrication of the a-Si:H film and in future  $V_{inn}$  will be varied in the fabrication for comparison.

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## Optical Energy Gap Measurement of Semiconductor Ultrathin Films Using Optical Waveguides

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Measurement of the optical energy gap ( $E_g$ ) using a slab optical waveguide (SOW) has been studied. With increasing hydrogenated amorphous silicon ( $a$ -Si:H) film thickness, transmittance was found to decrease with periodic oscillation. It has been clarified that the oscillation is caused by the change of the field strength distribution of a guided mode in  $a$ -Si:H according to the increase of  $a$ -Si:H film thickness, using the four-layer structure SOW simulation. By removing the oscillation due to the dependence of transmittance on  $a$ -Si:H film thickness, the influence of the oscillation on the values of  $E_g$  can be eliminated. As a result, it has been demonstrated that  $E_g$  of  $a$ -Si:H with thickness on the order of  $1/40$  that of samples used in the conventional method can be measured. It has been clarified that sufficient absorption to determine  $E_g$  of  $a$ -Si:H ultrathin films is obtained because the sensitivity of the sensor is increased by changing the size of the SOW.

KEYWORDS: interference fringe, ultrathin film, optical energy gap, band gap, slab optical waveguide,  $a$ -Si:H

### 1. Introduction

The optical energy gap ( $E_g$ ) is used as one of the factors in the evaluation of semiconductors.  $E_g$  is obtained from the dependence of transmittance on the wavelength for semiconductor films, by ultraviolet-visible spectroscopy. In conventional methods of measurement, a transmitted spectrum is obtained by irradiating ultraviolet-visible light perpendicularly onto a film surface. The spectrum is a curve with interference fringes due to multiple reflection between boundaries of the semiconductor. The fringes are removed by interpolating a curve which goes through the center of the fringes. Using the resultant spectrum without fringes,  $E_g$  is obtained using an expression in which  $E_g$  is proportional to the square root of the absorption coefficient.<sup>1,2)</sup> In these methods, when films are sufficiently thick, it is easy to determine the curve which goes through the center of the fringes because there are many fringes and their amplitude is small. Absorption by the semiconductor is high, so that error in the determination of  $E_g$  is low. On the other hand, when films are thin, it is difficult to determine the curve which goes through the center of the fringes because there are few fringes and their amplitude is high. The absorption is also low. Consequently, error in the determination of  $E_g$  becomes appreciable. Therefore, the conventional methods require thick semiconductor films of approximately  $1\mu\text{m}$ .<sup>3)</sup>

We have developed a measurement method for  $E_g$  of ultrathin hydrogenated amorphous silicon ( $a$ -Si:H) semiconductor film, using an optical fiber where the clad of a middle section is removed.<sup>4)</sup> In this method, the  $a$ -Si:H film is deposited on the core of the optical fiber section without the clad. In this region, some of the guided light is absorbed by the  $a$ -Si:H film. It has been found that even if the semiconductor film is thin, absorption sufficient to determine  $E_g$  can be obtained by increasing the length of the part from which the clad is removed (the bare part of the core). However, a problem that the semiconductor film is deposited nonuniformly on the core of the optical fiber arises in this method.

Based on the above, we devised a new measurement method in which a slab optical waveguide (SOW) is used as a sensor instead of the clad-removed optical fiber. By depositing the semiconductor only on the surface of the SOW sensor, the problem of nonuniform deposition of semiconductor film is overcome.

First, the experimental results show that with increasing  $a$ -Si:H film thickness, transmittance decreases with oscillation. This phenomenon is analyzed by simulation of the four-layer structure SOW of air,  $a$ -Si:H, optical waveguide and air. The absorption coefficient of the four-layer SOW was found to peak periodically since the electric field strength distribution of a guided mode around the  $a$ -Si:H layer becomes maximum according to the  $a$ -Si:H film thickness.

Next, two curves, one of which is an exponential curve which goes through each maximum oscillation in the dependence of transmittance on the deposited  $a$ -Si:H film thickness and the other of which is an exponential curve which goes through each minimum, are determined in order to remove the oscillation. The method for obtaining the exponential function without the oscillation, which is the arithmetic mean of the above two curves and goes through the point at which transmittance is 1 with deposited film thickness of 0 nm, is described. Using this method,  $E_g$  of ultrathin films can be determined in a range of thickness which could not be measured by conventional methods.

Finally, the dependences of  $E_g$  on the width of the part on which the  $a$ -Si:H film is deposited, the length, and the thickness of the optical waveguide are discussed based on results of experiments in which each of the parameters of the SOW sensor are changed.

### 2. Experimental Conditions and the SOW Sensor

Figure 1 shows our experimental setup. The chamber of the microwave plasma chemical vapor deposition (MPCVD) system is shown.  $a$ -Si:H is fabricated using Ar and  $\text{SiH}_4$  plasma flowing from the left-hand side of the system. The SOW sensor is set at the position of the substrate to be fabricated in this chamber. Guided white

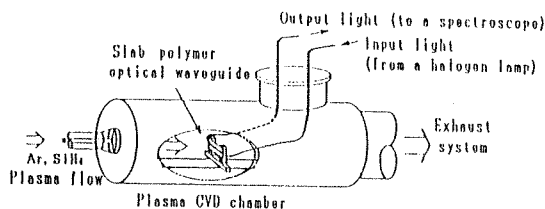


Fig. 1. Experimental setup.

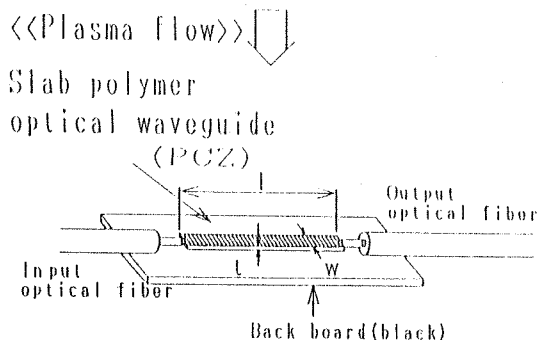


Fig. 2. Details of the slab optical waveguide (SOW) sensor.

light is irradiated, and during the deposition, absorption spectra which change continuously are measured.

Figure 2 shows the SOW sensor. The material of SOW is bisphenol Z polycarbonate (PCZ).<sup>5)</sup> The width of the part of the SOW sensor on which film is deposited is defined as  $w$  mm, its length is defined as  $l$  mm, and the thickness of SOW is defined as  $t$   $\mu$ m. The step index optical fibers with the 400  $\mu$ m silica core and the polymer clad are attached to the two ends of the SOW sensor to guide input and output beams. An acrylic resin board is used as the back board to prevent deposition of semiconductor films onto the back of SOW. The color of the board is black in order to reduce the amount of stray light guided through the board. Although this is not shown in Fig. 2, the joints between SOW and optical fibers, and the two remaining sides of SOW are covered with foil to prevent deposition of semiconductor films. A halogen lamp is used as a light source.

### 3. Experiment

To fabricate  $a$ -Si:H, the double-tubed coaxial-line-type MPCVD system has been used.<sup>6)</sup> In the chamber, the intensity of the ultraviolet-visible spectrum from 500 to 800 nm through the optical waveguide system is first measured before the semiconductor is deposited on the SOW sensor. Second,  $a$ -Si:H film is fabricated on the SOW sensor. The intensities of the ultraviolet-visible spectrum are measured at fixed time intervals. During the measurement, the film thickness does not change, because the intensity is measured quickly at approximately 0.5 s per scan while the deposition rate of  $a$ -Si:H is very low at approximately 0.05 nm/s. Third, transmittance spectra are obtained from the ratio of the spectrum intensity before the deposition to those measured for each film thickness. Finally, from the transmittance spectra, the dependence of  $(\alpha h\nu)^{1/2}$  (where  $\alpha$  is the absorption

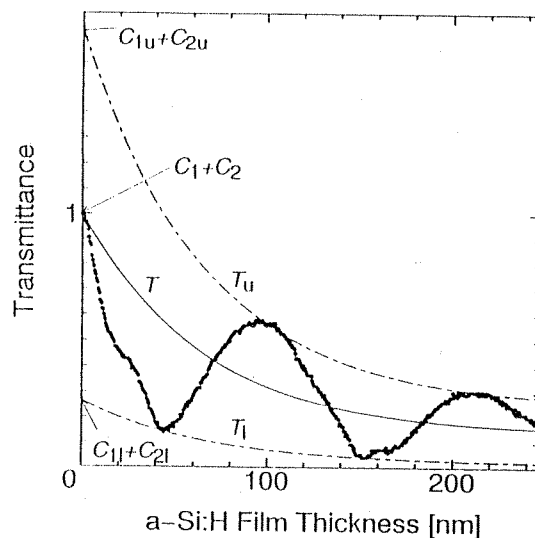


Fig. 3. Dependence of transmittance on the  $a$ -Si:H film thickness. •: experimental values; upper broken line  $T_u$ : upper transmittance through the maxima; lower broken line  $T_l$ : lower transmittance through the minima; solid line  $T$ : transmittance without oscillation.

coefficient,  $h$  is Planck's constant and  $\nu$  is frequency) is obtained.<sup>7)</sup> Then,  $E_o$  is determined from the linearity part of the curve which is expressed as

$$(\alpha h\nu)^{1/2} = B(h\nu - E_o), \quad (1)$$

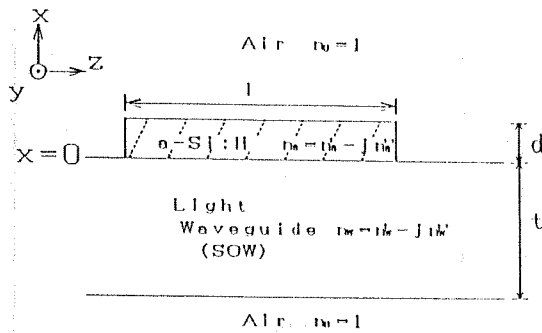
where  $B$  is a constant.

The thickness of the  $a$ -Si:H film on the SOW sensor is determined in the following manner. At the time of fabrication, a glass substrate and crystal-oscillation-type thickness monitor are placed close to the SOW sensor. During the fabrication, the  $a$ -Si:H film thickness is measured, and the change of the deposition rate is recorded. After the fabrication, the  $a$ -Si:H film thickness on the glass substrate is measured with a needle-tactile-type thickness meter. The results measured using the thickness monitor are corrected relative to the  $a$ -Si:H film thickness on the glass substrate. Then, the film thickness at each measurement of the transmittance spectrum is determined.

### 4. Oscillation in the Dependence of Transmittance on the Film Thickness

An example of the measured result is shown in Fig. 3. The plot of the experimental values (•) reveals the dependence of transmittance on the  $a$ -Si:H film thickness obtained using the SOW sensor with  $l = 50$  mm,  $t = 78$   $\mu$ m and  $w = 0.8$  mm at the wavelength of 632.8 nm. In Fig. 3, with increasing  $a$ -Si:H film thickness, transmittance decreases exponentially with oscillation.

The reason for the oscillation is investigated in terms of the dependence of field strength distribution near  $a$ -Si:H on the film thickness, by the SOW simulation in the TE guided mode. Figure 4 shows the profile of the four-layer structure of SOW of air,  $a$ -Si:H, optical waveguide and air. The effective complex refractive index and field strength distribution are obtained from solutions of an eigenvalue equation for a transversely guided mode.<sup>8)</sup>

Fig. 4. Structure of waveguide with the *a*-Si:H film.

The complex refractive index of SOW  $n_w$  and complex refractive index of *a*-Si:H  $n_a$  used in the simulation are obtained in the following manner.

First, ultraviolet-visible spectra of two SOW films which have different thicknesses are measured. A reflection coefficient and absorption coefficient are calculated using

$$T_i = T_0 \exp(-\alpha_w t_i) \quad (i = 1 \text{ or } 2) \quad (2)$$

$$(1 - R)^2 = T_0, \quad (3)$$

where  $T_i$  is the transmittance of each SOW film,  $i$  is the sample number,  $T_0$  is the transmittance when absorption of SOW is 0,  $\alpha_w$  is the absorption coefficient,  $t_i$  is the thickness of each SOW film and  $R$  is the reflection coefficient. The multiple reflection is neglected in the approximation here.

The real part of  $n_w$  is obtained using

$$R = (n'_w - 1)^2 / (n'_w + 1)^2, \quad (4)$$

where  $n'_w$  is the real part of  $n_w$ , and the refractive index of air is 1.

The imaginary part of  $n_w$  is obtained using

$$n''_w = \lambda / 2\pi \cdot \alpha_w, \quad (5)$$

where  $n''_w$  is the imaginary part of  $n_w$ , and  $\lambda$  is wavelength.

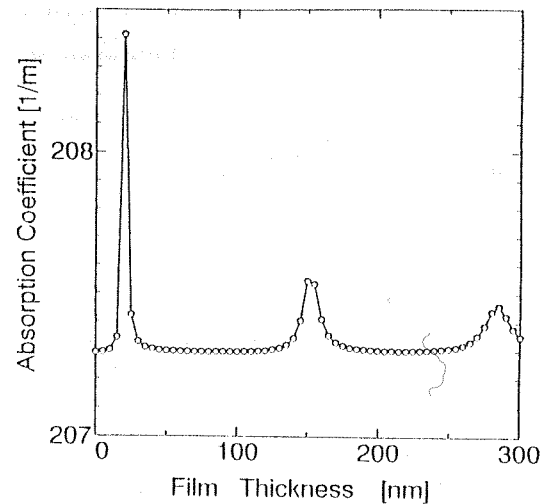
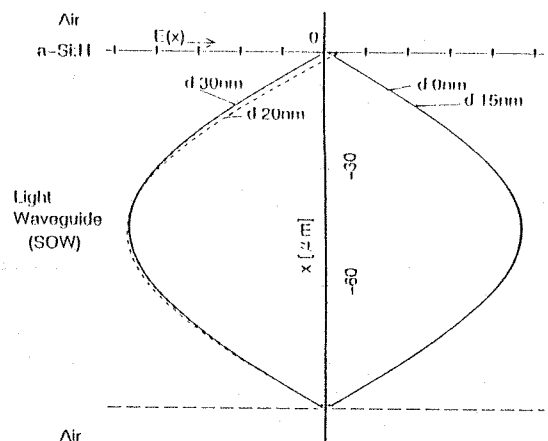
The real part of  $n_a$  is measured using an ellipsometer. The imaginary part of  $n_a$  is obtained using eq. (5), similarly to  $n''_w$ .

$n_w$ , obtained in the above manner, is  $1.62 - j2.09 \times 10^{-5}$ , and  $n_a$  is  $2.90 - j0.07$ .

We next studied the dependence of the absorption coefficient on the *a*-Si:H film thickness, obtained from the imaginary part of the effective complex refractive index of the four-layer structure SOW.

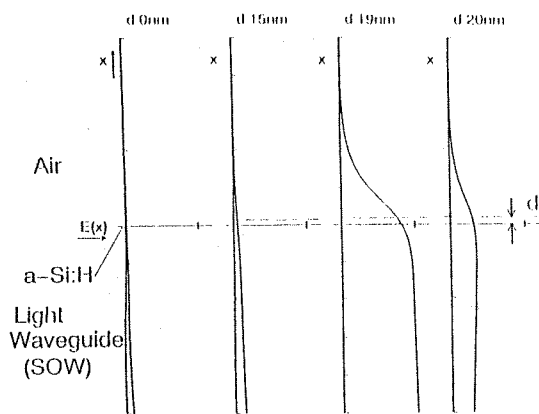
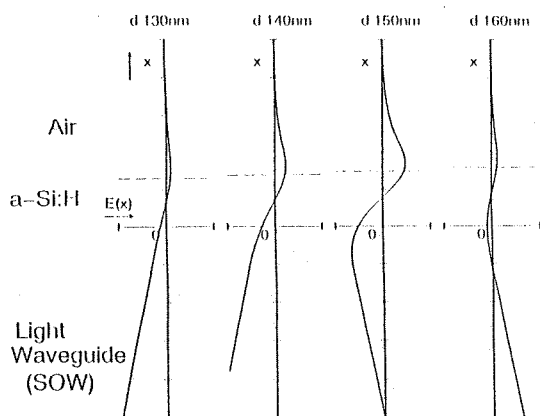
When the *a*-Si:H film thickness  $d$  is 0 nm, we observe the TE<sub>0</sub> mode. The dependence of the absorption coefficient of the four-layer structure SOW on the *a*-Si:H film thickness when the thickness of SOW  $t$  is constant at 95  $\mu\text{m}$ , is shown in Fig. 5. The absorption coefficient reaches a peak when the *a*-Si:H thickness  $d$  is around 20 nm, 150 nm and 280 nm with a period of approximately 130 nm.

Considering the results described above, we examine the electric field strength distributions observed at the *a*-Si:H film thicknesses  $d$  of around 20 nm and around 150 nm.

Fig. 5. Dependence of absorption coefficient on the *a*-Si:H film thickness for TE mode.Fig. 6. Field strength distributions of TE mode obtained by the SOW simulation.  $d = 0, 15, 20$  and  $30$  nm.

The field strength distributions throughout the entire optical waveguide at  $d$  of 0, 15, 20 and 30 nm are shown in Fig. 6. The line  $x = 0 \mu\text{m}$  corresponds to the boundary between the *a*-Si:H layer and the optical waveguide layer in Fig. 4. In Fig. 6, although the direction of the electric field is reversed between  $d = 15$  nm and 20 nm, the field distributions seem to be in the TE<sub>0</sub> mode throughout the entire waveguide including the *a*-Si:H layer. The details of the field distributions around  $x = 0 \mu\text{m}$  for  $d = 0, 15, 19$  and  $20$  nm are shown in Fig. 7.  $d$  increases in the positive direction along the  $x$  axis, and the boundary between air and *a*-Si:H is shown as the dashed line. The field distribution is in the TE<sub>0</sub> mode up to  $d = 19$  nm according to both Figs. 6 and 7. For  $d = 20$  nm, the direction of the electric field is reversed in Fig. 6, but not in Fig. 7. The number of antinodes of the electric field increases in Fig. 7.

The expanded view of the field distributions for thicker *a*-Si:H layers with  $d = 130, 140, 150$  and  $160$  nm is shown in Fig. 8. A new antinode of the electric field is observed between  $d = 140$  nm and  $d = 150$  nm. Here, the electric field in the *a*-Si:H layer becomes maximum. Therefore,

Fig. 7. Field strength distributions, at  $d = 0, 15, 19$  and  $20$  nm.Fig. 8. Field strength distributions, at  $d = 130, 140, 150$  and  $160$  nm.

in Fig. 5, the antinodes of the electric field in the  $a$ -Si:H layer are generated with a period of approximately  $130$  nm at approximately  $d = 20, 150$ , and  $280$  nm, at which the electric field in the  $a$ -Si:H layer becomes maximum. Because the absorption coefficient of  $a$ -Si:H is very large compared with that of the optical waveguide, the absorption must be large when amplitude of the field in the  $a$ -Si:H is high. From Figs. 7 and 8, as the amplitude of the field in the  $a$ -Si:H becomes high at  $d = 19$  nm and  $d = 150$  nm, the absorption of the four-layer SOW shows peaks.

When  $d$  is  $0$  nm, we observe the  $TE_n$  mode, and investigation in the same manner as described above reveals the same tendency. It has been confirmed that the absorption coefficient reaches a peak at almost the same thicknesses as shown in Fig. 5 as the  $a$ -Si:H film thickness increases.

The slab waveguide simulation of the four-layer structure clarified the following. As the  $a$ -Si:H film thickness increases from  $0$  nm, the field strength distribution in the  $a$ -Si:H film changes to the mode which has antinodes of the electric field. With each increase of the number of antinodes, the field strength distribution in the  $a$ -Si:H layer shows a maximum. As a result, oscillation occurs in the dependence of transmittance on the  $a$ -Si:H film thickness, as shown in Fig. 3, because the absorption coefficient of the entire optical waveguide becomes max-

imum periodically.

## 5. Method for Removing the Oscillation of Transmittance

The dependence of transmittance on the  $a$ -Si:H film thickness at each wavelength shows almost the same tendency as in Fig. 3.

The curve from which the oscillation in the dependence of transmittance on the deposited film thickness was removed at a certain wavelength goes through the point of transmittance of  $1$  at the thickness of  $0$  nm,  $(d, T) = (0, 1)$ , and is expressed as an exponential function with absorption coefficient  $\alpha$ . There is light which passes through the optical waveguide without interacting with the deposited film, in addition to light which is absorbed into the deposited film on the optical waveguide in this measurement method. The ratio of light which passes through the optical waveguide to the total amount of light is defined as the constant  $C_1$ , and the ratio of light which is absorbed into the deposited film is defined as the constant  $C_2$ . In Fig. 3, even if  $d$  becomes infinite, the transmittance approaches the constant  $C_1$  asymptotically instead of approaching  $0$ . Therefore, in our measurement method, the transmittance  $T$  is given by the expression below when the oscillation is removed.

$$T = C_1 + C_2 \exp(-\alpha d). \quad (6)$$

From eq. (6), when  $d = 0$ ,

$$C_1 + C_2 = 1. \quad (7)$$

The function  $T_u$  which goes through the maxima of the oscillation and function  $T_l$  which goes through the minima are expressed as

$$T_u = C_{1u} + C_{2u} \exp(-\alpha_u d) \quad (8)$$

$$T_l = C_{1l} + C_{2l} \exp(-\alpha_l d). \quad (9)$$

The relationship among  $T$ ,  $T_u$  and  $T_l$  is defined as

$$T = (T_u + T_l)/2. \quad (10)$$

Substituting eqs. (8) and (9) into eq. (10) yields,

$$C_1 + C_2 \exp(-\alpha d) = \{C_{1u} + C_{1l} + C_{2u} \exp(-\alpha_u d) + C_{2l} \exp(-\alpha_l d)\}/2. \quad (11)$$

For eq. (11) to hold for every  $d$ ,

$$\alpha = \alpha_u = \alpha_l. \quad (12)$$

From eqs. (6), (8), (9), (10) and (12),

$$C_1 = (C_{1u} + C_{1l})/2 \quad (13)$$

$$C_2 = (C_{2u} + C_{2l})/2. \quad (14)$$

From eqs. (7), (13) and (14),

$$C_1 + C_2 = (C_{1u} + C_{1l} + C_{2u} + C_{2l})/2 = 1. \quad (15)$$

Substituting the maxima  $(T_{u1}, d_2)$ ,  $(T_{u2}, d_4)$  and the minima  $(T_{l1}, d_1)$ ,  $(T_{l2}, d_3)$  into eqs. (8) and (9), applying eq. (12),  $C_{1u}$ ,  $C_{1l}$ ,  $C_{2u}$  and  $C_{2l}$  are given as functions of  $\alpha$  alone. Substituting  $C_{1u}$ ,  $C_{1l}$ ,  $C_{2u}$  and  $C_{2l}$  obtained above into eq. (15), the function wherein the  $1$  on the right-hand side is transposed to the other side is defined

as  $f(\alpha)$ . Therefore,

$$f(\alpha) = 0. \quad (16)$$

The values of the maxima and minima are obtained from the experimental values in Fig. 3. The values of  $C_{10}$  and  $C_{11}$  are also estimated roughly from the same figure. Substituting these values into eq. (8), the approximate value of  $\alpha_0$  is determined. On calculating  $f(\alpha)$  by varying  $\alpha$ , it becomes clear that there is only one value of  $\alpha$  which satisfies eq. (16) in the range of  $\alpha$  above 0 and below the value of two orders larger than  $\alpha_0$ . Then, using the Newton-Raphson method for eq. (16) with  $\alpha_0$  as the initial value, the value of  $\alpha$  is obtained.  $T$ ,  $T_u$  and  $T_l$  are determined using the value of  $\alpha$ , and are also shown in Fig. 3. The values of  $C_1 + C_2$ ,  $C_{10} + C_{11}$  and  $C_{20} + C_{21}$  when  $d = 0$ , obtained from eqs. (6), (8) and (9), and using eq. (12), are also shown in Fig. 3. It is clear that  $T_u$  passes through each maximum of the experimental values ( $\bullet$ ) and  $T_l$  passes through each minimum. Furthermore, it is clear that  $T$  almost passes through the middle of the experimental values ( $\bullet$ ). The same procedure to remove the oscillation is used at each wavelength. Figure 9 shows the experimental values ( $\bullet$ ) of the dependence of transmittance on the wavelength at the  $a$ -Si:H film thickness of 203.7 nm. The dependence of transmittance on the wavelength obtained from  $T$ ,  $T_u$  and  $T_l$  at each wavelength is also shown in the same figure ( $\circ$  is  $T$ , upper  $\circ$  is  $T_u$  and lower  $\circ$  is  $T_l$ ). From Fig. 9, it is clear that even if the abscissa is converted to wavelength the curves obtained from  $T_u$  and  $T_l$  go through the maxima and minima of the experimental values ( $\bullet$ ). The wavelength of 632.8 nm taken from Fig. 3 is also shown as the dashed line in Fig. 9.

