

OpenFOAM 流体構造連成解析

概要:

「OpenFOAM-1.5-devに搭載されている連成解析
ソルバー(icoFsiFoam)と、公開されている片持ち梁の
例題(flappingConsoleSmall)を使って、
それらの使用方法と、(例題の)拡張方法を演習する。」

目次

- はじめに
- プログラム (icoFsiFoam) の説明
- 公開ケース (flappingConsoleSmall) の説明
- DEXCSランチャーの説明
- 解析実習とパラメタ変更要領の概説
- 解析事例の紹介と課題

はじめに(背景)

- OpenFOAMによる流体構造連成解析
 - 公開版(~1.7.0)標準ソルバーは存在しない
 - 拡張版(1.5-dev)にicoFsiFoam有るがtutorialは無い
 - 一般公開情報はいくつか存在



<http://bit.ly/clogWp>

<http://www.cfd-online.com/Forums/openfoam-solving/58153-fsi-porous-media-thin-shell.html>

May 28, 2008, 06:15

Hi Hrv, Thanks for your rep #3

novak
New Member

Novak Elliott
Join Date: Mar 2009
Posts: 6
Rep Power: 3

Hi Hrv,

Thanks for your reply. I found the following thesis report on FSI with OpenFOAM:
http://powerlab.fsb.hr/ped/kturbo/Op...RIVOLA_FSI.pdf
(linked from the OpenFOAM page <http://foamcfd.org/resources/theses.html>)

The relative merits of the two solvers were compared:

1. **IcoFsiFoam:**
 - + integrated automesh motion capacity to minimise mesh degeneration
 - only allows for a domain with 2 regions
 - difficult