Next, Fig. 10 shows the same data, with ordinate of  $(\alpha h\nu)^{1/2}$  and abscissa of  $h\nu$ , translated from the experimental values ( $\bullet$ ) and  $\circ$  plots in Fig. 9.  $E_g$  is obtained by extrapolating the straight line represented by eq. (1).

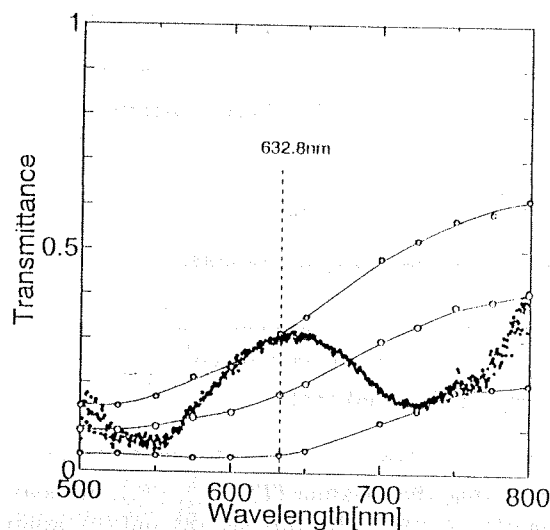


Fig. 9. Dependence of transmittance on wavelength.  $\bullet$ : from experimental values;  $\circ$ : transmittance without oscillation; upper  $\circ$ : upper transmittance  $T_u$ ; lower  $\circ$ : lower transmittance  $T_l$ . The data at the wavelength of 632.8 nm taken from Fig. 3 are also shown as the dashed line.

## 6. Dependence of $E_g$ on the Film Thickness

Next, the dependence of  $E_g$  on the  $a$ -Si:H film thickness, obtained using the SOW sensor, is shown in Fig. 11. The values with the transmittance oscillation removed ( $\circ$ ), as well as those without removal of the transmittance oscillation ( $\Delta$ ) for comparison are shown. From Fig. 11, it is clear that  $E_g$  is influenced significantly by the transmittance oscillation, and the errors in  $\Delta$  plots are marked. On the other hand, it is clear that  $E_g$  approaches a constant value when the  $a$ -Si:H film thickness is more than approximately 65 nm because the errors become small when the oscillation is removed. The value of  $E_g$  is approximately 1.8 eV which agrees with the value measured by the conventional method<sup>4)</sup> for an  $a$ -Si:H film on the order of 1  $\mu$ m thick.

After removing the influence of the transmittance oscillation, the increase of  $E_g$  with  $a$ -Si:H thickness less than 65 nm in  $\circ$  plots of Fig. 11 shows that absorption sufficient for determining  $E_g$  cannot be obtained in this range of film thickness.

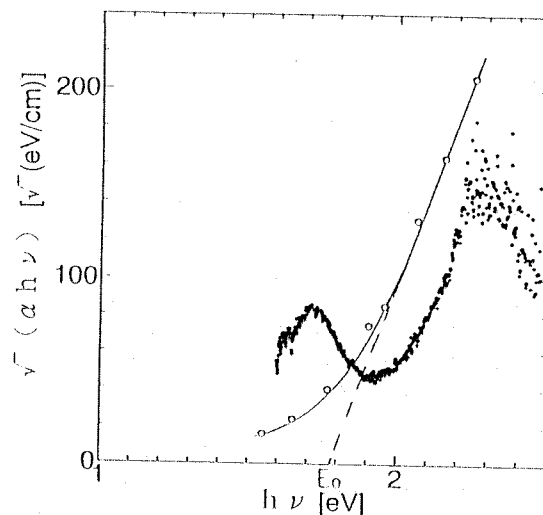


Fig. 10.  $(\alpha h\nu)^{1/2}$  versus photon energy  $h\nu$  translated from the plots in Fig. 9.  $\bullet$ : from experimental values;  $\circ$ : from transmittance without oscillation; dashed line: fitting straight line of eq. (1).

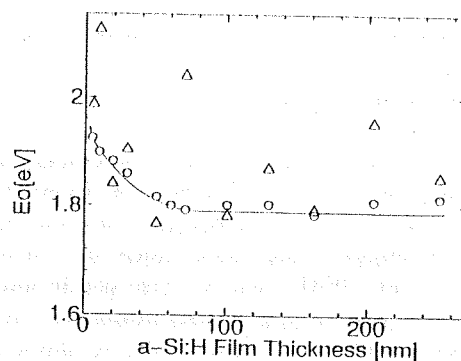


Fig. 11. Dependence of  $E_g$  on the  $a$ -Si:H film thickness.  $\circ$ : with the procedure to remove the oscillation and  $\Delta$ : without the procedure to remove the oscillation.

## 7. Characteristics of $E_g$ in Case of Changing the Dimensions of the SOW Sensor

We change the width and length of the SOW section on which film is deposited and the thickness of SOW, and investigate the dependence of  $E_g$  on the  $\alpha$ -Si:H film thickness.

### 7.1 Width of the SOW section with deposited film

The dependence of  $E_g$  on the  $\alpha$ -Si:H film thickness for various widths of the SOW section with  $\alpha$ -Si:H film deposition  $w$  is shown in Fig. 12. It is clear that  $E_g$  takes the same constant value at almost the same thickness when the width is 1 mm and 5 mm. Therefore, it is clear that the sensitivity of the sensor is not influenced if the range of  $w$  variation is small.

### 7.2 Length of the SOW section with deposited film

The dependence of  $E_g$  on the  $\alpha$ -Si:H film thickness for various lengths of the SOW section with  $\alpha$ -Si:H film deposition  $l$  is shown in Fig. 13. At  $l = 100$  mm,  $E_g$  takes a constant value for  $\alpha$ -Si:H film thickness  $d$  more than approximately 35 nm. At  $l = 50$  mm,  $E_g$  takes the same constant value when  $d$  is more than 65 nm. Therefore, it is clear that even if the  $\alpha$ -Si:H film is extremely thin,  $E_g$  can be determined when  $l$  is sufficiently long. It is considered that sufficient absorption for the determination of  $E_g$  is obtained because the interaction distance between  $\alpha$ -Si:H and guided light becomes longer when  $l$  becomes longer. Also, it is clear that the products of the minimum values of the thickness  $d$  needed to determine  $E_g$  and  $l$  in two samples are almost the same.

### 7.3 Thickness of SOW

The dependence of  $E_g$  on the  $\alpha$ -Si:H film thickness for various thicknesses of SOW  $t$  is shown in Fig. 14. At  $t = 30$   $\mu$ m,  $E_g$  has a constant value when the  $\alpha$ -Si:H film thickness  $d$  is more than approximately 20 nm. At  $t = 78$   $\mu$ m,  $E_g$  has the same constant value when  $d$  is more than approximately 65 nm. From this result, it is clear that  $E_g$  can be determined when  $t$  is sufficiently thin. When  $t$  becomes thin, the amount of light which passes through the optical waveguide without interacting with the  $\alpha$ -Si:H film decreases (corresponding to the

decrease of  $C_2$  in eq. (6)). Therefore, sufficient absorption is obtained to determine  $E_g$  because the effective absorption coefficient increases.

In our investigation using the conventional method for  $E_g$  with various thicknesses of the deposited film, the  $\alpha$ -Si:H film thickness is required to be more than approximately 750 nm,<sup>4)</sup> whereas a film thickness of approximately 20 nm is sufficient to measure  $E_g$  in our method. In other words, the  $E_g$  measurement of  $\alpha$ -Si:H is accomplished with thickness on the order of 1/40 that required in the conventional method.

## 8. Conclusions

For the optical energy gap measurement of  $\alpha$ -Si:H ultrathin films, we proposed a new method of using a SOW as the sensor.

(1) It has been shown experimentally that with increasing  $\alpha$ -Si:H film thickness, transmittance decreases with periodic oscillation. It was clarified analytically that this phenomenon occurs because the field strength distribution of the guided modes at the  $\alpha$ -Si:H layer periodically becomes maximum with increase of the film deposition thickness, so that the absorption coefficient of the entire waveguide including the  $\alpha$ -Si:H film exhibits peaks periodically.

(2) The method for removing the oscillation in the dependence of transmittance on the  $\alpha$ -Si:H film thickness has been described, and it has been shown that the

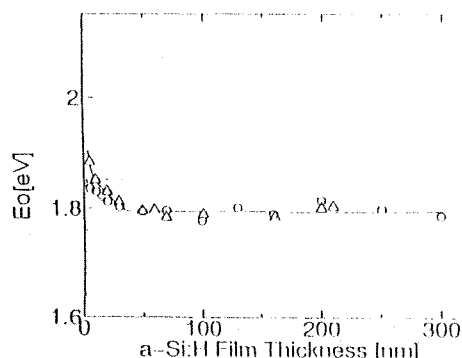


Fig. 12. Dependence of  $E_g$  on the  $\alpha$ -Si:H film thickness with variation of the width of the SOW section with film deposition  $w$ .  $\circ$ :  $w = 5$  mm,  $l = 100$  mm and  $t = 90$   $\mu$ m;  $\triangle$ :  $w = 1$  mm,  $l = 100$  mm and  $t = 87$   $\mu$ m.

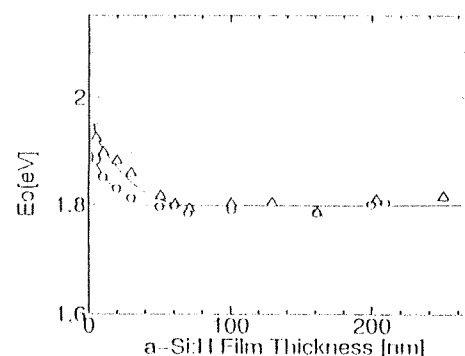


Fig. 13. Dependence of  $E_g$  on  $\alpha$ -Si:H film thickness with variation of the length of the SOW section with film deposition  $l$ .  $\circ$ :  $l = 100$  mm,  $w = 1$  mm;  $\triangle$ :  $l = 50$  mm,  $w = 0.8$  mm.

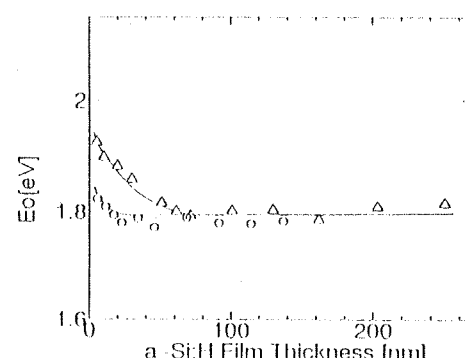


Fig. 14. Dependence of  $E_g$  on  $\alpha$ -Si:H film thickness with variation of the thickness of SOW  $t$ .  $\circ$ :  $t = 30$   $\mu$ m,  $w = 2.4$  mm;  $\triangle$ :  $t = 78$   $\mu$ m,  $w = 0.8$  mm.

exponential function which passes through the point of transmittance of 1 at the film thickness of 0 nm, with oscillation removed, can be obtained. It has been clarified that the influence of the oscillation in the dependence of  $E_g$  on the wavelength can be removed, and  $E_g$  can be determined in a range of thin films which could not be measured previously by conventional methods.

(3) To increase the sensitivity of the SOW sensor, we need only increase the length of the SOW section with film deposition  $l$  and/or decrease the thickness of the SOW sensor  $t$ . The width of the SOW section with film deposition  $w$  is not related to the sensitivity of the sensor in the range of width studied in this work (approximately from 1 to 5 mm).

(4)  $E_g$  can be determined for  $\alpha$ -Si:H film thicker than approximately 20 nm (approximately 1/40 the thickness required in the conventional method) when the SOW sensor (the material is PCZ,  $t$  is 100  $\mu\text{m}$ ,  $l$  is 100 mm and  $w$  is 5 mm) is used.

This method is an *in situ* measurement method in which the  $\alpha$ -Si:H film is not exposed to air, while in the conventional methods air exposure is unavoidable. This

is an especially important issue for ultrathin films which are easily affected by oxidation.

#### Acknowledgement

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# INFLUENCE OF LONGITUDINAL MAGNETIC FIELD APPLIED TO COAXIAL LINE TYPE MICROWAVE PLASMA (II)

## 同軸線路形マイクロ波プラズマへの縦磁界印加の影響 (II)

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**Abstract** The magnetic field along the gas flow (the longitudinal magnetic field) is applied to the discharge area in the double tubed coaxial line type microwave plasma chemical vapor deposition system and the effect of the applied longitudinal magnetic field to pure  $N_2$  plasma is considered as follows. The probe I-V characteristic is stabilized by applying the magnetic field over about 1000[Gauss]. When the magnetic flux density is about 1000[Gauss], the electron temperature and the electron density increase due to the effect of the electron cyclotron resonance. The effect of the applied longitudinal magnetic field doesn't vary over about 1000[Gauss] regardless of the magnetic flux density. In the vicinity of the place where plasma blows off into the deposition chamber, one can increase  $n_e$  at  $z=1.5$ [cm] by about ten times and can increase  $n_e$  at  $z=0$ [cm] by about three times. Therefore this plasma is proper for CVD because it is possible to fabricate films at high rate.

### 1. Introduction

In order to generate the stable plasma in a wider range of the gas pressure and with various kinds of gases, the coil is set up around the discharge tube of the double tubed coaxial line type microwave plasma chemical vapor deposition system. The magnetic field along the gas flow is applied to the discharge area. The plasma parameters are measured by the single probe method, and the effects resulted from depression of the diffusion of plasma in the radial direction are investigated.<sup>[1]~[5]</sup> In this report, the plasma parameters in the discharge area have been measured. And the discharge mechanism is examined in detail.

### 2. Experiment

In this system, the microwave electric field in the discharge area is the fundamental mode of the coaxial line and runs parallel with the gas flow, namely, with the applied magnetic field. Therefore the electron cyclotron resonance (ECR) doesn't fundamentally occur. The axial distance from the end of the discharge tube is defined as  $z$  and the radial distance from the center axis of the discharge tube is defined as  $r$ . For further details of this system, see ref. [2].

The experimental condition is shown in the Table 1. With the  $N_2$  gas flow rate 50 [ml/min], letting  $SiH_4$  gas flow, SiN films is fabricated. The experiment is made on pure  $N_2$  plasma. The magnetic flux density ( $B$ ) is the value at the center of the coil. The single probe method is applied in the measurement. At  $z=1.5$ [cm] in the deposition chamber, a probe of 0.05[cm] in



diameter and 1.0[cm] in length is used, where the gas flow rate is 30,40 and 50[ml/min]. At  $z=0$  and -1.5[cm] in the vicinity of the discharge area, a probe of 0.05[cm] in diameter and 0.1[cm] in length is used, where the gas flow rate is 50[ml/min]. The probe is set up perpendicularly to the gas flow, namely, to the magnetic field in some way like bending the tip of the probe perpendicularly. It is confirmed that the results of the measurements agree with each other regardless of the probe length. The end of the inner tube is set up at  $z=-2.0$ [cm]. It is the same position when SiN films are fabricated.

Table 1: Experimental Condition

|                              |                                 |          |
|------------------------------|---------------------------------|----------|
| Microwave Input Power        | 150                             | [W]      |
| Microwave Reflective Power   | 45                              | [W]      |
| N <sub>2</sub> Gas Flow Rate | 30,40,50                        | [ml/min] |
| Gas Pressure in Chamber      | 2.4,3.2,4.0                     | [mTorr]  |
| Position of Probe            | $z=1.5,0,-1.5$ [cm], $r=0$ [cm] |          |
| Coil Current                 | 0~6                             | [A]      |
| Magnetic Flux Density        | 0~1986                          | [Gauss]  |

### 3. Result and Discussion

First, we consider the results of the measurement in the deposition chamber, namely, at  $z=1.5$ [cm]. The dependences of the electron temperature ( $T_e$ ) and the electron density ( $n_e$ ) on  $B$  are shown in Fig. 1 and 2.

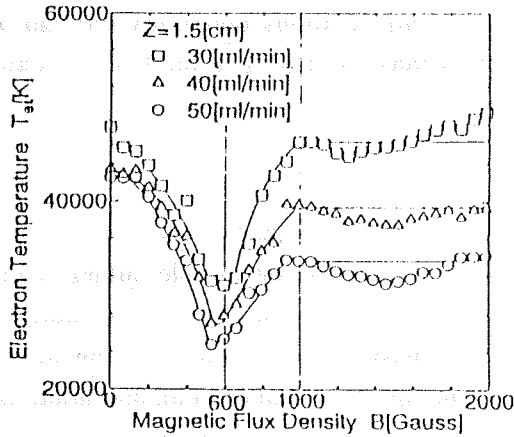


Figure 1: Dependence of Electron Temperature on Magnetic Flux Density

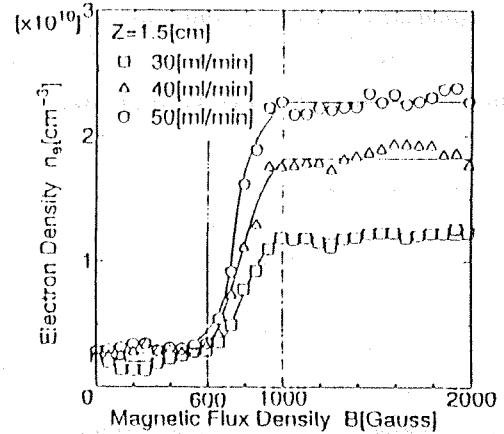


Figure 2: Dependence of Electron Density on Magnetic Flux Density

With increasing  $B$  from 0 to about 600[Gauss],  $T_e$  decreases and  $n_e$  keeps constant. The reason is as follows. The diffusion of electrons toward the wall of the discharge tube is depressed by applying the longitudinal magnetic field, the decay of electrons on the wall decreases, and in order to keep the balance of the generation and the decay of the plasma, the generation of electron must decrease. Therefore,  $T_e$  decreases. This reason is as follows. It becomes difficult that the microwave electric power penetrates the center of the plasma as  $n_e$  increases in the vicinity of the wall of the discharge tube.

With increasing  $B$  from about 600[Gauss] to about 1000[Gauss], both  $T_e$  and  $n_e$  increase and are saturated at about 1000[Gauss]. This is the effect of ECR. It occurs not at the resonance magnetic field 875[Gauss] but at about 1000[Gauss]. For further details about this, see ref. [2].

With increasing  $B$  over about 1000[Gauss],  $T_e$  and  $n_e$  keep constant. The reason is as follows. The dependence of the electron diffusion coefficient ( $D_{\perp}$ ) in the radial direction on  $B$  is given

by

$$D_{\perp} = \frac{D}{1 + \omega_c^2/\nu^2} \quad D = \frac{kT_e}{m_e \nu} \quad \omega_c = \frac{eB}{m_e}$$

where  $k$  is Boltzmann constant,  $e$  is quantum of electricity,  $\nu$  is collision frequency and  $m_e$  is electron mass. The result of this calculation is shown in Fig. 3.

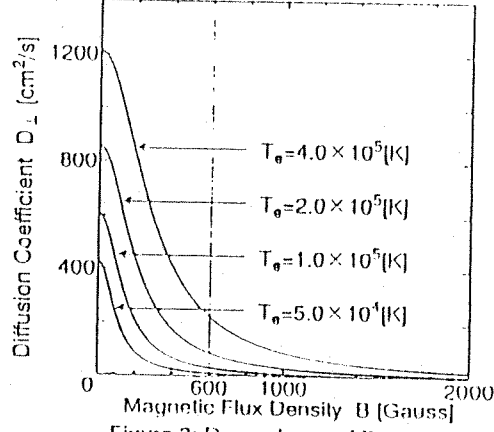


Figure 3: Dependence of  $D_{\perp}$  on  $B$

In this figure,  $D_{\perp}$  decreases rapidly with increasing  $B$  from 0[Gauss] to about 600[Gauss], and decreases gradually with increasing  $B$  over about 600[Gauss]. That is to say, the effect that the diffusion of electrons is depressed increases rapidly under about 600[Gauss], and that increases gradually over about 600[Gauss]. The reason for  $T_e$  and  $n_e$  are constant with increasing  $B$  over about 1000[Gauss] is as follows. The effect that the diffusion of electrons is depressed increases gradually and the effect of ECR decreases at the same time. And in this figure, the tendency that the slope of the curve around 0[Gauss] is nearly zero correspond with the tendency of the dependence of  $T_e$  on  $B$  which is shown previously.

In addition,  $n_e$  at  $z=1.5$ [cm] increases by about ten times applying the magnetic field (as shown Fig. 2).

Next, we will consider the results of the measurement in the vicinity of the discharge area, namely, at  $z=0, -1.5$ [cm]. The dependences of  $T_e$  and  $n_e$  on  $B$  are shown in Fig. 4 and 5.

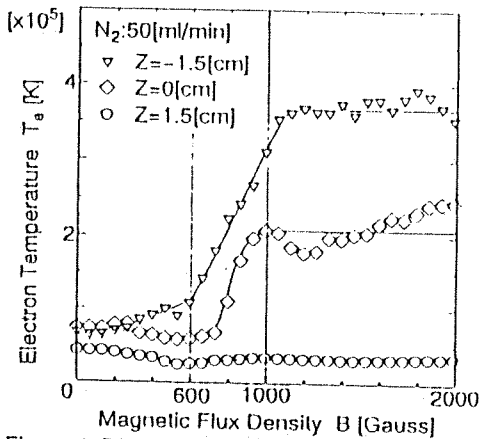


Figure 4: Dependence of Electron Temperature on Magnetic Flux Density

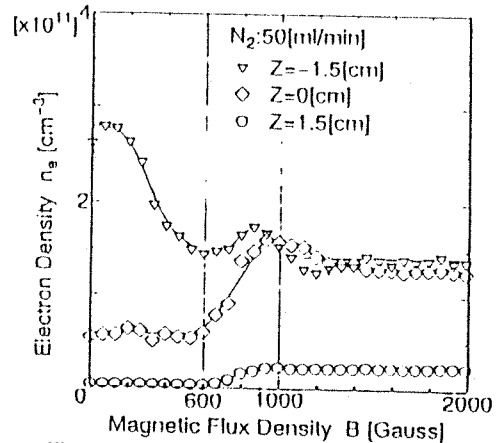


Figure 5: Dependence of Electron Density on Magnetic Flux Density

In case of  $z=0$ [cm], the results are as follows. With increasing  $B$  from 0[Gauss] to about 1000[Gauss],  $T_e$  decreases and  $n_e$  keep constant. With increasing  $B$  from about 600[Gauss] to about 1000[Gauss], both  $T_e$  and  $n_e$  increase due to the effect of ECR. And with increasing  $B$

over about 1000[Gauss], both of them keep constant. This tendency is same as the tendency at  $z=1.5$ [cm].

In addition,  $n_e$  at  $z=0$ [cm] increases by about three times applying the magnetic field.

In case of  $z=-1.5$ [cm], the results are as follows. With increasing B from 0[Gauss] to about 600[Gauss],  $T_e$  increases a little and  $n_e$  decreases rapidly. This tendency is different from the tendency at  $z=1.5$  and 0[cm]. The reason is as follows. The radial distribution of  $n_e$  in the discharge tube varies from the shape of zero degree Bessel function to the shape like trapezoid with increasing B and therefore  $n_e$  at  $r=0$ [cm] decreases. In addition, the distance from the end of the inner tube is only 0.5[cm] and many of the electrons can't reach the shadow of the inner tube due to depression of the diffusion of electrons. The reason why  $T_e$  increases is that most of the electrons which reach the shadow of the inner tube have high energy.

With increasing B from about 600[Gauss] to about 1000[Gauss], both  $T_e$  and  $n_e$  increase due to the effect of ECR. And with increasing B over about 1000[Gauss], both of them keep constant. This tendency is same as the tendency at  $z=1.5$  and 0[cm].

It follows from what has been said that the effect of the applied longitudinal magnetic field doesn't vary over about 1000[Gauss] regardless of B.

In addition, it is confirmed that the probe I-V characteristic is stabilized by applying the magnetic field over about 1000[Gauss].

#### 4. Conclusions

The magnetic field along the gas flow is applied to the discharge area, and the effects of the applied longitudinal magnetic field are considered as follows.

(1) The probe I-V characteristic is stabilized by applying the magnetic field over about 1000[Gauss].

(2) When B is about 1000[Gauss],  $T_e$  and  $n_e$  increase due to the effect of ECR.

(3) The effect of the applied longitudinal magnetic field doesn't vary over about 1000[Gauss] regardless of B.

(4) In the vicinity of the place where plasma blows off into the deposition chamber, one can increase  $n_e$  at  $z=1.5$ [cm] by about ten times and can increase  $n_e$  at  $z=0$ [cm] by about three times. Therefore this plasma is proper for CVD because it is possible to fabricate the films at high rate.

#### Acknowledgement

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INFLUENCE OF LONGITUDINAL MAGNETIC FIELD APPLIED TO  
COAXIAL LINE TYPE MICROWAVE PLASMA (III)  
同軸線路形マイクロ波プラズマへの縦磁界印加の影響 (III)

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**Abstract** The magnetic field along the gas flow (the longitudinal magnetic field) is applied to the discharge area in the double tubed coaxial line type microwave plasma chemical vapor deposition system and the electron density ( $n_e$ ) is measured in the Ar plasma. The effects of the applied magnetic field to the Ar plasma are investigated. The results are as follows. With increasing the magnetic flux density ( $B$ ),  $n_e$  in the deposition chamber has a peak but  $n_e$  in the vicinity of the discharge area doesn't vary remarkably. In the vicinity of the discharge area, in any  $B$ ,  $n_e$  at the center of the discharge tube is higher than that at the point which is away from the center of the discharge tube, because the plasma decays on the wall of the discharge tube by bipolar diffusion. Moreover the radial distribution of  $n_e$  varies from the shape which is described as  $J_0$  Bessel function to the shape like trapezoid, because the diffusion of the charged particles toward the wall of the discharge tube is depressed by applying the magnetic field.

## 1. Introduction

The plasma parameters have been measured in the double tubed coaxial line type microwave plasma chemical vapor deposition system. The plasma parameters in the deposition chamber, that is to say, in the spatial afterglow plasma have been measured, and the effects of the applied magnetic field to Ar plasma have been investigated<sup>(1)-(5)</sup>. In this report, the spatial distribution of the electron density ( $n_e$ ) are measured when the magnetic field is applied to Ar plasma. From the results of this measurement, the discharge mechanism in this system is investigated from the effects of the applied magnetic field to Ar plasma.

## 2. Experiment

Fig. 1 shows the configuration of this system. For further details of this system, see reference (2). Table 1 shows the experimental condition.

The  $n_e$  is measured by a single probe method. The cylindrical probe of 0.05[cm] in diameter and of 1.0 or 0.1[cm] in length is used. The probe is set perpendicularly to the magnetic force line. The axial distance from the end of the discharge tube is defined as  $z$  and the radial distance from the center axis of the discharge tube is defined as  $r$ .

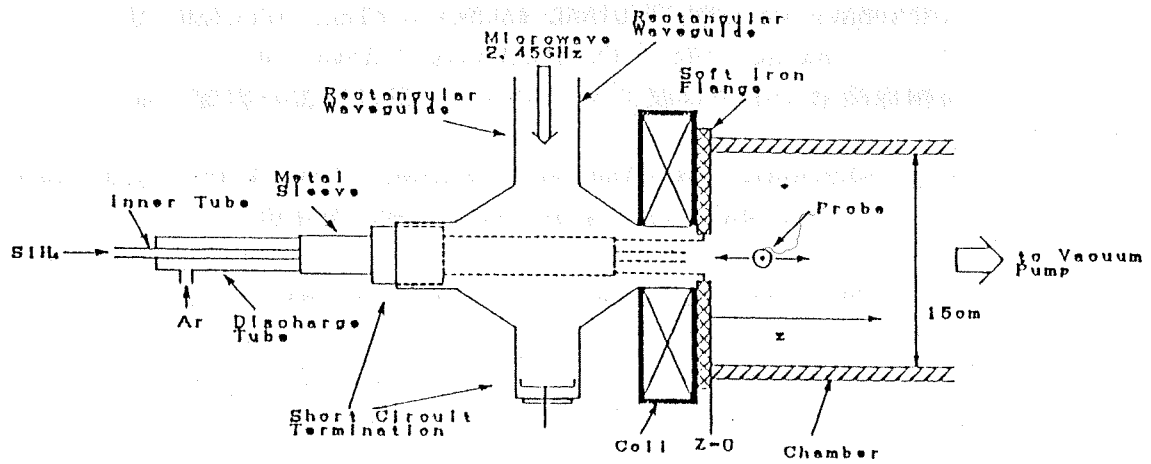


Fig. 1 Experimental Apparatus

Table 1. Experimental Condition

|                               |                           |
|-------------------------------|---------------------------|
| Microwave Input Power         | 100 [W]                   |
| Microwave Reflective Power    | 30 [W]                    |
| Ar Gas Flow Rate              | 30 [ml min]               |
| Gas Pressure in Chamber       | 2.6 [mTorr]               |
| Position of Probe             | $z = 1.0 \sim 1.5$ [cm]   |
|                               | $r = 0, 0.3$ [cm]         |
| Coil Current                  | $I = 0 \sim 6$ [A]        |
| Magnetic Flux Density(Center) | $B = 0 \sim 1986$ [Gauss] |

### 3. Result and Discussion

Fig. 2 shows the dependence of  $n_e$  on magnetic flux density ( $B$ ) at  $z = 1.5$  [cm]. The  $B$  is the value at the center of the coil. It shows that  $n_e$  increases gradually with  $B$  increased from 0 to about 700 [Gauss] because the radial diffusion of the charged particles is depressed by applying the magnetic field. Then,  $n_e$  increases rapidly and peaks out at about 1200 [Gauss]. This is the effect of the electron cyclotron resonance. With  $B$  increased further,  $n_e$  decreases because of the decay of the effect of the electron cyclotron resonance.

Fig. 3 shows the dependence of  $n_e$  on  $B$  at  $z = 0$  [cm]. It shows that the dependence of  $n_e$  has the same tendency as Fig. 2 ( $z = 1.5$  [cm]). However,  $n_e$  increases by about 2.5 times compared with  $n_e$  at  $z = 1.5$  [cm], because the point of the measurement ( $z = 0$  [cm]) is nearer to the discharge plasma area than the point of  $z = 1.5$  [cm].

Fig. 4 shows the dependence of  $n_e$  on  $B$  at  $z = 1.0$  [cm] as parameter is  $r$ . With  $B$  increased, both  $n_e$  at  $r = 0$  and  $0.3$  [cm] decrease and then are constant. The reason why  $n_e$  decreases is as follows. With  $B$  increased, the radial distribution of  $n_e$  varies from the shape which is described as  $J_0$  Bessel

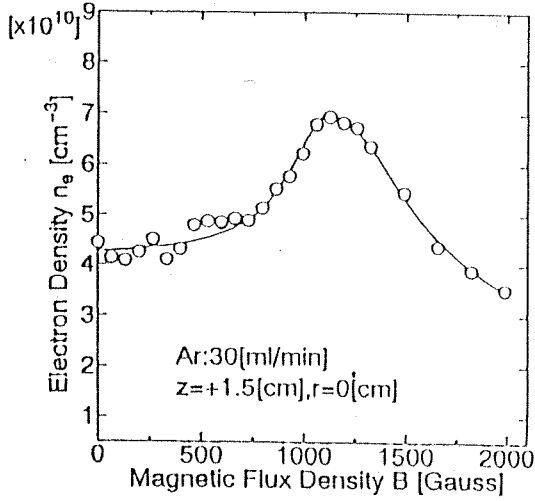


Fig.2 Dependence of Electron Density on Magnetic Flux Density

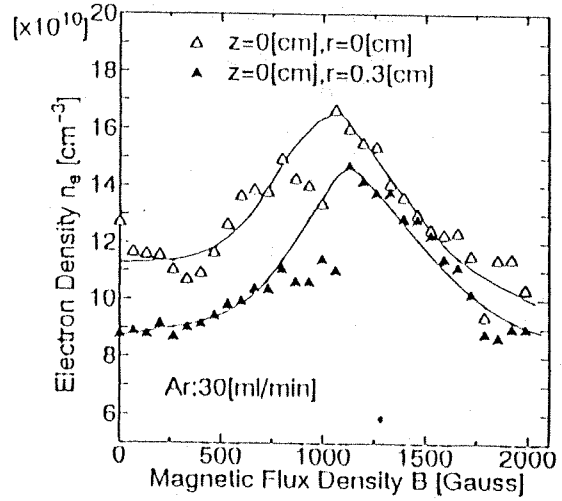


Fig.3 Dependence of Electron Density on Magnetic Flux Density

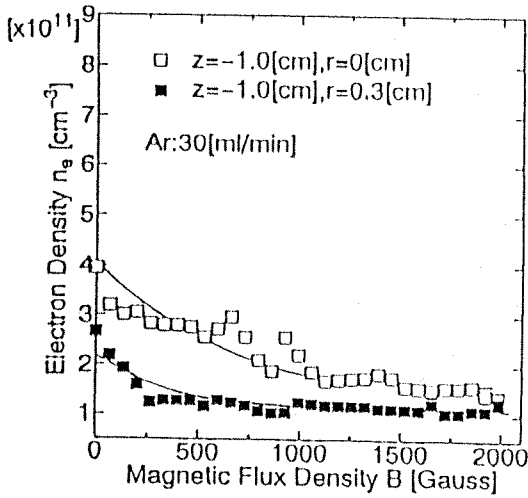


Fig.4 Dependence of Electron Density on Magnetic Flux Density

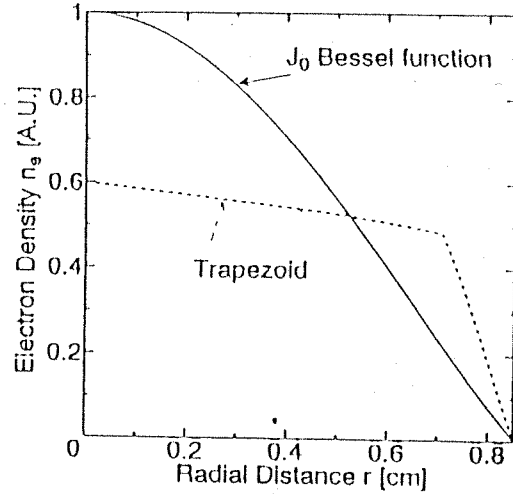


Fig.5 Distribution of Electron Density on Radial Distance

function to the shape like trapezoid (as shown in Fig.5), because the diffusion of the charged particles toward the wall of the discharge tube is depressed by applying the magnetic field, and it becomes difficult that the microwave electric power penetrates to the center of the plasma, and in the vicinity of the wall the rate of ionization increases. The value of both  $n_e$  at  $r=0$  and  $0.3[\text{cm}]$  becomes higher than that at  $z=0[\text{cm}]$ , because the point of the measurement ( $z=-1.0[\text{cm}]$ ) is nearer to the discharge area than the point of  $z=0[\text{cm}]$ .

Moreover, Fig.3 and 4 show that  $n_e$  at  $r=0.3[\text{cm}]$  is lower than that at  $r=0[\text{cm}]$  regardless of  $B$ . These results show that  $n_e$  decreases as the point

of the measurement is nearer to the wall of the discharge tube, because the plasma decays on the wall of the discharge tube by the surface recombination. That is to say, the radial distribution doesn't have a dimple in the center of the plasma, because the volume recombination doesn't occur on account of the low pressure. As  $B$  is increased, the difference between  $n_e$  at  $r=0$ [cm] and that at  $r=0.3$ [cm] decreases (as shown in Fig.3 and 4). This shows that the radial distribution of  $n_e$  varies from the shape which is described as  $J_0$  Bessel function to the shape like trapezoid, and shows that the conclusions mentioned above is valid.

#### 4. Conclusions

- (1) At  $z=1.5$  and  $0$ [cm], with  $B$  increased, the tendency of  $n_e$  has a peak at about  $1200$ [Gauss], because of the effect that the diffusion of the charged particles is depressed by applying the magnetic field and the effect of the electron cyclotron resonance.
- (2) At  $z=0$  and  $1.0$ [cm],  $n_e$  at  $r=0.3$ [cm] is lower than that at  $r=0$ [cm]. It shows the natural result that  $n_e$  decreases as the point of the measurement is nearer to the wall of the discharge tube, because the plasma decays on the wall of the discharge tube by the surface recombination.
- (3) At  $z=-1.0$ [cm], the vicinity of the discharge area, with  $B$  increased,  $n_e$  decreases and then is constant. As  $B$  is increased, the difference between  $n_e$  at  $r=0$ [cm] and that at  $r=0.3$ [cm] decreases.
- (4) From these results, it is cleared that the radial distribution in the discharge tube varies from the shape which is described as  $J_0$  Bessel function to the shape like trapezoid. This shows that the uniform plasma in radial direction, which is proper for CVD, is obtained.

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# Film Deposition under Control of Sheath Voltage on the Film Surface in MPCVD Apparatus

## MPCVDにおける膜前面のシース電圧の制御と成膜

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**Abstract** It is necessary to discuss the ion bombardment on the film surface while film deposition when the thin films are fabricated in a plasma CVD method. The ion bombardment energy is caused by not merely DC substrate bias voltage but the sheath voltage on the film surface. Therefore, it is considered that the ion bombard energy can be controlled when the sheath voltage on the film surface is controlled. In this paper, it is clear that the sheath voltage on the film surface can be controlled from 0[V] to -95[V] when DC substrate bias voltage is varied from +40[V] to -80[V]. And then, a-Si:H films are fabricated when the sheath voltage on the film surface is varied from 0[V] to -95[V]. As a result, it is clear that the dangling bond density increases, however, Si concentration and the ratio of the SiH bond density to the SiH<sub>2</sub> bond density increase.

## 1. Introduction

We have developed the double tubed coaxial line type microwave plasma CVD (MPCVD) apparatus. In this apparatus, the microwave power is confined in the cylindrical cavity. Therefore, a discharge plasma is created only in the cavity region. In the deposition chamber, a spatial afterglow plasma without supply of the microwave power is created by gas flow and diffusion. The discharge region of the apparatus has the double tubed structure that consists of the fused quartz outer discharge tube and the stainless steel inner tube concentrically. The Ar gas is fed to the outer discharge tube and the SiH<sub>4</sub> gas is fed to the inner tube. The argon atoms are ionized in the cavity region by the microwave power. The inner tube guide the SiH<sub>4</sub> gas to the discharge tube end, then SiH<sub>4</sub> is dissociated by the collision with the Ar plasma particles. The substrate table is placed at 10[cm] of the axial distance from the discharge tube end in the spatial afterglow plasma. Under this condition, the distribution of the electron temperature ( $T_e$ ) and density ( $n_e$ ) don't change when DC substrate bias voltage ( $V_{dc}$ ) is varied from +40[V] to -80[V] (in this voltage limits DC discharge doesn't generate). However, the plasma space potential ( $V_s$ ) change, therefore, the sheath voltage on the film surface ( $V_{sh}$ ) change. We reported that  $V_{sh}$  doesn't become

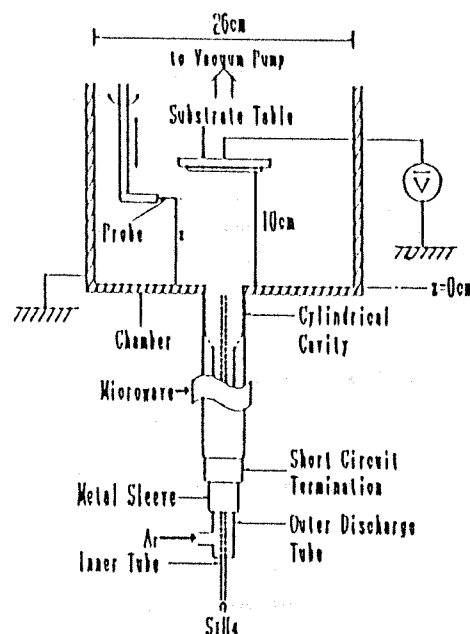


Fig.1 Configuration of the MPCVD apparatus



0[V] with varying  $V_{dc}$  when the substrate table area ( $A_s$ ) is large (about 50[cm<sup>2</sup>]), but  $V_{sh}$  become 0[V] or positive value with varying  $V_{dc}$  when  $A_s$  is small<sup>(1)</sup>.

In this paper, it is clear that  $V_{sh}$  can be controlled from 0[V] to -95[V] when  $A_s=40$ [cm<sup>2</sup>] and  $V_{dc}=+40$ [V] ~ -80[V]. And then, a-Si:H films are fabricated when  $V_{sh}$  is varied from 0[V] to -95[V] and the film properties are evaluated.

## 2. Experiment

Figure 1 shows the configuration of the MPCVD apparatus. The axial distance from the discharge tube end is defined as  $z$ . The substrate table is placed at  $z=10$ [cm]. The substrate table area ( $A_s$ ) is 40[cm<sup>2</sup>] and  $V_{dc}$  is varied from +40[V] to -80[V]. The single probe measurement is performed in the Ar/SiH<sub>4</sub> plasma (Ar gas flow rate: 110[ml/min], SiH<sub>4</sub> gas flow rate: 30[ml/min]). In this plasma a-Si:H films are also fabricated. The cylindrical probe of 0.05[cm] in diameter and 1[cm] in length is used for the probe measurement. The probe measurement is performed at  $z=9$ [cm] on the deposition chamber axis. And then, a-Si:H films are fabricated and the film properties are evaluated.

## 3. Result and Discussion

Figure 2 shows the dependence of  $T_e$  and  $n_e$  at  $z=9$ [cm] on  $V_{dc}$ . In fig. 2, the values in case of different  $A_s$  are showed for reference. The  $T_e$  and  $n_e$  don't change with varying  $V_{dc}$ . Therefore, the reactivity in this plasma is not influenced with varying  $V_{dc}$ .

Figure 3 shows the dependence of  $V_s$  at  $z=9$ [cm] on  $V_{dc}$ . The  $V_s$  is constant in the range of negative value of  $V_{dc}$ , and increases with increasing  $V_{dc}$  in the range of positive value of  $V_{dc}$ . And then,  $V_s$  becomes 40[V] when  $V_{dc}=+40$ [V] (on the dotted line in fig. 3).

Subtract  $V_s$  at  $z=9$ [cm] from  $V_{dc}$  and we get  $V_{sh}$ . Therefore,  $V_{sh}$  is calculated by using fig. 3. Figure 4 shows the dependence of  $V_{sh}$  on  $V_{dc}$ . The  $V_{sh}$  is 0[V] when  $V_{dc}=+40$ [V], and  $V_{sh}$  is -95[V] when  $V_{dc}=-80$ [V]. This figure indicates that a-Si:H films can be fabricated under controlling  $V_{sh}$  from 0[V] to -95[V] by using the substrate table which area is 40[cm<sup>2</sup>].

The a-Si:H films are fabricated with varying  $V_{sh}$  and these film properties are evaluated. Figure 5 shows the dependence of the deposition rate on  $V_{sh}$ . The deposition rate decreases with increasing the ion bombardment energy.

Figure 6 shows the dependence of the Si concentration on  $V_{sh}$ . The film density increases

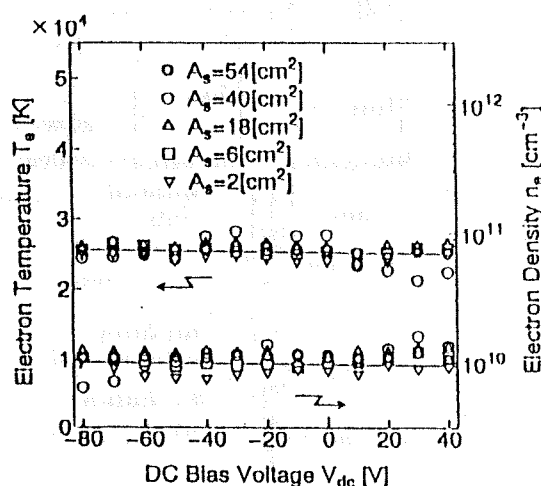


Fig.2 Dependence of  $T_e$  and  $n_e$  at  $z=9$ [cm] on  $V_{dc}$

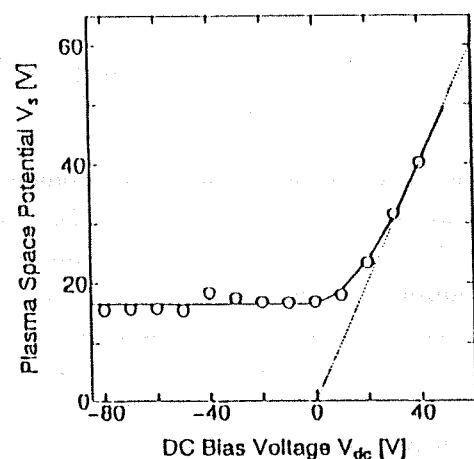


Fig.3 Dependence of  $V_s$  at  $z=9$ [cm] on  $V_{dc}$

with increasing the ion bombardment energy.

Figure 7 shows the dependence of the ratio of the SiH bond density to the SiH<sub>2</sub> bond density on  $V_{sh}$ . The SiH bond density increases with increasing the ion bombardment energy and SiH<sub>2</sub> bond density decreases with increasing the ion bombardment energy.

Figure 7 shows that the hydrogen atoms are disconnected because the film surface is heated by the ion bombardment. Because the film surface heated up, mobility of the radicals on the film surface increase and the radicals fill in the defects caused by the disconnection of the hydrogen atoms. It results high density a-Si:H films as shown in fig.6.

Figure 8 shows the dependence of the amount of Si deposited per unit area and unit time, calculated by (Si concentration ( $C_{Si}$ ) as shown fig.6  $\times$  the deposition rate (D.R.) as shown fig.5), on  $V_{sh}$ . The amount of Si deposited per unit area and unit time is constant in the range of  $V_{sh} >$  about -40[V] and decreases with increasing the ion bombardment energy in the range of  $V_{sh} <$  about -40[V]. This figure indicates the sputtering occurs when  $V_{sh}$  is about -40[V].

Figure 9 shows the dependence of the Ar atom density on  $V_{sh}$ . The Ar atom density is under the limit of detection in the range of  $V_{sh} >$  about -40[V]. It is considered that the Ar atom is not implanted in the film. The Ar atom is implanted in the film in the range of  $V_{sh} <$  about -40[V]<sup>(2)</sup>. Generally, it is said that the Ar plasma etching occurs when the accelerating voltage is lower than about -50[V] and this figure indicates that Ar ion implantation occurs when the accelerating voltage is lower than about -40[V]. These values show good agreement.

Figure 10 shows the dependence of the dangling bond density on  $V_{sh}$ . The dangling bond density increases with increasing the ion bombardment energy. It is considered that the void is formed around Ar atom implanted by the ion bombardment.

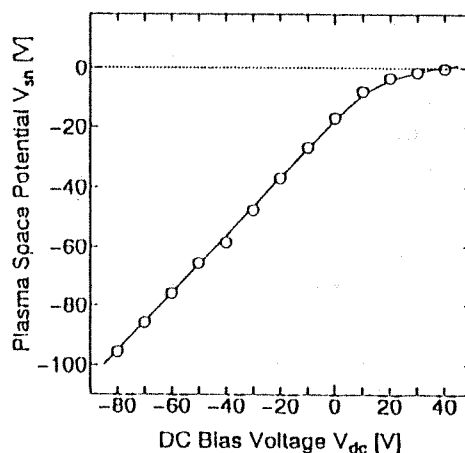


Fig.4 Dependence of  $V_{sh}$  on  $V_{dc}$

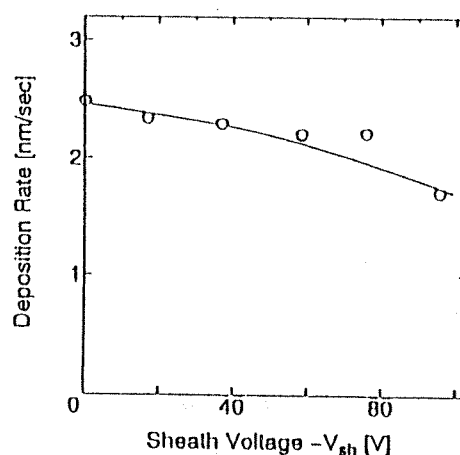


Fig.5 Dependence of the deposition rate on

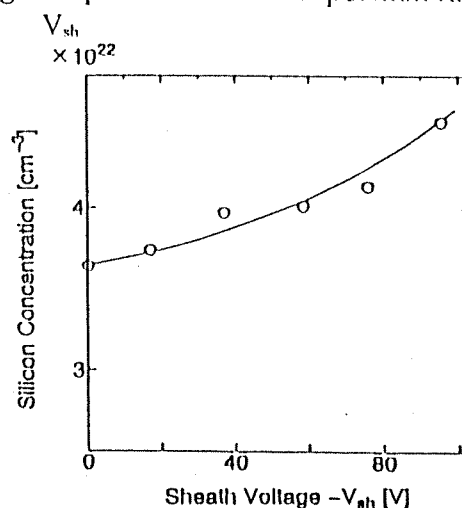


Fig.6 Dependence of the Si concentration on  $V_{sh}$

#### 4. Conclusion

The  $V_{sh}$  changes with varying  $V_{dc}$ . It has been clear that  $V_{sh}$  is controlled from 0[V] to -95[V] by using the substrate table which area is 40[cm<sup>2</sup>]. When  $V_{sh}$  is 0[V], a-Si:H films can be fabricated under the condition that the ion bombardment energy is zero. The ion bombardment has the effect to make the film properties good because the film surface is heated. However, the ion bombardment has another effect to cut the bond in the film because the Ar atoms are implanted in the film. Thus the effect of the ion bombardment has both merits and demerits.

#### 5. Acknowledgement

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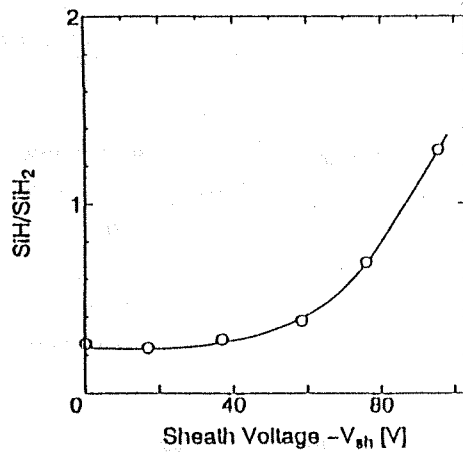


Fig. 7 Dependence of the ratio of the SiH bond density to the SiH<sub>2</sub> bond density on  $V_{sh}$

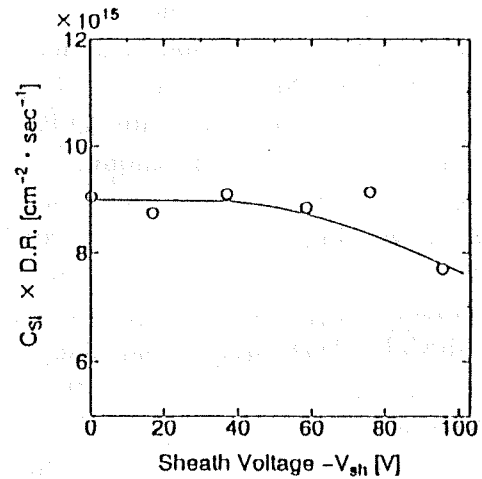


Fig. 8 Dependence of the amount of Si deposited per unit area and unit time on  $V_{sh}$

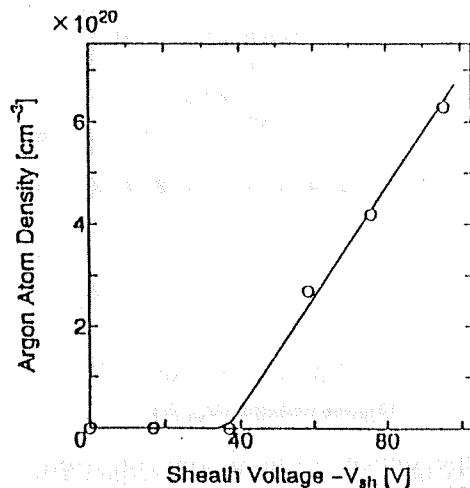


Fig. 9 Dependence of the Ar atom density on  $V_{sh}$

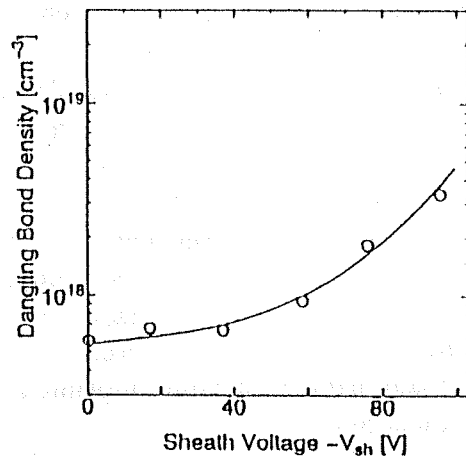


Fig. 10 Dependence of the dangling bond density on  $V_{sh}$

# マイクロ波プラズマ中に設置した電極の電位がプラズマパラメータに与える影響

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Dependence of Plasma Parameters on Electric Potential of Electrode in Microwave Plasma

Isamu KATO<sup>†</sup>, Toru MATSUSHITA<sup>†</sup>, and Makoto YAMASHITA<sup>†</sup>

あらまし 筆者らは、これまで2重管式同軸線路形マイクロ波プラズマCVD (MPCVD) の研究を行ってきている。本 MPCVD 装置の放電管部は溶融石英製の外側放電管とステンレス製の内管の2重管構造となっている。筆者らは、以前に、本 MPCVD 装置において、空間的アフターグロープラズマ中に設置した基板の電位を変化させることにより、電子密度、電子温度は変化させずにイオン衝撃エネルギーを制御できることを明らかにしている。本研究では、放電プラズマ中に設置されている内管の電位を変化させてもイオン衝撃エネルギーを制御できることを明らかにした。しかしながら、電子密度、電子温度は基板電位を変化させたときとは異なる傾向を示した。そこで、電子密度、電子温度についてマクスウェル・ボルツマン分布に基づく理論計算を行い、異なる傾向を示すのは、プラズマ空間電位が約 13 V から約 4 V と低下するに従い、電子が高エネルギー側から堆積室壁面で順次消滅し、その結果、電子の速度分布が変化することにより説明できることを明らかにした。

キーワード 基板電位、内管電位、イオン衝撃、プラズマパラメータ、マクスウェル・ボルツマン分布

## 1. はじめに

水素化アモルファスシリコン (a-Si: H) 膜は薄膜トランジスタなどの電子材料や太陽電池などの光子材料として用いられている。a-Si: H 膜の作製法としては、大面積化が容易である、低温プロセスであるといった特徴をもつプラズマ CVD 法が広く用いられている。この膜質を制御するためにはプラズマを制御する必要があるにもかかわらず、プラズマの研究はあまり行われていないのが現状である。プラズマ CVD において、イオン衝撃に関する問題は切り放すことのできない問題であり、筆者らは、放電プラズマを所定の領域に閉じ込めることにより、イオン衝撃の少ない空間的アフターグロープラズマ中で成膜できる2重管式同軸線路形マイクロ波プラズマCVD (MPCVD) 装置を開発し、いち早くイオン衝撃の問題に取り組んできた [1]~[5]。これらの研究において筆者らは、空間的アフターグロープラズマ中に設置した基板に印加する DC バイアス電圧を変化させることにより、基板に入射するイオンのフラックス密度を変化させずにイオン衝撃エネルギーを制御できることを明らかにしている [1]。

本研究では本 MPCVD 装置において放電プラズマ中に設置されているステンレス製の内管の電位を変化させてプラズマパラメータの測定を行い、空間的アフターグロープラズマ中に設置されている基板の電位を変化させた場合と同様にイオン衝撃エネルギーを制御できるかどうか検討した。その結果、内管電位を変化させてもイオン衝撃エネルギーを制御できることを明らかにした。しかしながら、プラズマパラメータは基板電位を変化させた場合と内管電位を変化させた場合では一部異なる傾向をもつことがわかった。そこで、この点について理論的に検討を加え、その理由を明らかにした。

2. 実験

## 2. 実験

図1に実験に用いた MPCVD 装置の概略図を示す。本装置の放電管部は、溶融石英製の外側放電管 (outer discharge tube) とステンレス製の内管 (inner tube)

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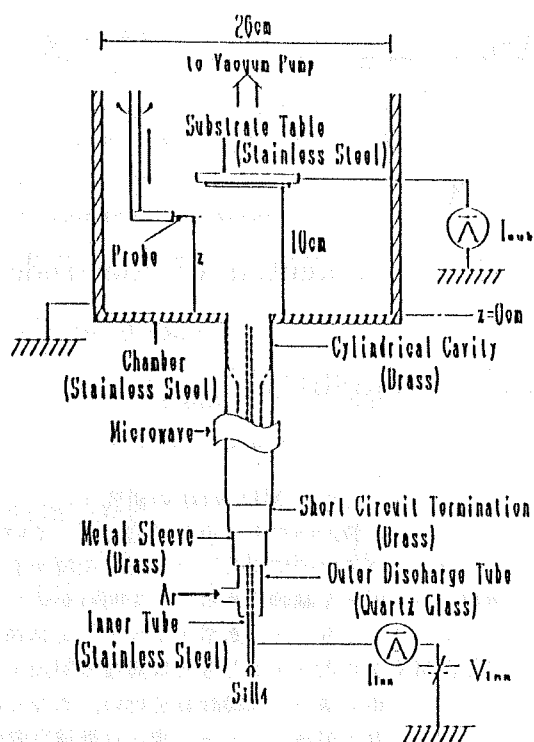


图 1 实验装置概略图

Fig. 1 Schematic diagram of experimental system.

の2重管構造となっている。外側放電管にArガスを流し、内管に $\text{SiH}_4$ ガスを流す。マグネトロンで発振した2.45 GHzのマイクロ波(microwave)は、方形導波管内を伝搬し、金属製円筒キャビティ(cylindrical cavity)に導かれる。Arガスはキャビティ領域においてマイクロ波電力により電離される。 $\text{SiH}_4$ ガスはステンレス製の内管により放電管端まで導かれ、Arプラズマ中に混入され、Arプラズマの粒子と衝突し、解離される。本MPCVD装置ではマイクロ波電力は円筒キャビティ内に閉じ込められており、堆積室内には、マイクロ波電力が注入されていない空間的アフターグロープラズマがフローと拡散により生成されている。本装置の詳細については文献[2], [3], [4]を参照されたい。筆者らはこれまでに内管と堆積室壁をアースして基板電位を変化させて研究を行ってきたが[1], 本研究では基板と堆積室壁をアースして内管電位を変化させている。ここで、内管電位を $V_{inn}$ 、基板電位を $V_{sub}$ 、内管に流れる電流を $I_{inn}$ 、基板に流れる電流を $I_{sub}$ 、放電管端からの管軸方向の距離を $z$ と定義する(図1参照)。

実験条件を以下に述べる。マイクロ波電力を 150 W とした。基板を  $z=10$  cm の位置に設置した。  $V_{inn}$  が  $\pm 40$  V を越えると、空間的アフターグロープラズマ内の発光状態が変化することから、内管と堆積室壁の間

で直流放電が起こり、プラズマ中に電力が注入されていることがわかる。更に、 $V_{inn}$  が  $-30$  V を越えると内管が Ar イオンによりスパッタリングされ、ステンレス製の内管壁から飛び出した金属原子が放電管に付着するためマイクロ波放電の状態が変化する。そこで、本研究では直流放電が起きず、かつ内管がスパッタリングされない  $-30$  V から  $+40$  V の範囲で  $V_{inn}$  を変化させた。このとき、 $V_{sub}$  は  $0$  V とした。プラズマパラメータの測定をシングルプローブ法を用い純 Ar プラズマ中 (Ar ガス流量:  $110$  ml/min) および a-Si: H 膜作製時と同一条件の Ar/SiH<sub>4</sub> プラズマ中 (Ar ガス流量:  $110$  ml/min, SiH<sub>4</sub> ガス流量:  $30$  ml/min) で行った。プローブには直径  $0.05$  cm, 長さ  $0.3$  cm の円筒プローブを用いた。なお、測定は堆積室の中心軸上の  $z=3, 5, 7, 9$  cm の位置で行った。

反応性プラズマである Ar/SiH<sub>4</sub> プラズマ中におけるプローブ計測は、プローブ表面に膜が堆積してしまうため、通常の方法ではできない。筆者らはこれまでに Ar/SiH<sub>4</sub> プラズマ中でも行えるプローブ計測法を確立している [5]。本研究でもこの方法を用いて Ar/SiH<sub>4</sub> プラズマ中での計測を行った。

なお、本論文では、既に報告している電子密度、電子温度、プラズマ空間電位、 $I_{sub}$  の  $V_{sub}$  依存性についても再現性をみるために測定しなおした。その結果は、以前報告した結果とよく一致していた。また、 $I_{inn}$  の  $V_{sub}$  依存性は以前には測定しておらず、今回初めて測定したものである。

### 3. 結果と考察

図2に  $I_{inn}$  の  $V_{sub}$  依存性と  $V_{inn}$  依存性を示す。なお、電子電流を正にとる。図より、 $V_{sub}$  を変化させると、 $I_{inn}$  は  $V_{sub}$  が負の領域ではほとんど変化しないが、 $V_{sub}$  が正の領域では、 $V_{sub}$  を増加させるに従い急激に減少することがわかる。 $V_{sub}$  が負の領域で  $I_{inn}$  が変化しないのは内管表面のシース電圧が変化しないためであると考えられる。 $V_{sub}$  が正の領域で  $I_{inn}$  が急激に減少するのは、内管表面のシース電圧が急激に増加するためであると考えられる。一方、 $V_{inn}$  を変化させた場合は、 $V_{inn}$  を増加させるに従い、 $I_{inn}$  は急激に増加し、その後飽和する。 $I_{inn}$  が急激に増加するのは内管表面のシース電圧が急激に減少するからであり、 $I_{inn}$  が飽和するのは、内管表面のシース電圧の変化が小さくなるからであると考えられる。図より、 $I_{inn}$  の  $V_{sub}$  依存性と  $V_{inn}$  依存性はほぼ対称形になっていることが

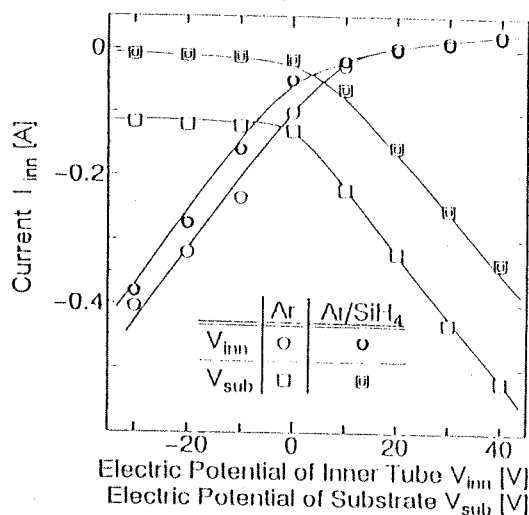


図2  $I_{inn}$  の  $V_{inn}$  依存性と  $V_{sub}$  依存性  
Fig. 2 Dependence of  $I_{inn}$  on  $V_{inn}$  and  $V_{sub}$ .

わかる。

次に、 $\text{SiH}_4$ ガスを混入させると両者共に  $I_{inn}$ が増加する理由について検討する。まず、図1の装置の概略図から明かなように、内管の表面積は堆積室の内壁の面積、更に基板テーブル面積より小さい。ガス流は図1上で上向きとなっており、Arプラズマは上方に流れている。ここで、 $\text{SiH}_4$ ガスを混入させると、Arイオンは  $\text{SiH}_4$ の解離に使われ、更にはチャージトランスファにより減少する。すなわち、シラン系のイオンや水素イオンが増加することになる。これらのArイオンより軽いイオンは、ガス流によって上方に流されると共に拡散により堆積室の内壁あるいは基板テーブルに到達しやすくなる。従って、内管に流れるイオン電流は減少するので、 $I_{inn}$ は増加すると考えられる。しかし、 $V_{inn}$ を変化させた場合、 $V_{inn}$ が約15 Vより大きい範囲では  $\text{SiH}_4$ ガスを混入させても、混入していない場合と一致している。これは、イオン電流が小さくなり、電子電流が主となるため、イオンの種類には依存しなくなるためである。

図3に  $I_{sub}$  の  $V_{sub}$  依存性と  $V_{inn}$  依存性を示す。なお、図3においても図2と同様に電子電流を正にとる。図より、 $V_{sub}$ を増加させるに従い、 $I_{sub}$ は  $V_{sub}$ が約-10 V以下のとき、緩やかに増加し、約-10 Vから約20 Vのとき、急激に増加し、その後飽和することがわかる。一方、 $V_{inn}$ を変化させた場合、 $V_{inn}$ を増加させるに従い、 $I_{sub}$ は急激に減少し、その後一定となることわかる。図より  $I_{sub}$  の  $V_{sub}$  依存性と  $V_{inn}$  依存性はほぼ対称形となっていることがわかる。

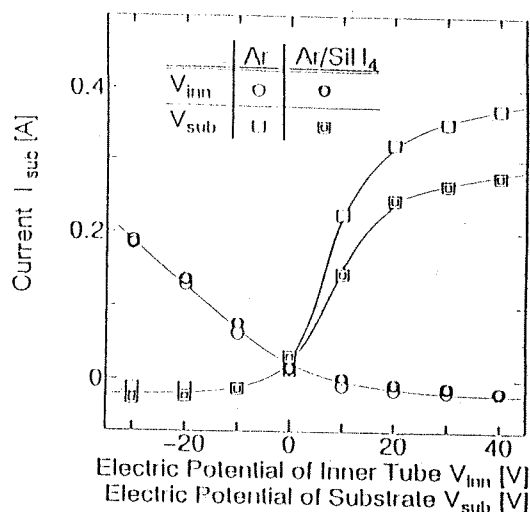


図3  $I_{sub}$  の  $V_{inn}$  依存性と  $V_{sub}$  依存性  
Fig. 3 Dependence of  $I_{sub}$  on  $V_{inn}$  and  $V_{sub}$ .

すなわち、図2、図3より内管電位 ( $V_{inn}$ ) を変化させることにより、基板電位 ( $V_{sub}$ ) を変化させたときと同様にイオン衝撃エネルギーを制御できるであろうことが推察できる。

次にプローブ計測の結果を示す。図4は  $z=3$  cm におけるプラズマ空間電位 ( $V_s$ ) の  $V_{sub}$  依存性と  $V_{inn}$  依存性である。 $V_{sub}$  を変化させた場合は、 $V_{sub}$  を増加させるに従い、 $V_{sub}$  が負の領域では  $V_s$  はわずかに増加し、 $V_{sub}$  が正の領域では急激に増加することがわかる。一方、 $V_{inn}$  を変化させた場合には、 $V_s$  は  $V_{inn}$  を増加させるに従い急激に増加することがわかる。なお、他の測定位置においても同様な結果を得ている。

また、図より  $V_{sub}$  を負にしたとき、 $V_s$  の減少は小さく約13 Vまでしか減少しないが、 $V_{inn}$  を負にした場合には、 $V_s$  は減少しつづき約4 Vまで減少することがわかる。これは、基板が電子密度、電子温度の低い空間的アフターグロープラズマ中に設置されているのに対し、内管は電子密度、電子温度の高い放電プラズマ中に設置されているため、 $V_{inn}$  が  $V_s$  に強く影響を与えるためである。

基板表面のシース電圧 ( $V_{sh,sub}$ ) は、シース端における  $V_s$  と  $V_{sub}$  の差を取ることで求められる。シース厚は数ミリであるので基板から数ミリの位置で  $V_s$  の測定をする必要がある。しかしながら、本実験において  $V_s$  の  $z$  方向へのこう配は、わずかであるのでシース端における  $V_s$  は  $z=9$  cm における  $V_s$  で近似できる[1]。そこで、 $z=9$  cm における  $V_s$  と  $V_{sub}$  の差を取ることで  $V_{sh,sub}$  を求める。図5にその結果を示

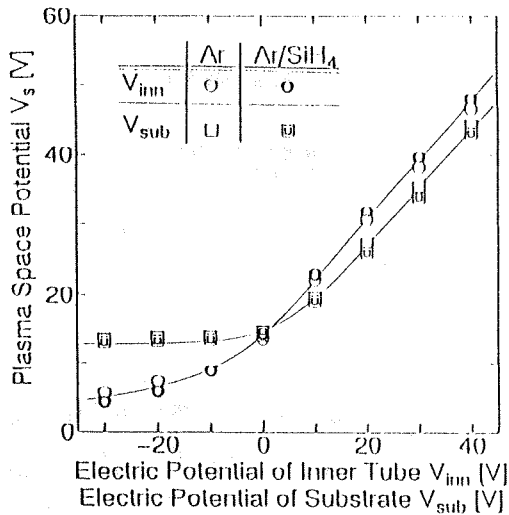


図4  $V_s$  の  $V_{inn}$  依存性と  $V_{sub}$  依存性  
Fig. 4 Dependence of  $V_s$  on  $V_{inn}$  and  $V_{sub}$ .

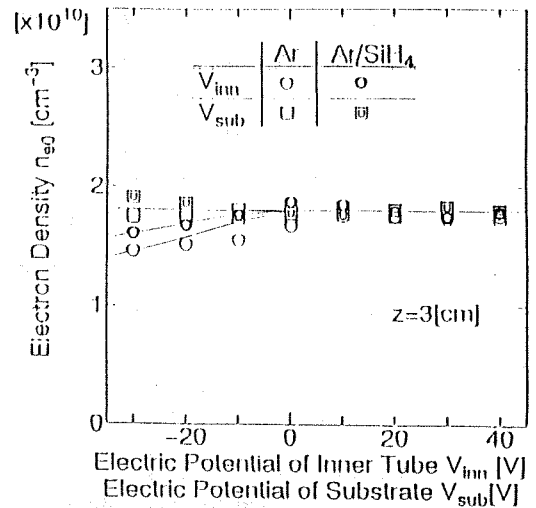


図6  $n_{eo}$  の  $V_{inn}$  依存性と  $V_{sub}$  依存性  
Fig. 6 Dependence of  $n_{eo}$  on  $V_{inn}$  and  $V_{sub}$ .

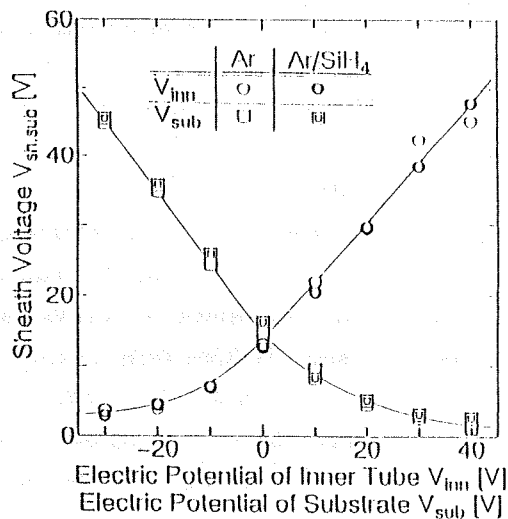


図5  $V_{sh,sub}$  の  $V_{inn}$  依存性と  $V_{sub}$  依存性  
Fig. 5 Dependence of  $V_{sh,sub}$  on  $V_{inn}$  and  $V_{sub}$ .

す。ここで、 $V_{sh,sub}$  の  $V_{inn}$  依存性は  $V_{sub}$  を 0 V としているので  $z=9$  cm における  $V_s$  の  $V_{inn}$  依存性と同じである。図より、 $V_{sub}$  を変化させた場合は、 $V_{sub}$  を増加させるに従い  $V_{sh,sub}$  は減少することがわかる。この結果は  $V_{sub}$  を増加させるに従い、イオン衝撃エネルギーは減少することを示している。一方、 $V_{inn}$  を変化させた場合には、 $V_{sh,sub}$  は  $V_{inn}$  を減少させるに従い減少することがわかる。この結果は  $V_{inn}$  を減少させるに従い、イオン衝撃エネルギーは減少することを示している。以上の結果より、 $V_{inn}$  を変化させても、イオン衝撃エネルギーを制御できることがわかる。

また、イオン衝撃エネルギーは  $V_{inn}$  を変化させた場

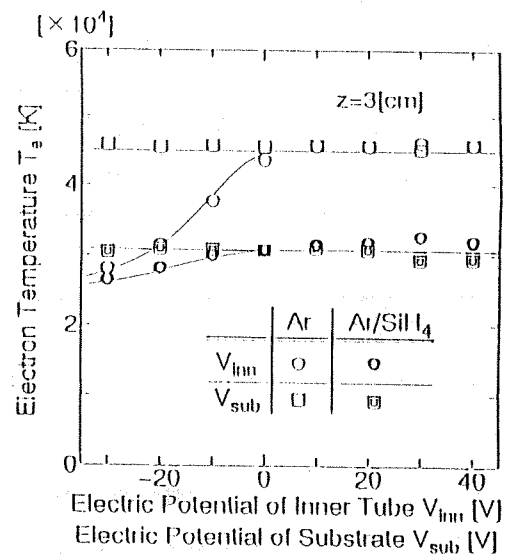


図7  $T_e$  の  $V_{inn}$  依存性と  $V_{sub}$  依存性  
Fig. 7 Dependence of  $T_e$  on  $V_{inn}$  and  $V_{sub}$ .

合には  $V_{inn}$  を -30 V にしたとき、約 3 eV まで低減でき、 $V_{sub}$  を変化させた場合には  $V_{sub}$  を +40 V にしたとき、約 3 eV まで低減できることがわかる。しかしながら、 $V_{sub}$  と  $V_{inn}$  のどちらを変化させてもイオンを跳ね返すような電界は形成されないこともわかる。

図6に  $z=3$  cm における電子密度 ( $n_{eo}$ ) の  $V_{sub}$  依存性と  $V_{inn}$  依存性を示す。図より  $n_{eo}$  は  $V_{sub}$  を変化させても変化しないことがわかる。一方、 $V_{inn}$  を変化させた場合、 $n_{eo}$  は  $V_{inn}$  が負の領域で  $V_{inn}$  を 0 V に近づけるに従いやや増加し、 $V_{inn}$  が正の領域では変化しないことがわかる。他の測定位置においても同様な結

果を得ている。

図7に $z=3\text{ cm}$ における電子温度( $T_e$ )の $V_{sub}$ 依存性と $V_{inn}$ 依存性を示す。図より、 $T_e$ は $V_{sub}$ を変化させても変化しないことがわかる。一方、 $V_{inn}$ を変化させた場合、 $T_e$ は $V_{inn}$ が負の領域で $V_{inn}$ を0Vに近づけるに従い増加し、 $V_{inn}$ が正の領域では変化しないことがわかる。この結果は他の測定位置においても同様である。

また、図より、Ar/SiH<sub>4</sub>プラズマの $T_e$ のほうが、純Arプラズマの $T_e$ よりも低くなっていることがわかる。これはAr/SiH<sub>4</sub>プラズマは分子ガスであるSiH<sub>4</sub>ガスをArプラズマに混入して生成されているため、SiH<sub>4</sub>の解離に伴う非弾性衝突が増加しているからである[5]。

以上のように、 $V_{sub}$ と $V_{inn}$ 、すなわち、放電プラズマ中に設置した電極の電位( $V_{inn}$ )と空間的アフターグロープラズマ中に設置した電極の電位( $V_{sub}$ )は $V_s$ に対しほぼ同様な影響を与えることを明らかにした。しかし、 $n_{e0}$ と $T_e$ は $V_{sub}$ を変化させた場合は変化しないのに対し、 $V_{inn}$ を変化させた場合には、 $V_{inn}$ が負の領域で $V_{inn}$ を負に増加させるに従い減少することを実験的に明らかにした。そこで、この異なる傾向を示す理由について次に検討する。

電子の速度分布は一般にマクスウェル・ボルツマン分布となっている。

$$n_e(v) = 4\pi n_{e0} \left( \frac{m_e}{2\pi k T_e} \right)^{3/2} v^2 \exp\left( -\frac{m_e v^2}{2k T_e} \right) \quad (1)$$

ここで、 $k$ はボルツマン定数、 $m_e$ は電子の質量、 $T_e$ は電子温度、 $v$ は電子の速度、 $n_{e0}$ は全電子密度、 $n_e(v)$ は速度 $v$ をもつ電子の密度である。ここで

$$\frac{1}{2} m_e v^2 = eV \quad (2)$$

であるので、式(1)は

$$n_e(V) = 8\pi n_{e0} \left( \frac{m_e}{2\pi k T_e} \right)^{3/2} \frac{eV}{m_e} \exp\left( -\frac{eV}{k T_e} \right) \quad (3)$$

となる。ここで、 $e$ は電気素量、 $V$ は電圧である。堆積室壁面のシース電圧、すなわち $V_s$ が十分大きければほとんどすべての電子が堆積室壁面で跳ね返されてしまうが、 $V_s$ が小さくなるに従い、マクスウェル・ボルツマン分布に従う電子は高エネルギー側の電子から順次、堆積室壁面に到達し、壁面でイオンと再結合することにより消滅することになる。

図8の実線は $V_s$ が十分大きいとき( $V_{inn} > 0$ )の $n_{e0}$ 、 $T_e$ の実験値を式(3)に代入し得られた電子の速

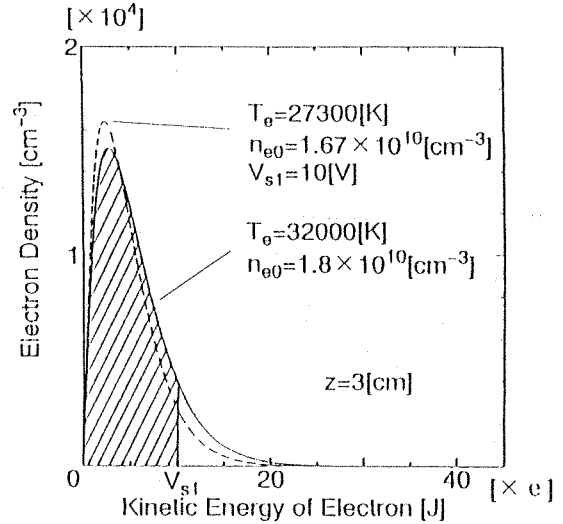


図8 マクスウェル・ボルツマン分布  
Fig. 8 Maxwell-Boltzmann's distribution.

度分布である。但し、実験値には $z=3\text{ cm}$ における値を用いた。次に、 $V_s$ が小さくなり図中の $V_{s1}$ となったとき、 $eV_{s1}$ より小さい運動エネルギーをもつ電子はシース電圧によって跳ね返されるが、これより大きい運動エネルギーをもつ電子はシース電圧に打ち勝って堆積室壁面で消滅すると考えられる。従って、 $V_s$ が $V_{s1}$ のときの電子密度 $n'_{e0}$ は図8の斜線部を積分したものであり次式で与えられる。

$$n'_{e0} = \int_0^{V_{s1}} n_e(V) dV \quad (4)$$

図8の斜線部のような分布になった電子群は、他の粒子と衝突しながら堆積室内を拡散し図8の破線で示すように再びマクスウェル・ボルツマン分布になると考えられる。この再分布したときの電子温度を $T'_e$ とすると、 $n_e(V)'$ は次式で与えられる。

$$n_e(V)' = 8\pi n'_{e0} \left( \frac{m_e}{2\pi k T'_e} \right)^{3/2} \frac{eV}{m_e} \exp\left( -\frac{eV}{k T'_e} \right) \quad (5)$$

このとき、プラズマ中の全電子のもつエネルギーは保存されることより、

$$\int_0^{V_{s1}} n_e(V) eV dV = \int_0^{\infty} n_e(V)' eV dV \quad (6)$$

が成り立つ。すなわち、式(5)、(6)を連立することにより1次近似として $T'_e$ を求めることができる。

図9に式(4)より求めた電子密度と実験値を比較した結果を、図10に式(5)、(6)を連立させることにより求めた電子温度と実験値を比較した結果をそれぞれ示す。両図において実線が理論計算の結果である。これらの図から、 $V_s$ が小さいとき( $V_{inn} < 0$ )に $n_{e0}$ 、 $T_e$ が小さくなるという実験結果が前述の理論によって説



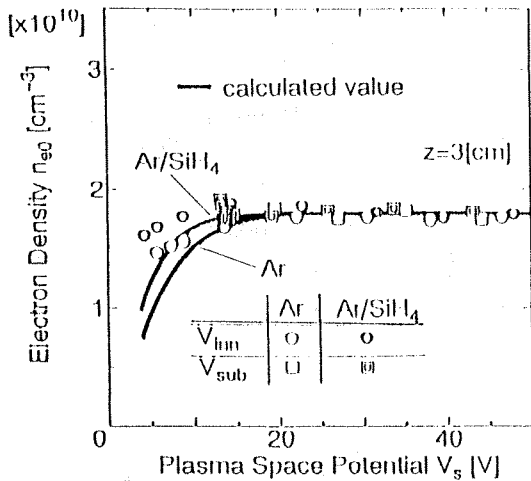


図9  $n_{e0}$  の計算値と実験値の比較  
Fig. 9 Comparison of calculated values with experimental values of  $n_{e0}$ .

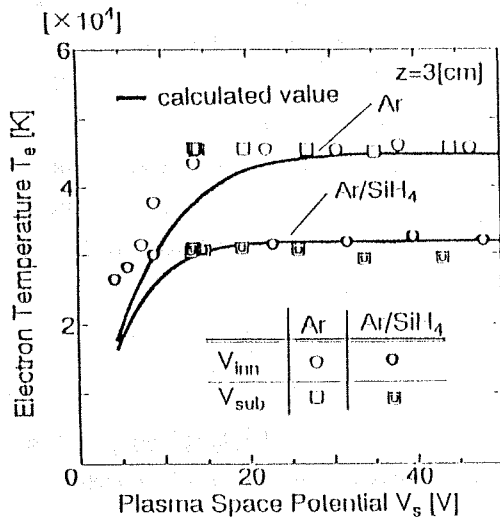


図10  $T_e$  の計算値と実験値の比較  
Fig. 10 Comparison of calculated values with experimental values of  $T_e$ .

明できることがわかる。

図9, 図10において計算結果と実験結果は  $V_s$  が小さくなると  $n_{e0}$  と  $T_e$  が減少するという傾向は同じであるが理論計算の結果は減少傾向が大きい。これは先に述べたような反応は堆積室内全空間で起こるのではなく堆積室壁面でのみ起こる反応であるが、理論計算では全空間で高エネルギー電子が堆積室壁面に到達し消滅するとして計算したため計算結果が実験結果より小さく算出されたためである。これらの結果より  $V_{sub}$  を変化させた場合に  $n_{e0}$ ,  $T_e$  が変化しないのは、 $V_{sub}$  を負にしても  $V_s$  は13V程度までしか減少しないた

め(図4参照), 堆積室壁面における電子の消滅がほとんどなく電子の速度分布は変わらないからである。一方,  $V_{inn}$  を変化させた場合に  $n_{e0}$ ,  $T_e$  が変化するのは,  $V_{inn}$  を負にすると  $V_s$  は4V程度まで大きく減少するため(図4参照), 堆積室壁面において高エネルギー側の電子が多量に消滅するので, 電子密度は減少し, 電子温度は低下することを明らかにした。

#### 4. む す び

2重管式同軸線路形マイクロ波プラズマCVD装置において, 基板電位 ( $V_{sub}$ ) および内管電位 ( $V_{inn}$ ) を変化させてプラズマパラメータの測定を行った結果, 以下のことが明らかになった。

(1) プラズマ空間電位 ( $V_s$ ) は,  $V_{sub}$  を増加させるに従い,  $V_{sub}$  が負のとき, わずかに増加し,  $V_{sub}$  が正のとき急激に増加する。  $V_{inn}$  を変化させた場合,  $V_{inn}$  を増加させるに従い,  $V_s$  は急激に増加する。  $V_{sub}$  を変化させた場合,  $V_{sub}$  を負にしても  $V_s$  は約13Vまでしか減少しないのに対し,  $V_{inn}$  を変化させた場合,  $V_{inn}$  を負にすると  $V_s$  は約4Vまで減少する。

(2)  $V_{sub}$  を変化させた場合は,  $V_{sub}$  を増加させることによりイオン衝撃エネルギーを低減できる。  $V_{inn}$  を変化させた場合には  $V_{inn}$  を減少させることによりイオン衝撃エネルギーを低減できる。

(3)  $V_{sub}$  を変化させた場合は, 電子密度 ( $n_{e0}$ ), 電子温度 ( $T_e$ ) は変化しない。  $V_{inn}$  を変化させた場合には,  $n_{e0}$ ,  $T_e$  は  $V_{inn}$  が負の領域で,  $V_{inn}$  を負に増加させるに従い減少する。

(4)  $n_{e0}$ ,  $T_e$  の上述の(3)における変化は,  $V_s$  が小さくなるに従いマクスウェル・ボルツマン分布の高エネルギー電子から順次堆積室壁面で消滅するため電子密度は減少し, 更にプラズマ中の全電子のもつ平均エネルギーが減少するためとして説明できることを明らかにした。

(5) イオン衝撃エネルギーを制御する方法としては基板電位を変化させる方法が一般的であるが, 基板をアースした場合, または基板がアースされてしまう場合にも, マイクロ波プラズマ中の他の電極 (内管) の電位を変化させてイオン衝撃エネルギーを制御できることを明らかにした。

今後,  $V_{inn}$  を変化させて a-Si:H 膜を作製し,  $V_{sub}$  を変化させた場合と比較検討する予定である。

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## Control of Radical Species in Microwave Plasma Chemical Vapor Deposition

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### SUMMARY

The spatial distributions of electron temperature and density in pure Ar plasma in a double-tubed coaxial-line type microwave plasma chemical vapor deposition (CVD) system were measured using the probe method. It was found that the electron temperature and electron density dropped sharply in an area 4 cm from the edge of the discharge tube and they decreased slowly in an area farther away from the forementioned area.  $\text{SiH}_4$  gas was dissociated in Ar plasma, and the electron temperature and density of the plasma were varied by changing the location of the  $\text{SiH}_4$  gas inlet. As a result, it was found that the fragmentation pattern of radical species could be varied by changing the location of the  $\text{SiH}_4$  gas inlet.

In addition, films were fabricated under various fragmentation patterns and the qualities of these films were evaluated. It was found that the film quality could be improved by dissociating  $\text{SiH}_4$  gas at low electron temperature.

**Key words:** Microwave plasma CVD; electron temperature; fragmentation pattern; a-Si:H film.

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### 1. Introduction

Hydrogenated amorphous silicon (a-Si:H) films have been used widely for optical and electronic devices and considerable effort has been made to improve the film quality and to find applications of these films for new devices. An a-Si:H film can be deposited on a large-area substrate using the low-temperature plasma chemical vapor deposition (CVD) technique.

To improve the quality of a film fabricated by plasma CVD, it is important to understand reactions in gas and on the film surface. For this purpose, it is necessary to investigate the behavior of radical species and the measurement methods such as LIF [1], IRLAS [2], and so forth. In addition, by comparing the result of evaluating the film formed by only  $\text{SiH}_3$  radicals with the result of simulation, the probability of the  $\text{SiH}_3$  radical becoming a film and the film surface loss probability have been studied [3].

In this paper, the electron temperature and electron density were changed by changing the location of the  $\text{SiH}_4$  gas inlet to Ar plasma. Using Ar plasma with various electron temperatures and electron densities,  $\text{SiH}_4$  gas was dissociated to investigate the ratio among the numbers of radical species, that is, fragmentation pattern. As a result, it was found that the fragmentation pattern of radical species could be changed by changing the location of the  $\text{SiH}_4$  gas inlet. Films were grown under various

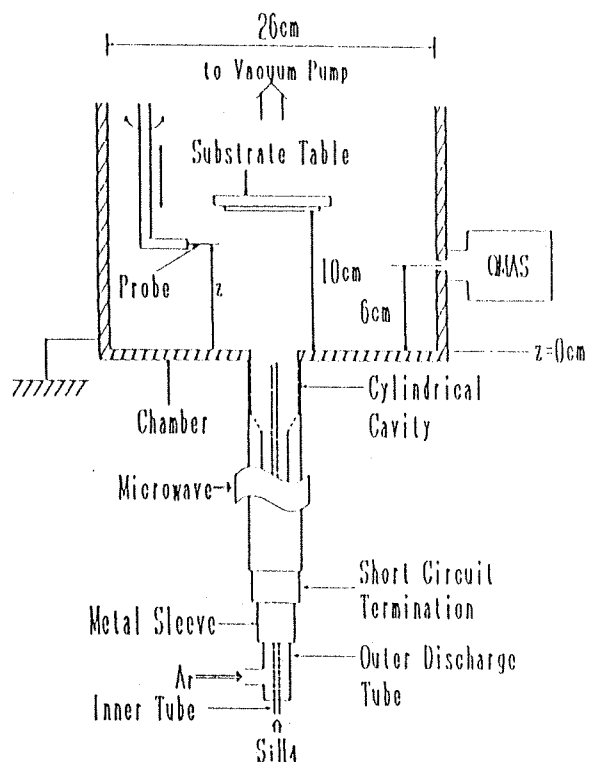


Fig. 1. Schematic diagram of experimental system.

fragmentation patterns and then evaluated. It was found that film quality could be improved.

## 2. Experiment

The double-tubed coaxial-line-type microwave plasma CVD (MPCVD) system was used in this paper. Figure 1 illustrates the CVD system. Ar gas flows in the outer discharge tube made of fused silica to generate Ar plasma by microwave power. The microwave is coupled with plasma under the fundamental mode of the coaxial line. Since the microwave power is confined in the cylindrical cavity, the discharge plasma is generated only in the cylindrical cavity and flows into the deposition chamber.  $\text{SiH}_4$  gas is led through a stainless steel inner tube to the discharge tube end where it is mixed with Ar plasma. Then,  $\text{SiH}_4$  gas is dissociated due to collision with Ar plasma particles. Details of this system are reported in [4] and [5].

The distance from the discharge tube end in the direction along the center axis is defined by  $z$ .

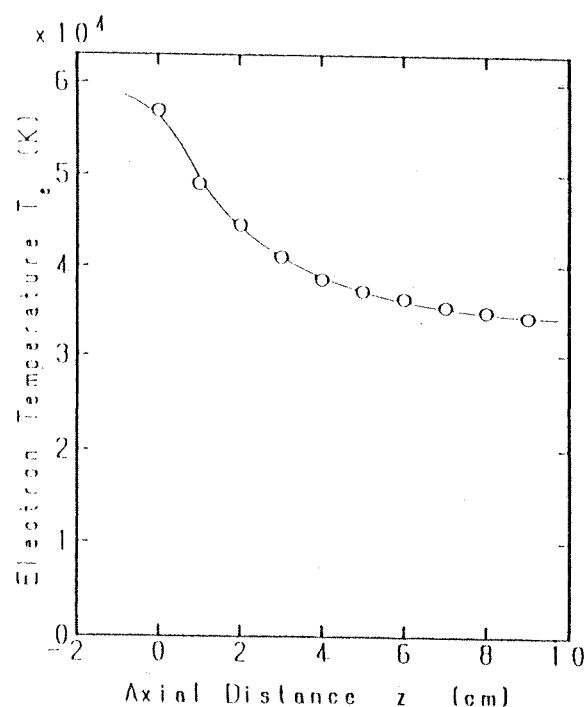


Fig. 2. Dependence of electron temperature on  $z$ .

The substrate table is located at  $z = 10$  cm. This location is the spatial afterglow plasma region where no microwave power is provided. Therefore, a film can be grown from radicals without ion bombardment at this location [5]. A cylindrical probe with a diameter of 0.05 cm and length of 0.3 cm is used to measure the electron temperature and density. The probe is installed on a movable shaft and its location can be changed in the deposition chamber. A quadrupole mass spectrometer (QMAS) is located at  $z = 6$  cm outside the chamber and it is connected to the inside of the chamber via an orifice with a diameter of 200  $\mu\text{m}$  (see Fig. 1).

The discharge condition is as follows. Microwave power of 150 W was used for probe measurement where the Ar gas flow was 110 ml/min and the gas pressure in the chamber was about 3.5 mtorr. The probe measurement was carried out along the center axis of the chamber at  $z = 0 \sim 9$  cm. The same condition was used for the QMAS analysis and film deposition. During film deposition, the  $\text{SiH}_4$  gas flow as 50 ml/min and the gas pressure was about 5 mtorr. The location of the  $\text{SiH}_4$  gas inlet was varied from  $z = -2$  cm to  $z = 3$  cm to vary the electron temperature and density.

The film thickness was measured by using a needle-type film-thickness measurement apparatus. The

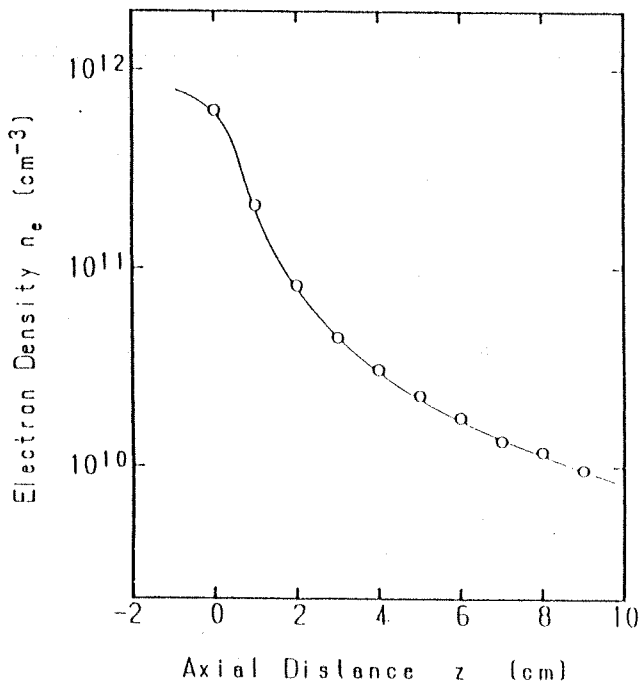


Fig. 3. Dependence of electron density on  $z$ .

atomic density of Si in the film was measured by Rutherford backscattering spectra. The integrated intensities of stretching modes of SiH and SiH<sub>2</sub> bonds were obtained by using the infrared absorption spectra and film thickness. By multiplying these intensities by  $1.4 \times 10^{20} \text{ cm}^{-2}$ , the hydrogen atomic densities in both bonds were calculated [6]. The optical energy gap was obtained by using the ultraviolet and visible absorption spectrum and film thickness. The dangling bond density was obtained by using the result of electron spin resonance measurement and film thickness.

### 3. Experimental Results

Figure 2 shows the dependence of electron temperature on  $z$ . The electron temperature decreases rapidly as  $z$  increases to 3 cm, and when  $z$  exceeds 3 cm, the electron temperature decreases slowly.

Figure 3 shows the dependence of electron density on  $z$ . The electron density decreases rapidly as  $z$  increases to 3 cm. When  $z$  exceeds 3 cm, the electron density decreases exponentially [7]. No experiment was carried out for the area of negative value of  $z$ , namely in the discharge tube, because the probe could not reach the

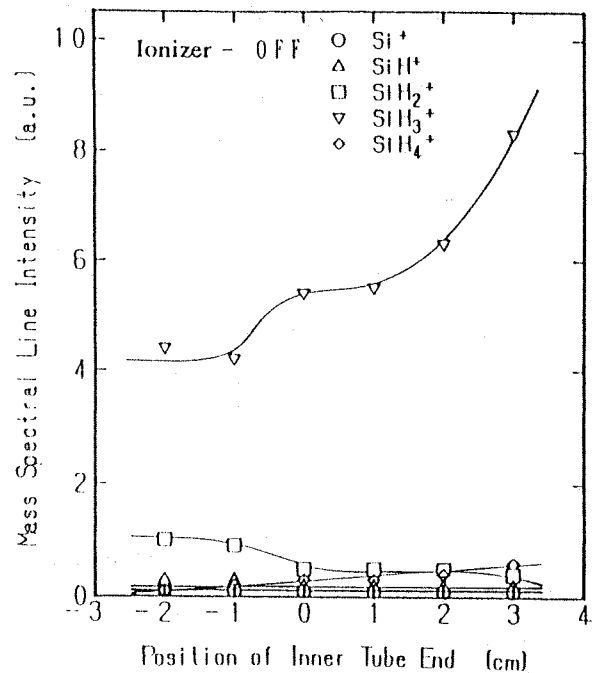


Fig. 4. Dependence of mass spectral line intensity on the position of the inner tube end (ionizer off).

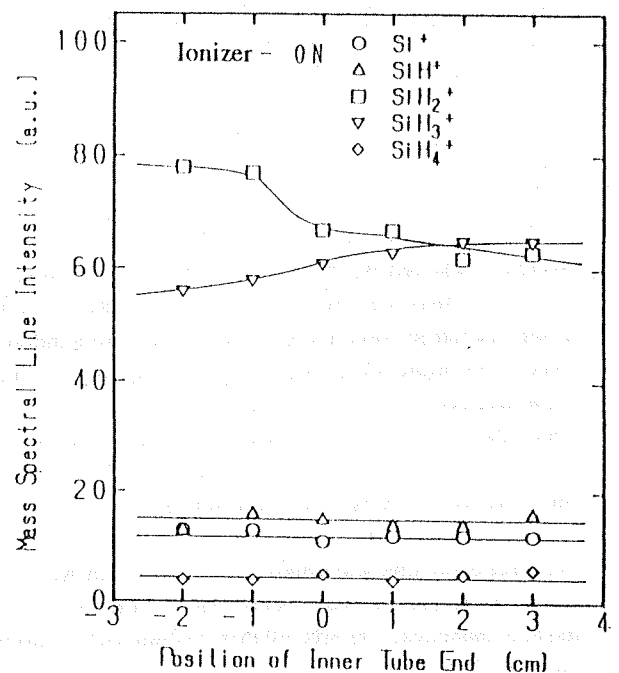


Fig. 5. Dependence of mass spectral line intensity on the position of the inner tube end (ionizer on).

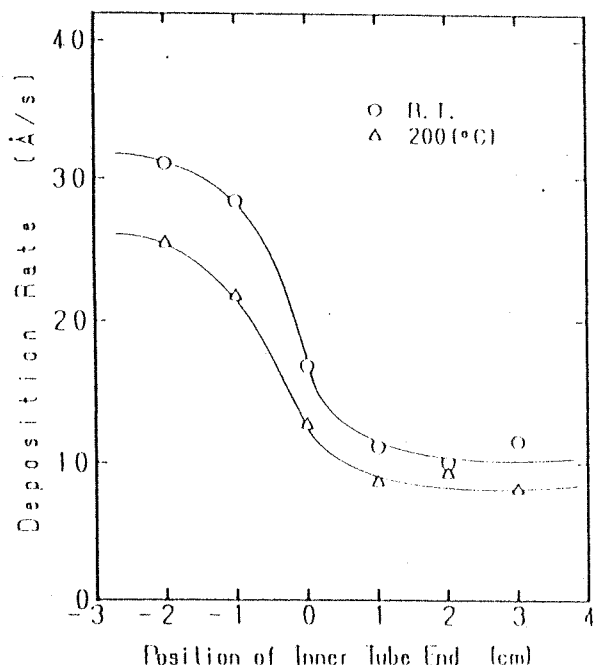


Fig. 6. Dependence of deposition rate on the position of the inner tube end.

area of a negative value of  $z$ . However, since the incident microwave power is uniform in the area of negative value of  $z$ , both electron temperature and density are believed to saturate when  $z < -2$  cm.

As described above,  $\text{SiH}_4$  gas is led to the discharge tube end via the inner tube and is dissociated by Ar plasma particles. Therefore, by changing the position of the inner tube end (the location of the  $\text{SiH}_4$  gas inlet),  $\text{SiH}_4$  gas confronts Ar plasma with various electron temperatures and densities. In this way, the fragmentation pattern of radical species can be varied.

Figures 4 and 5 show the dependence of the mass-spectral line intensity obtained by QMAS on the position of the inner tube end. Figure 4 shows the result on the ionized radicals when the ionizer is off. Figure 5 shows the result when the ionizer is on. In both results,  $\text{SiH}_2^+$  decreases and  $\text{SiH}_3^+$  increases as the position of the inner tube end moves from a negative to a positive value of  $z$ . This indicates that the fragmentation pattern can be varied by varying the position of the inner tube end in the MPCVD system.

The increase of  $\text{SiH}_2^+$  and the decrease of  $\text{SiH}_3^+$  occur because when the electron temperature and density decrease, the degree of dissociation causing ionization

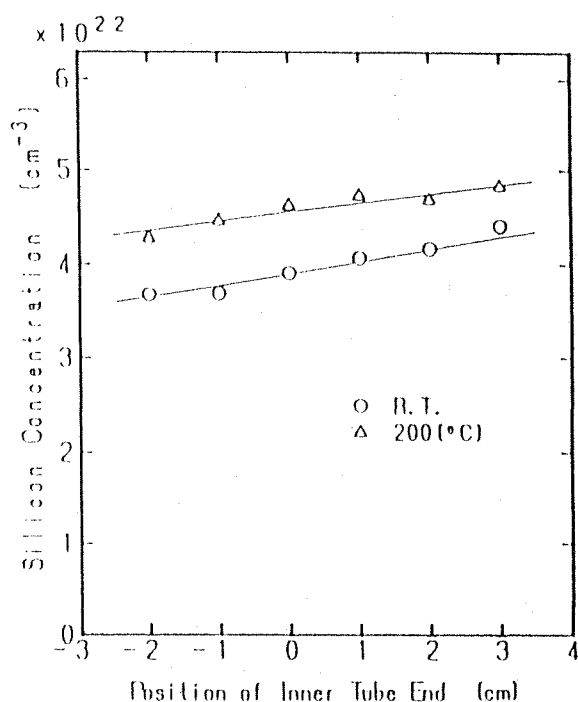


Fig. 7. Dependence of silicon concentration on the position of the inner tube end.

which generates  $\text{SiH}_2^+$  is suppressed and the degree of dissociation causing ionization which generates  $\text{SiH}_3^+$  increases. The change of ionized radicals is not always in proportion to the change of neutral radicals. However, it is considered that the former is in proportion to the latter under a weakly ionized plasma where the degree of ionization is less than several percent. Therefore, when the number of  $\text{SiH}_2$  radicals decreases, the number of  $\text{SiH}_3$  radicals increases.

It has been reported that the film quality is improved selectively introducing radicals with a high surface mobility such as  $\text{SiH}_3$  radicals [8]. Therefore, by moving the position of the inner tube end from negative to positive values of  $z$ , the film quality can be optimized; a-Si:H films were fabricated under various fragmentation patterns by changing the position of the inner tube end and the qualities of these films were evaluated.

Figure 6 shows the dependence of the deposition rate on the position of the inner tube end. The deposition rate decreases rapidly as the position of the inner tube end is moved from  $z = -1$  to  $+1$  cm regardless of the substrate temperature. When  $z$  exceeds  $+1$  cm, the deposition rate becomes constant, also regardless of the substrate temperature. This symptom is due to the large

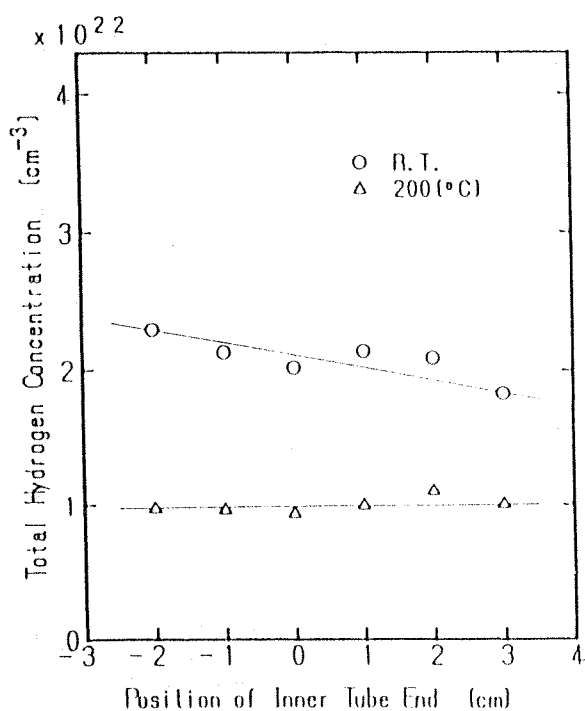


Fig. 8. Dependence of total hydrogen concentration on the position of the inner tube end.

changes in the degree of dissociation of  $\text{SiH}_4$  and fragmentation pattern. The deposition rate is constant when the position is between  $z = -1$  and  $z = -2$  cm because electron temperature and density do not change in this region. When the substrate temperature is  $200^\circ\text{C}$ , the deposition rate is lower than when it is room temperature as reported [9], because the silicon concentration in a film increases as substrate temperature increases.

Figure 7 shows the dependence of silicon concentration on the position of the inner tube end. Regardless of substrate temperature, silicon concentration increases as the position changes from a negative to a positive value of  $z$ , indicating that the film becomes more dense. The densification of the film is caused by the number of  $\text{SiH}_3$  radicals which have a high mobility. When the substrate is heated at  $200^\circ\text{C}$ , the concentration of Si is higher than when the substrate temperature is room temperature, as reported [10].

Using the results shown in Figs. 6 and 7, the amount of Si contributing to the formation of the film per unit time per unit area, which is given by silicon concentration times deposition rate, was calculated. The amount of Si in a film per unit time per unit area depends on the

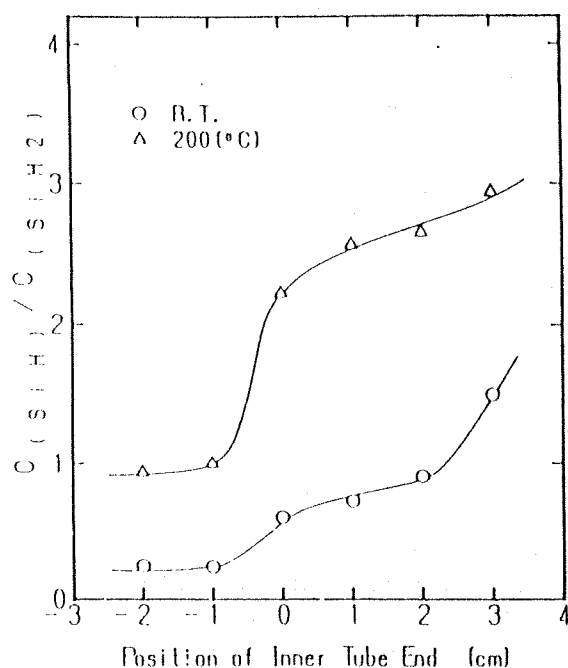


Fig. 9. Dependence of  $(\text{SiH bond density})/(\text{SiH}_2 \text{ bond density})$  ratio on the position of the inner tube end.

position of the inner tube end which is similar to the dependence of the deposition rate on the position of the inner tube end as shown in Fig. 6. Therefore, it is clear that the decrease of the deposition rate is due not only to the densification of the film.

As the position of the inner tube end is moved from a negative to a positive value of  $z$ , the deposition rate decreases because the range of the position of the tube end ( $-2 \text{ cm} < z < 3 \text{ cm}$ ) includes the transition area from the discharge plasma region where microwave power is supplied to the spatial after-glow plasma region where no microwave power is supplied. That is, in the transition area, the dissociation of  $\text{SiH}_4$  degrades and the number of  $\text{SiH}_3$  radicals with high adherence decreases because of the suppression of the dissociation of  $\text{SiH}_4$  [8], causing the increase of the number of  $\text{SiH}_3$  radicals with a low adherence [8]. The dependence of the amount of Si in a film per unit time per unit area on the position of the inner tube end is independent of the substrate temperature. Therefore, the decrease of the deposition rate by increasing the substrate temperature is caused by the densification of the film.

Figure 8 shows the dependence of total hydrogen concentration on the position of the inner tube end. As

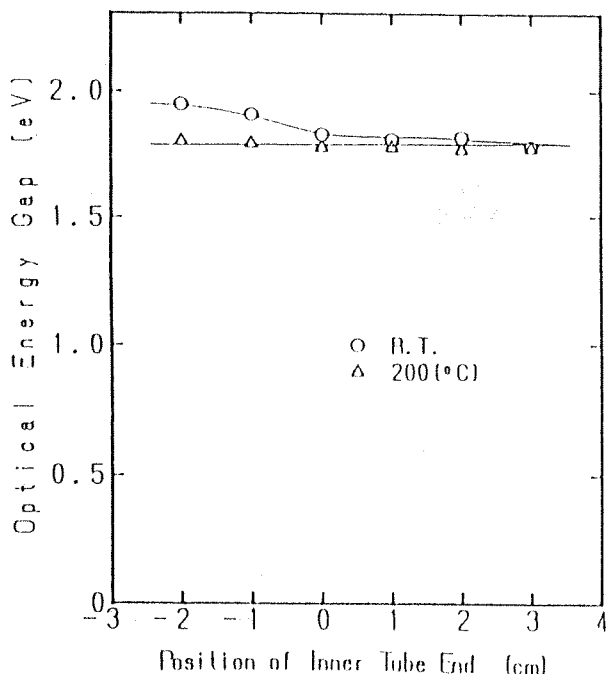


Fig. 10. Dependence of optical energy gap on the position of the inner tube end.

the position of the inner tube end moves from a negative to a positive value, the hydrogen concentration decreases. When the substrate temperature is 200°C, the hydrogen concentration is almost constant at about  $1 \times 10^{22} \text{ cm}^{-3}$ , regardless of the position of the inner tube end.

As the position of the inner tube end moves from a negative to a positive value, the SiH bond density increases and the SiH<sub>2</sub> bond density decreases. Figure 9 shows the dependence of (SiH bond density)/(SiH<sub>2</sub> bond density) ratio on the position of the inner tube end. Regardless of the substrate temperature, the a-Si:H films contain more SiH bonds as the position of the inner tube end moves from a negative to a positive value. When the substrate temperature is 200°C, the films contain more SiH bonds than when the substrate temperature is room temperature, as reported.

Figure 10 shows the dependence of the optical energy gap on the position of the inner tube end. When the substrate temperature is room temperature, the optical energy gap decreases as the position of the inner tube end moves from a negative to a positive value. When the

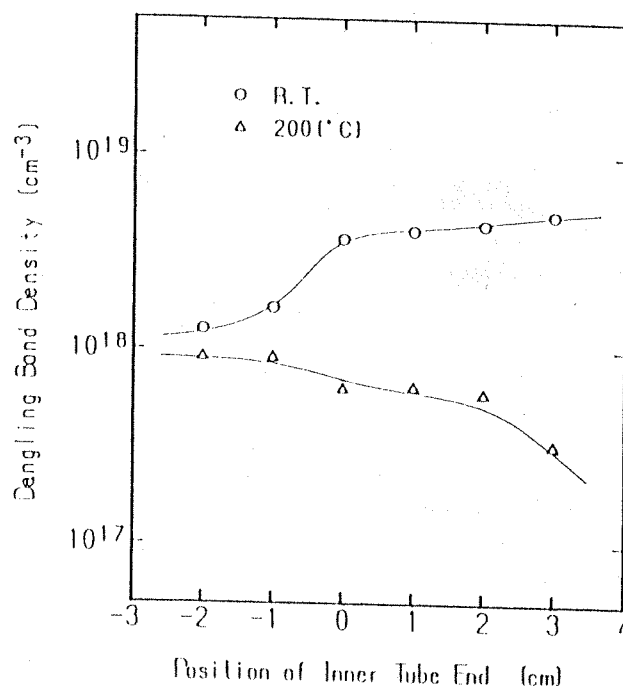


Fig. 11. Dependence of dangling bond density on the position of the inner tube end.

substrate temperature is 200°C, the optical energy gap is about 1.78 eV, regardless of the position of the inner tube end. This tendency is similar to the dependence of total hydrogen concentration on the position of the inner tube end.

Figure 11 shows the dependence of the dangling bond density on the position of the inner tube end. When the substrate temperature is room temperature, the dangling bond density increases slightly as the position of the inner tube end moves from negative to positive value. That is, when the substrate is not heated, the dangling bond density can be minimized if the number of SiH<sub>2</sub> radicals is increased by installing the position of the inner tube end at negative value. When the mobilities of radicals are increased by heating the substrate temperature at 200°C, the dangling bond density decreases and the quality of the a-Si:H film improves as the position of the inner tube end moves from negative to positive value.

The above results show that as the position of the inner tube end moves from a negative to a positive value, the film quality improves although the deposition rate decreases because of the increase in the number of SiH<sub>3</sub> radicals with high mobility.



## 4. Conclusions

The spatial distributions of electron temperature and density in pure Ar plasma in the deposition chamber of a double-tubed coaxial-line-type microwave plasma CVD system was investigated. In addition, by introducing  $\text{SiH}_4$  gas into Ar plasma at various inlet locations, namely the position of the inner tube end,  $\text{SiH}_4$  gas was dissociated by Ar plasma with different electron temperatures and densities to measure the fragmentation pattern by mass spectroscopy. As a result, the following facts were found.

(1) As  $z$  increased to about 3 cm, the electron temperature decreased rapidly. When  $z$  exceeded 3 cm, the decrease of electron temperature became slower with an increase of  $z$ .

(2) As  $z$  increased to about 3 cm, the electron density decreased rapidly. When  $z$  exceeded 3 cm, the decrease of electron density became exponential with an increase of  $z$ .

(3) As the position of the inner tube end moved from a negative to a positive value, the concentration of  $\text{SiH}_2^+$  decreased and that of  $\text{SiH}_3^+$  increased.

In addition, films were fabricated by changing the position of the inner tube end and the qualities of these films were evaluated. As the position of the inner tube end was moved from a negative to a positive value of  $z$ , the deposition rate and film quality changed as follows.

(1) The deposition rate decreased rapidly as the position of the inner tube end was moved to  $z = 1$  cm. When the position exceeded 1 cm, it saturated. This was because the degree of dissociation of  $\text{SiH}_4$  decreased and the number of  $\text{SiH}_3$  radicals with low-adhesion increased.

(2) The Si concentration, total hydrogen concentration, hydrogen bond state, and optical energy gap represented the film quality improved.

(3) As the position of the inner tube end was moved from negative to positive value, the dangling bond density increased when the substrate temperature was room temperature, but it decreased when the substrate temperature was 200°C.

The above results indicate that the film quality improved by dissociating  $\text{SiH}_4$  in plasma at lower

electron density because the number of  $\text{SiH}_3$  radicals with a high mobility increased.

In the future, the fragmentation pattern of neutral radicals should be investigated quantitatively to discuss the detailed deposition mechanism.

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# マイクロ波プラズマ CVD におけるラジカル種の制御

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## Control of Radical Species in Microwave Plasma CVD

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あらまし 純 Ar プラズマ中でグローブ法を用いて、2 重管式同軸線路形マイクロ波プラズマ CVD 装置の堆積室内における電子温度、電子密度の空間分布測定を行った。その結果、電子温度、電子密度は、放電管端から 4 cm 程度までは急激に減少し、その後、減少傾向は緩やかになることを明らかにした。SiH<sub>4</sub> ガスの混入位置を変化させることにより、電子温度、電子密度の異なる Ar プラズマ中で SiH<sub>4</sub> ガスを解離させた。その結果、SiH<sub>4</sub> ガスの混入位置を変化させることにより、ラジカルフラグメンテーションパターンを変化させることができることを明らかにした。更に、フラグメンテーションパターンを変化させて成膜し、その膜質評価を行い、低い電子温度のプラズマで SiH<sub>4</sub> を解離させることにより、膜質を改善できることを明らかにした。

キーワード マイクロ波プラズマ CVD、電子温度、電子密度、フラグメンテーションパターン、a-Si:H 膜

### 1. ま え が き

今日、水素化アモルファスシリコン(a-Si:H)膜は、光・電子素子の材料として用いられており、膜質の向上、新しいデバイスへの応用を目指し研究開発が盛んに進められている。a-Si:H 膜の作製法としては、大面積化が容易である、低温プロセスであるといった特長をもつプラズマ CVD 法が広く用いられている。

プラズマ CVD 法において、膜質の向上をはかるためには、気相中および膜表面における反応を解明する必要がある。そのためには、ラジカル種の測定が必要であり、LIF<sup>(1)</sup>、IRLAS<sup>(2)</sup> 等、ラジカル種測定法の開発が進められてきている。また、SiH<sub>3</sub> ラジカルだけを選択的に基板表面に導いて成膜した結果とシミュレーションの結果とを比較することにより、SiH<sub>3</sub> ラジカル膜となる確率(付着確率)や膜表面損失確率等に関する検討が進められてきている<sup>(3)</sup>。

本論文では、SiH<sub>4</sub> ガスのプラズマ中への混入位置を変化させることにより、電子温度、電子密度の異なる

Ar プラズマ中で SiH<sub>4</sub> ガスを解離させることにより、各ラジカル種の割合、すなわちフラグメンテーションパターン、を変化させることを試みた。その結果、SiH<sub>4</sub> ガスの混入位置を変化させることにより、ラジカルフラグメンテーションパターンを変化させることができることを明らかにした。そこで、フラグメンテーションパターンを変化させて成膜し、その膜質評価を行い、膜質が改善できることを明らかにした。

### 2. 実 験

実験には筆者らが研究開発を進めてきている 2 重管式同軸線路形マイクロ波プラズマ CVD (MPCVD) 装置を用いた。図 1 に本 MPCVD 装置の概要図を示す。溶融石英製の外側放電管(outer discharge tube)に Ar ガスを放電ガスとして流し、マイクロ波により Ar プラズマを生成する。このとき、マイクロ波は同軸線路の基本モードでプラズマと結合する。マイクロ波電力は円筒キャビティ(cylindrical cavity)内に閉じ込められているので、電力の注入されている放電プラズマは円筒キャビティ内でのみ生成され、堆積室(chamber)内に拡散、流入する。SiH<sub>4</sub> ガスは、放電管端までステンレス製の内管(inner tube)を用いて導かれ、放電管端で Ar プラズマ中に混入され、Ar プラズマ粒子

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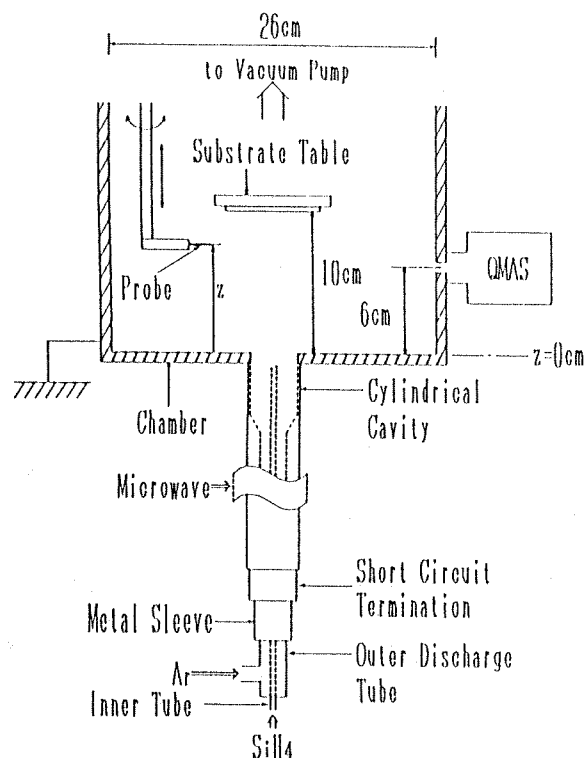


図1 実験装置概略図

Fig. 1 Schematic diagram of experimental system.

との衝突により解離される。本装置の詳細については文献 (4), (5) を参照されたい。

ここで、堆積室内における位置を示す座標として、放電管端から中心軸方向への距離を  $z$  と定義する。

基板テーブル (substrate table) は  $z=10$  cm の位置に設置した。この位置は、マイクロ波電力の供給がない空間的アフターグロープラズマ領域であり、イオン衝撃なしに、ラジカルをソフトランディングさせて成膜できる位置である<sup>(6)</sup>。電子温度、電子密度の測定には、直径 0.05 cm、長さ 0.3 cm の円筒プローブ (probe) を用いた。プローブは駆動シャフトに取り付けられており、堆積室内を可動である。4 重極質量分析装置 (QMAS) は  $z=6$  cm の位置の堆積室の側壁に直径 200  $\mu$ m のオリフィスを介して設置した (図1参照)。

次に放電条件を示す。プローブ測定においては、マイクロ波電力を 150 W とし、Ar ガス流量を 110 ml/min とした。このときの堆積室内のガス圧は約 3.5 mTorr となった。プローブ測定は  $z=0$  cm $\sim$ 9 cm で、堆積室の中心軸上で行った。4 重極質量分析および成膜においても、マイクロ波電力、Ar ガス流量をプローブ測定のとおり条件にしている。また、成膜時の

SiH<sub>4</sub> ガス流量は 50 ml/min とした。このとき、堆積室内のガス圧は約 5 mTorr となった。SiH<sub>4</sub> ガスを Ar プラズマ中に混入させる位置である内管端の位置を  $z=-2$  cm $\sim$ 3 cm まで変化させた。これは、後述のように Ar プラズマの電子温度、電子密度が大きく変化する範囲である。

膜厚の測定には、触針式膜厚計を用いた。ラザフォード・バックスキャタリング測定より得たスペクトルから、膜中の Si 原子密度を求めた。赤外吸収スペクトルと膜厚より、SiH 結合と SiH<sub>2</sub> 結合のストレッチングモードの積分強度を求め、これに、係数  $1.4 \times 10^{20}$  cm<sup>-2</sup> をかけることにより、両結合の形で含まれる水素原子密度を算出した<sup>(6)</sup>。紫外可視吸収スペクトルと膜厚より、光学エネルギーギャップを求めた。電子スピン共鳴測定の結果と膜厚より、ダングリングボンド密度を求めた。

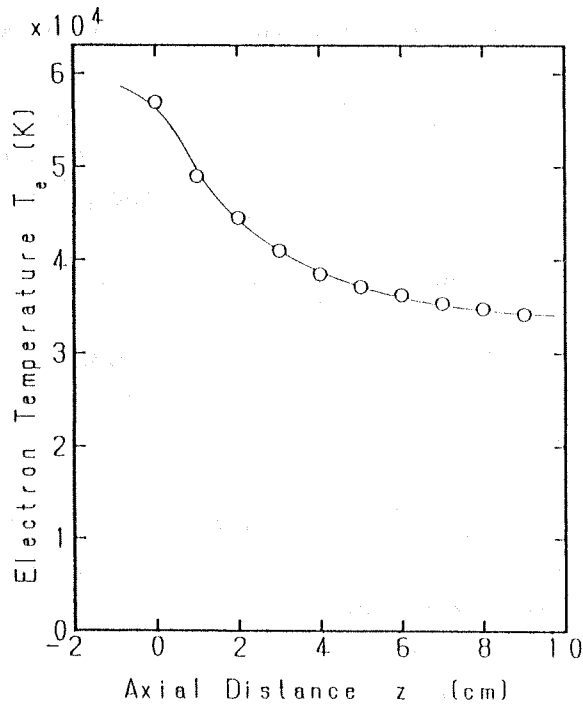
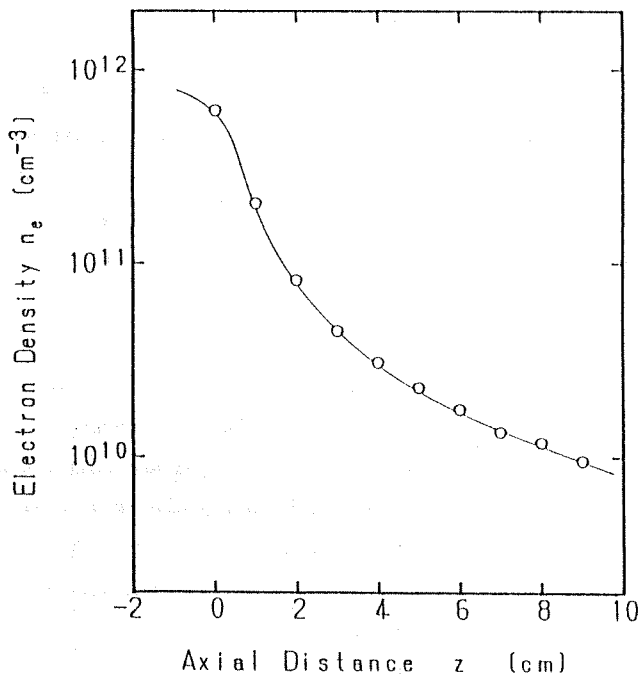
### 3. 実験結果

図2に電子温度の  $z$  依存性を示す。図より、電子温度は  $z=3$  cm 程度までは急激に減少し、その後は減少こう配が小さくなることわかる。

図3に電子密度の  $z$  依存性を示す。図より、電子密度は  $z=3$  cm 程度までは急激に減少し、その後は指数関数的に減少することわかる<sup>(7)</sup>。なお、 $z$  が負の領域 (すなわち放電管内) にはプローブが入らないため測定していないが、この領域ではマイクロ波電力が均一に入射するので、電子温度、電子密度ともに  $z=-2$  cm 程度までで急速に飽和して一定となると考えられる。

先に述べたように本 MPCVD 装置では、SiH<sub>4</sub> ガスを放電管端まで内管を用いて導き、そこで Ar プラズマ中に混入させ、Ar プラズマ粒子との衝突により解離させている。以上のことから、内管端の位置を変化させることにより、電子温度、電子密度の異なる Ar プラズマ中で SiH<sub>4</sub> ガスを解離させることができ、ラジカルのフラグメンテーションパターンを変化させることができると考えられる。

図4,5に4重極質量分析により求めたマススペクトル線強度の内管端位置依存性を示す。図4がイオナイザを OFF にしたときの結果であり、シラン系のイオンラジカルの変化を示す。図5はイオナイザを ON にしたときの結果である。いずれの結果においても、内管端の位置を  $z$  軸上で負から正にするに従い、SiH<sub>2</sub><sup>+</sup> が減少し、SiH<sub>3</sub><sup>+</sup> が増加していることがわかる。このことから、本 MPCVD 装置において内管端の位置を変化

図 2 電子温度の  $z$  依存性Fig. 2 Dependence of electron temperature on  $z$ .図 3 電子密度の  $z$  依存性Fig. 3 Dependence of electron density on  $z$ .

させることにより、ラジカルフラグメンテーションパターンを変化させることができることが明らかである。このように、 $\text{SiH}_2^+$  が減少し、 $\text{SiH}_3^+$  が増加するのは電子温度、電子密度が低下するので、 $\text{SiH}_2^+$  を作る電

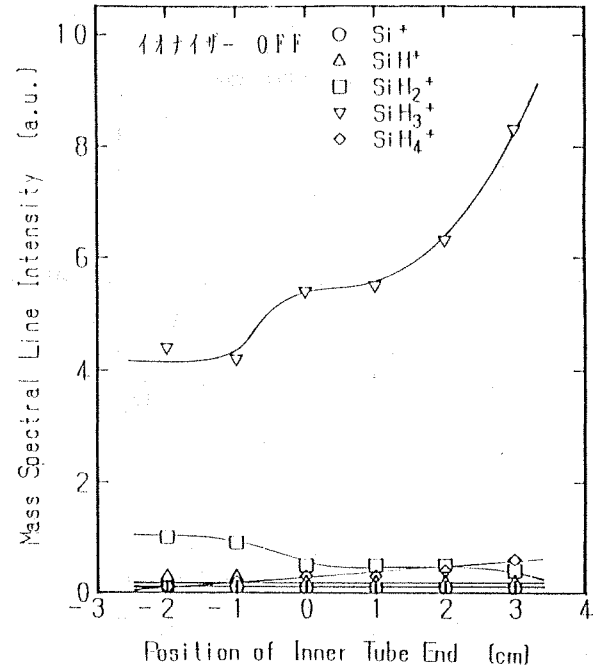


図 4 マススペクトル線強度の内管端位置依存性 (イオンイザ OFF)

Fig. 4 Dependence of mass spectral line intensity on the position of the inner tube end (ionizer off).

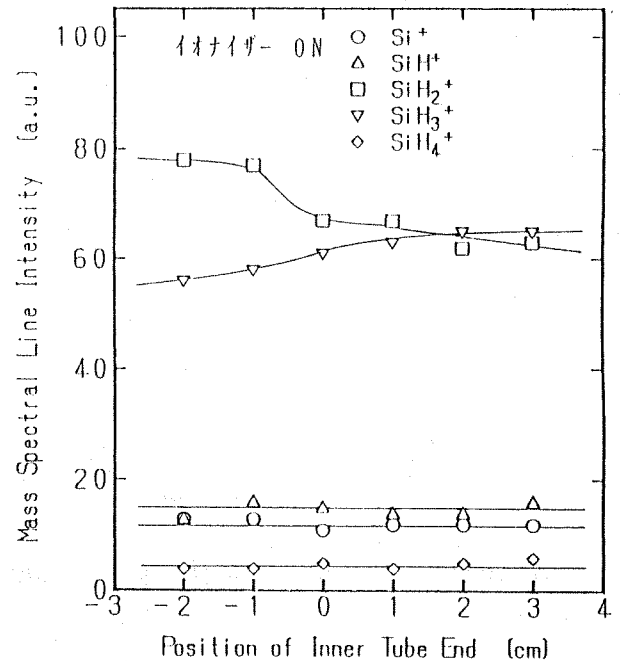


図 5 マススペクトル線強度の内管端位置依存性 (イオンイザ ON)

Fig. 5 Dependence of mass spectral line intensity on the position of the inner tube end (ionizer on).

離を伴う解離の度合いが抑制され、 $\text{SiH}_3^+$  を作る電離を伴う解離の度合いが増加したためである。イオンラジカルの変化と中性ラジカルの変化は必ずしも比例す

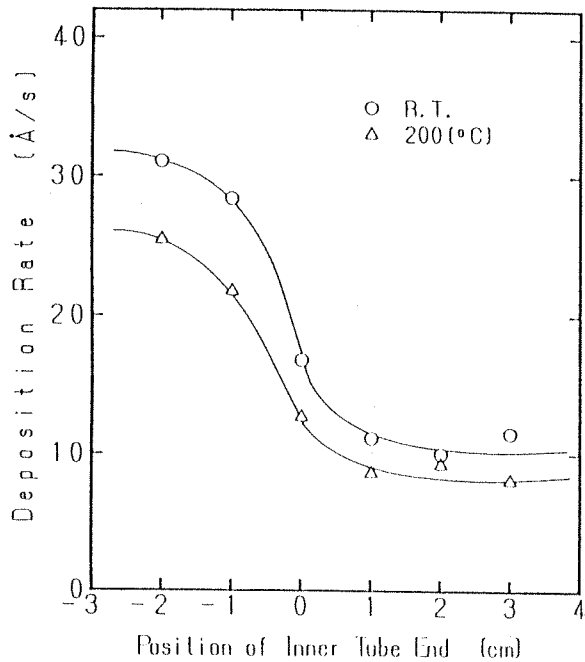


図 6 堆積速度の内管端位置依存性

Fig. 6 Dependence of deposition rate on the position of the inner tube end.

るとは限らないが、本研究で用いている電離度数%以下の弱電離プラズマにおいてはほぼ比例すると考えるのが妥当である。従って、 $\text{SiH}_2$  ラジカルは減少し、 $\text{SiH}_3$  ラジカルは増加していると考えられる。これまでに、 $\text{SiH}_3$  ラジカルのような膜表面でのモビリティの大きいラジカルを選択的に膜表面に導くことにより、膜質が改善されたという結果が報告されている<sup>(9)</sup>。以上のことから、内管端の位置を負から正にして成膜することにより、膜質の改善が期待できる。そこで、内管端の位置を変化させることにより、ラジカルのフラグメンテーションパターンを変化させて a-Si:H 膜を作製し、その膜質評価を次に行う。

図 6 に、堆積速度の内管端位置依存性を示す。図より、堆積速度は基板温度にかかわらず、内管端の位置が  $z = -1$  cm 程度から  $+1$  cm 程度の間に急激に減少し、その後は飽和傾向を示すことがわかる。これは、前述のように  $\text{SiH}_4$  の解離度およびフラグメンテーションパターンが大きく変化するためである。また、 $z = -1$  cm 程度から  $-2$  cm では堆積速度が大きく変化していないのは、前述のように電子温度、電子密度が大きく変化しないためと考えられる。なお、基板を  $200^\circ\text{C}$  に加熱して成膜すると基板温度を室温として成膜したときに比べ、従来の報告どおり<sup>(9)</sup>、堆積速度は遅くなることがわかる。これは、後述のように膜中の単

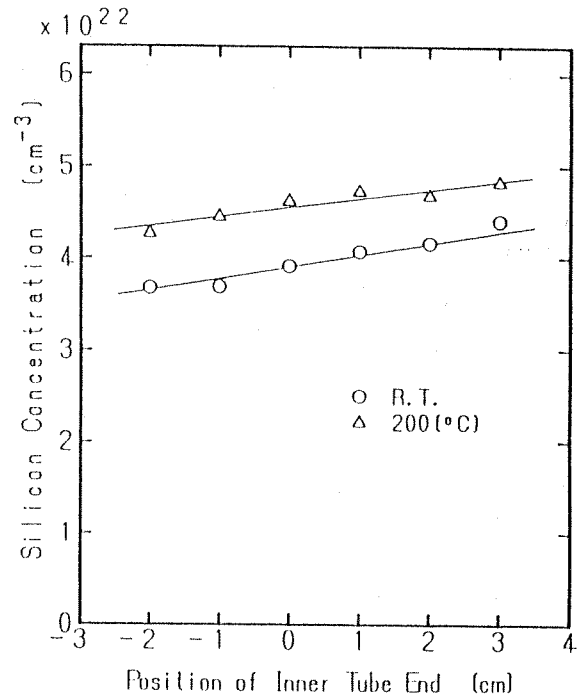


図 7 単位体積当たりのシリコン含有量の内管端位置依存性

Fig. 7 Dependence of silicon concentration on the position of the inner tube end.

位体積当たりのシリコン含有量が増加するためである。

図 7 に、単位体積当たりのシリコン含有量の内管端位置依存性を示す。図より基板温度にかかわらず、内管端の位置を負から正にするに従い、シリコン含有量は増加し、膜がち密化していることがわかる。これは、膜表面でのモビリティの大きい  $\text{SiH}_3$  ラジカルが増加したため、より安定な準位に入りながら膜堆積が進むためであると考えられる。なお、基板温度を  $200^\circ\text{C}$  に加熱して成膜すると基板温度を室温にして成膜したときに比べ、従来の報告どおり<sup>(9)</sup>、更にシリコン含有量が高くなることがわかる。

図 6, 7 より、(単位体積当たりのシリコン含有量)  $\times$  (堆積速度) で与えられる単位時間、単位面積当たりに膜となるシリコンの量を算出した。その結果、単位時間、単位面積当たりに膜となるシリコンの量は内管端の位置の変化に対し、図 6 に示した堆積速度と同様な傾向を示した。この結果から、内管端の位置を負から正に変化させることにより堆積速度が減少するのは、膜がち密化するためだけではないことがわかる。

内管端の位置を負から正に変化させることにより堆積速度が減少するのは、本実験における内管端位置の変化範囲 ( $z = -2$  cm から  $z = 3$  cm) が電力供給のある

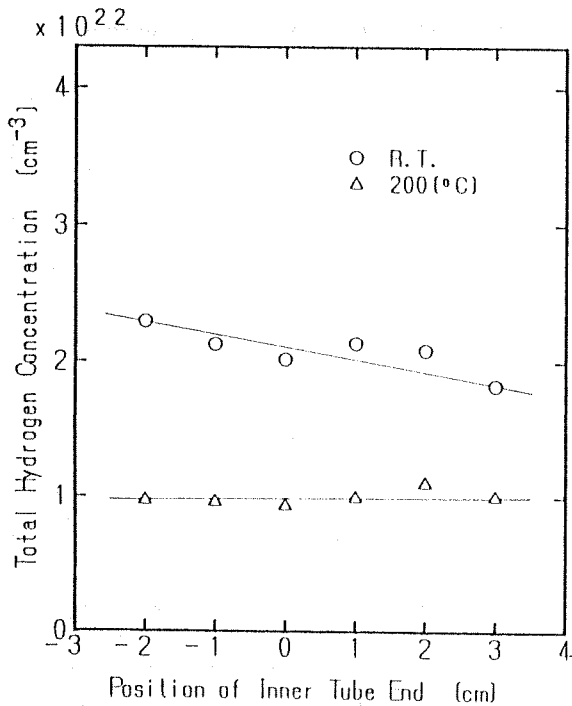


図 8 単位体積当たりの全水素含有量の内管端位置依存性  
Fig. 8 Dependence of total hydrogen concentration on the position of the inner tube end.

放電プラズマ領域から電力供給のない空間的アフターグロープラズマ領域への遷移領域を含むためである。すなわち、この間に  $\text{SiH}_4$  の解離度が低下すること、および解離の度合いが抑制され付着確率の高い  $\text{SiH}_2$  ラジカル<sup>(a)</sup>が減少し、付着確率の低い  $\text{SiH}_3$  ラジカル<sup>(a)</sup>が増加することによって考えられる。また、基板温度を変化させても単位時間、単位面積当たりに膜となるシリコンの量の内管端位置依存性は変化せずほぼ一定である。このことから、基板を加熱することにより堆積速度が減少するのは、膜が密化されるためであることがわかる。

図 8 に、単位体積当たりの全水素含有量の内管端位置依存性を示す。図より、基板温度が室温の場合は内管端の位置を負から正にするに従い、全水素含有量は減少することがわかる。基板温度を  $200^\circ\text{C}$  にすると、水素含有量は内管端の位置にかかわらず、約  $1 \times 10^{22} \text{ cm}^{-3}$  でほぼ一定となった。

内管端位置を負から正にするに従い、膜中の  $\text{SiH}$  結合密度は増加し、 $\text{SiH}_2$  結合密度は減少した。図 9 に、 $(\text{SiH 結合密度})/(\text{SiH}_2 \text{ 結合密度})$  比の内管端位置依存性を示す。図より基板温度にかかわらず内管端の位置を負から正にするに従い、 $\text{SiH}$  結合優勢な a-Si:H 膜が作製されることがわかる。なお、基板温度を  $200^\circ\text{C}$

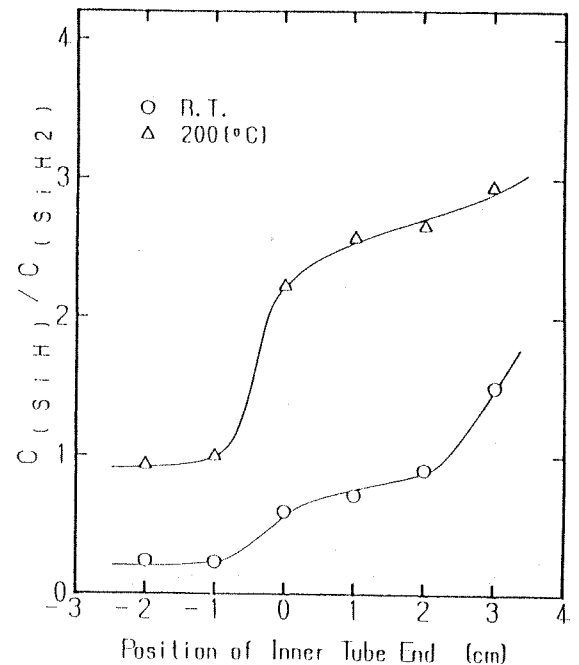


図 9  $(\text{SiH 結合密度})/(\text{SiH}_2 \text{ 結合密度})$  比の内管端位置依存性

Fig. 9 Dependence of (SiH bond density)/(SiH<sub>2</sub> bond density) ratio on the position of the inner tube end.

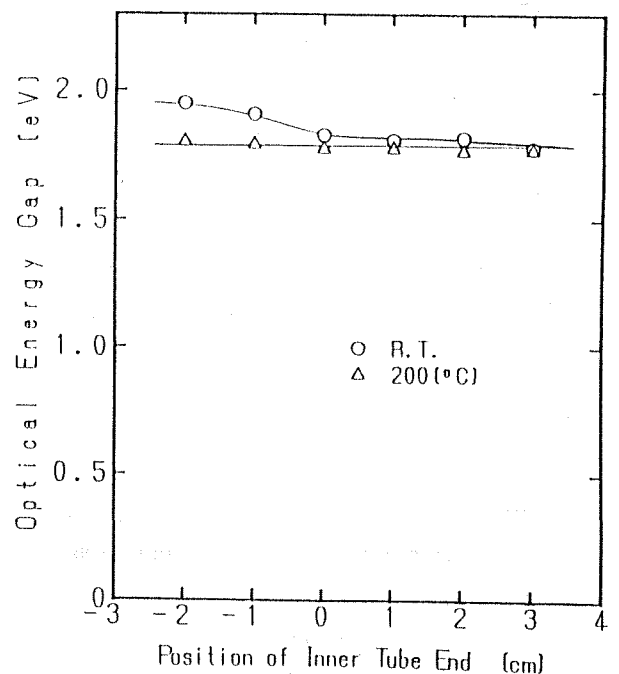


図 10 光学エネルギーギャップの内管端位置依存性

Fig. 10 Dependence of optical energy gap on the position of the inner tube end.

に加熱して成膜すると基板温度を室温にして成膜したときに比べ、更に  $\text{SiH}$  結合優勢な膜が作製できるという従来どおりの結果が得られている。

図 10 に、光学エネルギーギャップの内管端位置依存

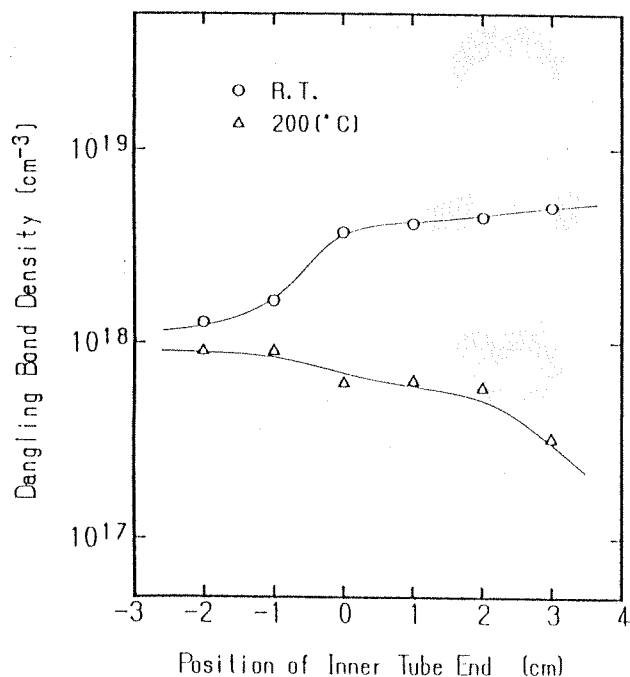


図 11 ダングリングボンド密度の内管端位置依存性  
Fig. 11 Dependence of dangling bond density on the position of the inner tube end.

性を示す。図より、基板温度が室温の場合は内管端の位置を負から正にするに従い、光学エネルギーギャップは減少することがわかる。基板温度を 200°C にすると、光学エネルギーギャップは、内管端の位置にかかわらず、約 1.78 eV でほぼ一定となった。この傾向は、全水素含有量の内管端位置依存性と一致している。

図 11 に、ダングリングボンド密度の内管端位置依存性を示す。図より、基板温度が室温の場合は内管端の位置を負から正にするに従い、ダングリングボンド密度はやや増加することがわかる。すなわち、基板を加熱しない、または加熱できない場合には、内管端位置を負にして  $\text{SiH}_2$  ラジカルを大きくしたほうがダングリングボンド密度を低減できることを示している。基板を 200°C に加熱し膜表面でのラジカルのモビリティを大きくすると、ダングリングボンド密度は内管端の位置を負から正にするに従い減少し、より良質な a-Si:H 膜を作製できることがわかる。

以上の結果から、内管端の位置を負から正にして成膜するに従い、堆積速度は低下するものの、膜質を改善できることが明らかとなった。これは、膜表面でのモビリティの大きい  $\text{SiH}_3$  ラジカルが増加したためである。

#### 4. む す び

2 重管式同軸線路形マイクロ波プラズマ CVD 装置の堆積室内において、純 Ar プラズマ中で電子温度、電子密度の空間分布測定を行った。更に、 $\text{SiH}_4$  ガスの Ar プラズマ中への混入位置（内管端の位置）を変化させることにより、電子温度、電子密度の異なる Ar プラズマ中で  $\text{SiH}_4$  ガスを解離させ、そのフラグメンテーションパターンを質量分析法により測定した。その結果、以下のことが明らかになった。

(1) 電子温度は  $z=3$  cm 程度までは急激に減少し、その後、減少こう配が小さくなる。

(2) 電子密度は  $z=3$  cm 程度までは急激に減少し、その後、指数関数的に減少する。

(3) 内管端の位置を負から正にするに従い、 $\text{SiH}_2^+$  は減少し、 $\text{SiH}_3^+$  は増加する。

更に、内管端の位置を変化させて成膜し、その膜質評価を行った。その結果、内管端の位置を  $z$  軸上で負から正にするに従い、堆積速度および膜質は以下のように変化することが明らかになった。

(1) 堆積速度は内管端の位置が  $z=1$  cm 程度までは急激に減少し、その後飽和傾向を示す。これは、 $\text{SiH}_4$  の解離度の低下および付着確率の低い  $\text{SiH}_3$  ラジカルの増加によると考えられる。

(2) シリコン含有量、全水素含有量、水素の結合状態および光学エネルギーギャップの変化は、膜質の改善を示す。

(3) ダングリングボンド密度は、室温で成膜した場合にはやや増加するものの、基板温度を 200°C とし成膜すると減少する。

以上の結果から、低い電子温度のプラズマで  $\text{SiH}_4$  を解離させることにより、膜表面でのモビリティの大きい  $\text{SiH}_3$  ラジカルを増加させることができるので、膜質の改善がはかれることがわかる。

今後、中性ラジカルのフラグメンテーションパターンを定量的に明らかにし、堆積機構のより詳細な検討を行う予定である。

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# Influence of Ion Bombardment on a-Si : H Films Fabricated by Plasma Chemical Vapor Deposition

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## SUMMARY

Plasma parameters of Ar/SiH<sub>4</sub> plasma were measured as a function of dc bias in a double-tubed coaxial line-type microwave plasma chemical vapor deposition (CVD) apparatus. The results indicate that it is possible to control the ion bombardment energy without affecting either the gas phase reaction or ion flux density incident to the substrate. Hydrogenated amorphous silicon films were deposited as a function of the ion bombardment energy and characteristics of the deposited films were investigated. The results indicate that the ion bombardment improves film density, bonding characteristics of hydrogen, and optical band gap but increases the concentration of dangling bonds due to Ar ion implantation. The ion bombardment not only causes the heating of the films but also induces sputtering and ion implantation.

**Key words:** Plasma CVD; a-Si : H; dc bias voltage; sheath voltage; ion bombardment.

## 1. Introduction

Hydrogenated amorphous silicon (a-Si : H) has been used extensively as optoelectronic materials for solar

cells and copiers and as semiconducting materials for thin-film transistors. To improve the performance and to develop new applications, amorphous silicon has been a focus of intensive studies. The deposition of a-Si : H has been investigated extensively using high-frequency discharge and electrocyclotron resonance (ECR) discharge plasma chemical vapor deposition (CVD) methods.

It has been reported [1, 2] that ion bombardment improves the film characteristics. The authors have also reported [3, 4] that ion bombardment causes the increase in the film density, the decrease of SiH<sub>2</sub> bonds and the increase of SiH bonds due to film heating.

Because films fabricated by the commonly used high-frequency plasma CVD method are deposited in a discharge plasma to which electric energy is supplied, the films are exposed to ion bombardment. The ion bombardment has been controlled by discharge voltage that causes the variation in self-bias of the substrates. The self-bias is controlled by changing electron temperature and electron density, and thus the process also influences gas phase reactions. Therefore, it is not possible to investigate the sole influence of ion bombardment on film characteristics.

We have developed a double-tubed coaxial-line-type microwave plasma CVD (MPCVD) apparatus that allows the film deposition in a spatial afterglow plasma region with very little ion bombardment by confining the discharge plasma to a restricted area [3-9]. DC bias ( $V_{dc}$ ) is

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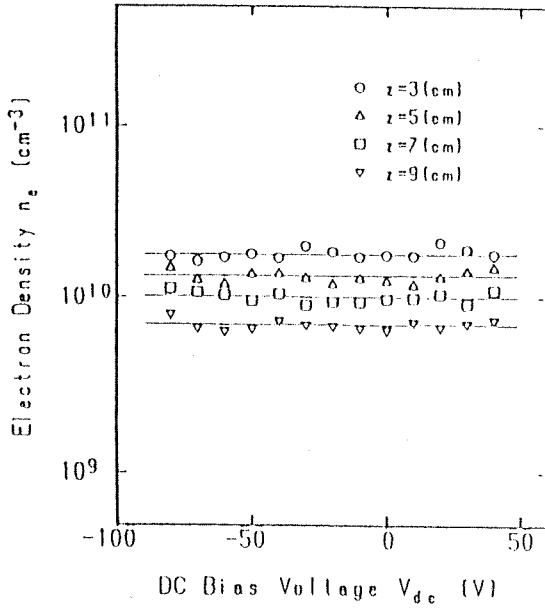


Fig. 2. Dependence of  $n_e$  on  $V_{dc}$ .

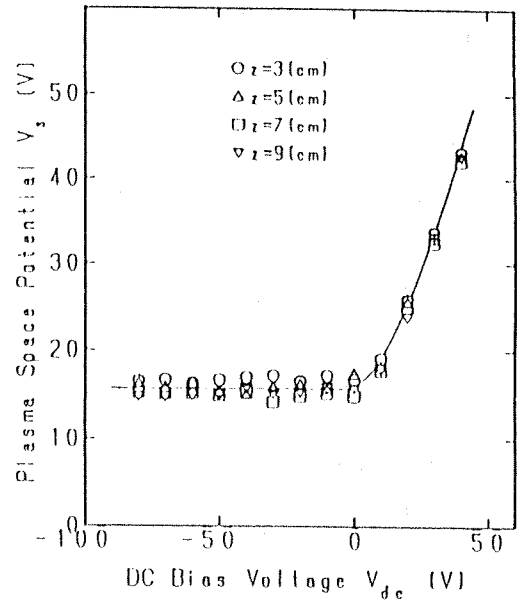


Fig. 4. Dependence of  $V_s$  on  $V_{dc}$ .

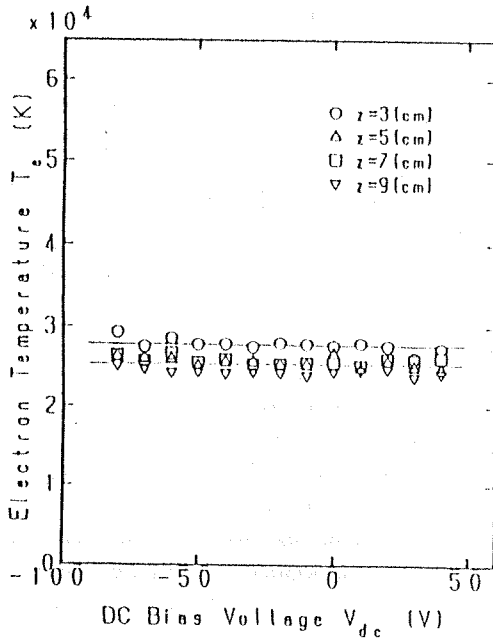


Fig. 3. Dependence of  $T_e$  on  $V_{dc}$ .

### 3. Experimental Results

#### 3.1. Influence of $V_{dc}$ on the plasma parameters

Figure 2 shows the dependence of the electron densities ( $n_e$ ) on  $V_{dc}$  at various  $z$  positions;  $n_e$  is constant regardless of  $V_{dc}$  at a given  $z$  position but decreases with increasing  $z$ .

Figure 3 shows the dependence of the electron temperature ( $T_e$ ) on  $V_{dc}$ ;  $T_e$  is constant regardless of  $V_{dc}$  but decreases slightly with increasing  $z$  to 5 cm but remains constant above 5 cm.

The independence of  $T_e$  and  $n_e$  on  $V_{dc}$  in Figs. 2 and 3 indicates the absence of dc discharge, which in turn indicates no effect of  $V_{dc}$  on the gas phase reaction.

It has been reported [1] that the influence of positive bias voltage on the film characteristics can be attributed to the presence of positive electric field at the surface of the substrate, which causes the acceleration of electrons. But we have observed the dependence of plasma space potential ( $V_s$ ) on  $V_{dc}$  when the substrate was positively biased. This indicates that it is not necessarily correct to assume the acceleration of electrons [12]. In this study  $V_s$  was measured for a substrate table with a surface area of 54 cm<sup>2</sup> and the results were analyzed to quantify the electric field at the surface of the substrate.

from concentrations of Si, Ar, and total H, the optical band gaps from UV absorption spectra and film thickness, and the densities of dangling bonds from the result of electron spin resonance measurements and film thickness.

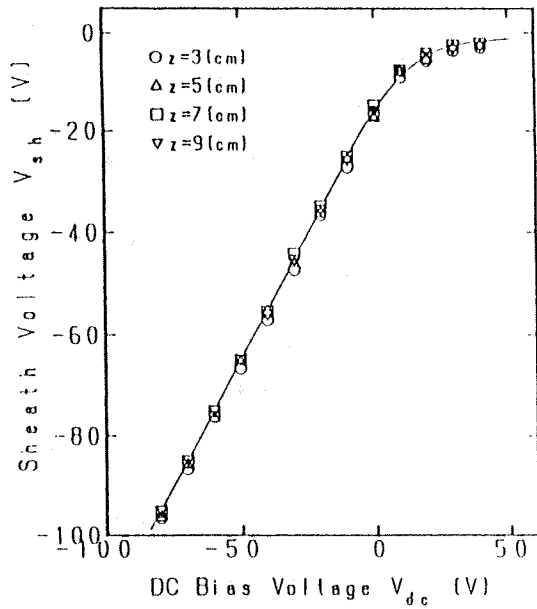


Fig. 5. Dependence of  $V_{sh}$  on  $V_{dc}$ .

Figure 4 shows the dependence of  $V_s$  on  $V_{dc}$ . The figure indicates that  $V_s$  remains constant for negative bias but increases with increasing positive bias. It also indicates that  $V_s$  does not depend on  $z$  in the range between 3 and 9 cm.

The sheath voltage ( $V_{sh}$ ) is defined by  $V_{dc} - V_s$ . The sheath voltages were calculated from the data presented in Fig. 4 and are shown in Fig. 5. Ions are either accelerated or decelerated by the sheath voltage. Since  $V_{sh}$  is negative regardless of  $V_{dc}$  as indicated in Fig. 5, it is evident that ions are neither decelerated nor recoiled at the surface of the substrate even by the application of positive bias.

Because electrons are recoiled by the electric field in the sheath, the ion density becomes higher than  $n_e$  at the surface of the substrate even when a positive bias voltage is applied. This indicates the formation of an ion sheath. Since it is not possible for the ions to follow the microwave field and there exists no electric field gradient in the deposition chamber as indicated earlier, it is expected that the kinetic energy of the ions is quite small and about the order of room temperature prior to the injection into the sheath. Therefore, the kinetic energy of the ions at the moment of incidence to the substrate can be determined solely by the sheath voltage. The mean-free path of the ions is about 2 cm for the gas pressure of 4 mtorr in the deposition chamber.

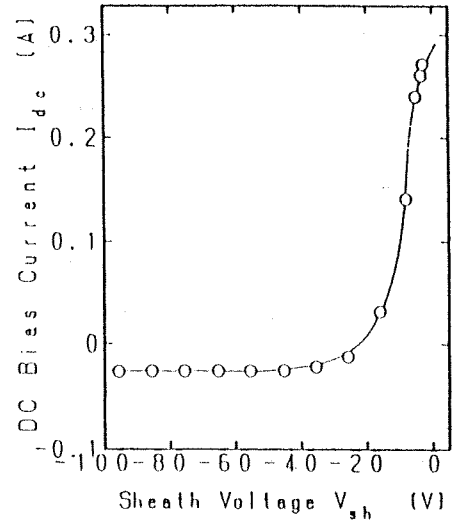


Fig. 6. Dependence of  $I_{dc}$  on  $V_{sh}$ .

Since the thickness of the ion sheath is about 2 mm [12], the ions pass through the sheath without colliding with other particles. Thus the kinetic energy of the ions at the moment of incidence to the substrate, i.e., the energy of ion bombardment ( $E_i$ ), is given by the product of the unit electric charge and the absolute value of the sheath voltage when all ions are assumed to be singly charged. By varying  $V_{dc}$  from -80 V to +40 V, it is possible to change  $E_i$  from about 95 eV to about 3 eV.

Figure 6 shows the dependence of electric current through the substrate ( $I_{dc}$ ) on  $V_{sh}$ ;  $I_{dc}$  is the sum of electron and ion currents. Since  $V_s$  is always larger than  $V_{dc}$  whose values are between -80 V and +40 V in this study, there always exists an electric field that accelerates ions at the surface of the substrate; but there does not exist any electric field that recoils ions even when a positive bias voltage is applied. The figure indicates that  $I_{dc}$  remains constant for  $V_{sh}$  less than about -45 V. The constant value of  $I_{dc}$  is the saturated ion current ( $I_{is}$ ). This indicates that the ion current is constant regardless of  $V_{sh}$  and equals  $I_{is}$ . For  $V_{sh}$  higher than -45 V,  $I_{dc}$  increases with increasing  $V_{sh}$ . The increase is not due to ion current but due to electron current. Electrons have some kind of energy distribution, generally Maxwell distribution. With increasing  $V_{sh}$ , a part of the electrons with high energy overcome the electric field and begin passing through the substrate, thereby causing the increase of  $I_{dc}$ . Assuming that all ions are singly charged in the plasma, the ion flux density incident to the substrate ( $\Gamma_i$ ) is given by the following equation:

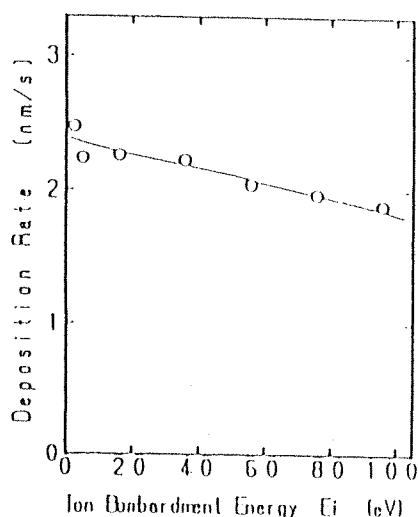


Fig. 7. Dependence of deposition rate on  $E_i$ .

$$\Gamma_i = \frac{I_{is}}{e \cdot S}$$

where  $e$  and  $S$  are the unit electric charge and the surface area of the substrate table, respectively. In the experimental range of this study,  $\Gamma_i$  is constant regardless of  $V_{dc}$ .

Since  $T_e$  and  $n_e$  are not affected by  $V_{dc}$  as shown in Figs. 2 and 3, the gas phase reaction is not affected by  $V_{dc}$  either. Since the gas phase reaction is not affected, the ionic species incident to the substrate remains unaffected.

In the experimental range of this study where the ion sheath is formed at the surface of the substrate, the ionic current remains constant and therefore  $\Gamma_i$  also remains constant as can be seen in Fig. 6. Therefore, it is possible to control  $E_i$  without affecting the gas phase reaction and  $\Gamma_i$  by using the MPCVD apparatus.

### 3.2. Influence of ion bombardment on film characteristics

To delineate the influence of ion bombardment on film characteristics, thin films of a-Si:H were deposited as a function of  $E_i$  by varying  $V_{dc}$  and their film characteristics were evaluated.

Figure 7 shows the dependence of the deposition rate on  $E_i$ . The deposition rate decreases almost linearly with increasing  $E_i$ . As will be discussed later, the

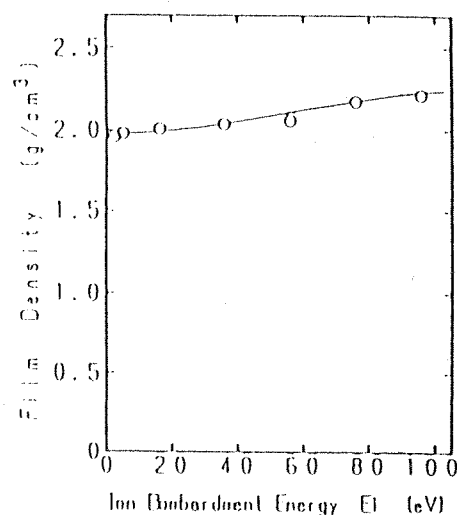


Fig. 8. Dependence of film density on  $E_i$ .

decrease is due to the densification of the films, sputtering of the films and decreasing residence time of the molecules caused by the increasing kinetic energy of the ions.

Figure 8 shows the dependence of film density on  $E_i$ . The film density increases with increasing  $E_i$ . Since we observed previously that the film density increased by the heating of the substrate [7], the increase of film density is inferred to the heating of the film surface by ion bombardment. The film deposited at  $E_i$  of about 95 eV has about 15 percent higher density than that deposited at  $E_i$  of about 3 eV.

By comparing the density of the film deposited at  $E_i$  of about 95 eV with the previously reported results on film density as a function of substrate temperature [7], the surface temperature of the film is estimated to be about 250°C for  $E_i$  of about 95 eV. As discussed earlier, the densification of the film is a cause of the decrease in deposition rate. The deposition rate decreased about 40 percent with increasing  $E_i$  from 3 eV to 95 eV. On the other hand, the film density increased about 15 percent. Hence, about 40 percent ( $\sim 15/40 \times 100$ ) of the decrease in the deposition rate can be attributed to the densification of the films.

Figure 9 shows the dependence of the optical band gap on  $E_i$ . The optical band gap decreases with increasing  $E_i$ .

Figure 10 shows the dependence of hydrogen concentration in the film on  $E_i$ . The hydrogen concentration

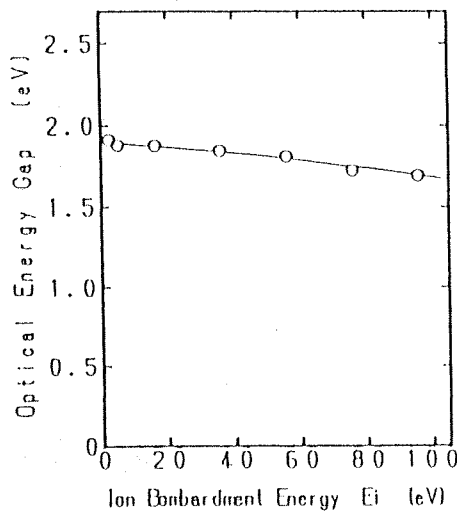


Fig. 9. Dependence of optical energy gap on  $E_i$ .

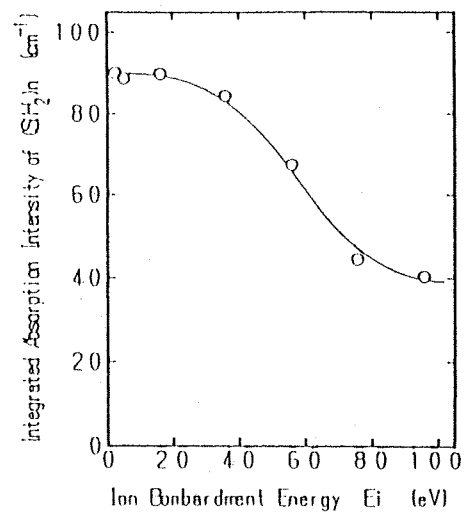


Fig. 11. Dependence of integrated absorption intensity of  $(SiH_2)_n$  on  $E_i$ .

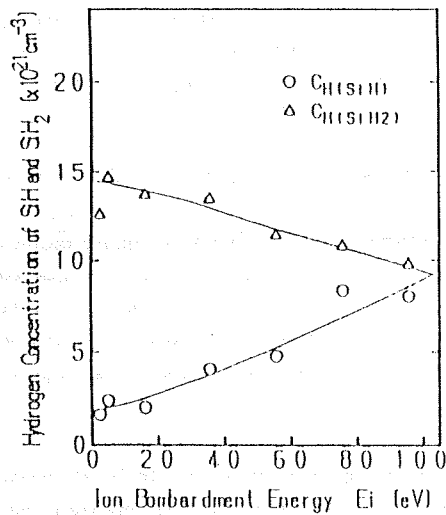


Fig. 10. Dependence of hydrogen concentration of SiH and SiH<sub>2</sub> on  $E_i$ .

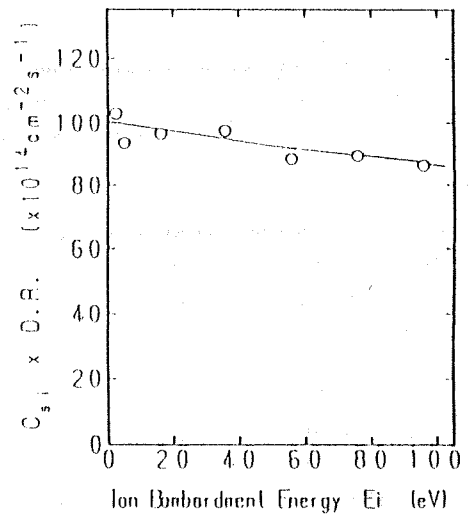


Fig. 12. Dependence of  $C_{Si} \times D.R.$  on  $E_i$ .

of SiH bonds increased with increasing  $E_i$ , while the hydrogen concentration of SiH<sub>2</sub> decreased. At  $E_i$  of about 60 eV the concentration of SiH bonds ( $= C_{H(SiH)}$ ) in the film surpassed that of SiH<sub>2</sub> bonds  $C_{H(SiH_2)/2}$ . Therefore, the films deposited at  $E_i$  higher than 60 eV contain SiH bonds predominantly.

Figure 11 shows the dependence of integrated absorption intensity of  $(SiH_2)_n$  chains on  $E_i$ . The concentration of  $(SiH_2)_n$  chains decreased with increasing  $E_i$ .

The amount of Si deposited for a unit time per unit area can be calculated from the product of the deposition rate and Si concentration ( $C_{Si}$ ). The results are shown in Fig. 12 as a function of  $E_i$ . The amount of Si deposited for a unit time per unit area decreased with increasing  $E_i$ . The decrease might be the result of sputtering of the films by ion bombardment and the decreasing residence time of molecules due to increasing kinetic energy. The contribution of these effects on the deposition rate is estimated similarly to that of the film densification, and a value of about 60 percent is obtained as expected.

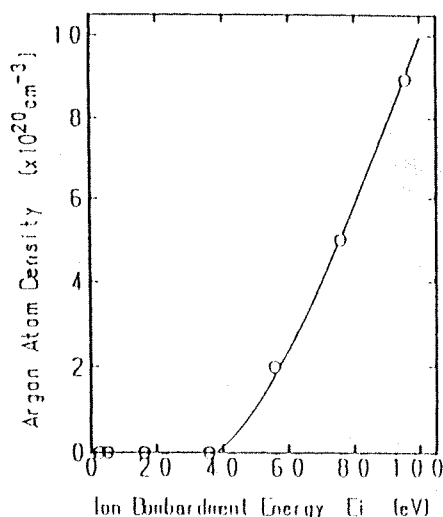


Fig. 13. Dependence of Ar concentration on  $E_i$ .

Figure 13 shows the dependence of Ar concentration on  $E_i$ . The Ar concentration of the films deposited at  $E_i$  less than about 40 eV is less than the detection limit of the instrument, but the Ar concentration of the films deposited at  $E_i$  higher than about 40 eV increases with increasing  $E_i$ . At  $E_i$  higher than about 40 eV, the kinetic energy of Ar ions is high enough to cause the deeper penetration of the ions into the film and, therefore, the probability of Ar retention increases. Specifically, the ion bombardment causes the implantation of Ar ions in the films.

Figure 14 shows the dependence of dangling bond density on  $E_i$ . The dangling bond density increases with increasing  $E_i$ . The increase is caused by the implantation of Ar ions that damaged the films [8].

The results in Figs. 8 to 11 indicate that the ion bombardment improves the film quality due to heating during deposition. However, as indicated in Figs. 13 and 14, the ion bombardment causes the implantation of Ar ions which in turn causes the increase of Ar concentration and of dangling bond density in the films. Although the ion bombardment has pros and cons, it is desirable to avoid ion bombardment during the deposition of high-quality a-Si:H films due to the increase of dangling bonds.

#### 4. Conclusions

The plasma parameters were measured for dc bias voltage ( $V_{dc}$ ) between -80 V and +40 V in the double-

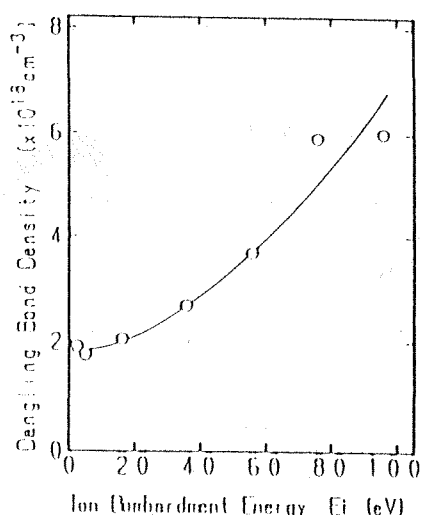


Fig. 14. Dependence of dangling bond density on  $E_i$ .

tubed coaxial-line microwave plasma CVD apparatus. The results are as follows:

(1) Neither electron temperature nor electron density is affected by  $V_{dc}$ .

(2) The plasma space potential is not affected by negative  $V_{dc}$ , but the plasma space potential increases with increasing  $V_{dc}$  when  $V_{dc}$  is positive. The application of positive  $V_{dc}$  does not create an electron sheath but rather an ion sheath.

(3) It is possible to control ion bombardment energy ( $E_i$ ) by  $V_{dc}$  without affecting either the gas phase reaction or the ion flux density incident to the substrate.

a-Si:H films were deposited for various values of  $E_i$ . The results are as follows:

(1) The ion bombardment causes the heating of the film surface as well as ion implantation and sputtering.

(2) The film heating improves the film density, the bonding characteristic of hydrogen, and the optical band gap.

(3) The ion implantation increases the Ar concentration and dangling bond density in the films.

(4) The amount of Si deposited for a unit time per unit area decreases due to sputtering and decreasing residence time of molecules on the film surface caused by increasing kinetic energy.



A further study will be conducted to delineate the mechanism of film growth during ion bombardment.

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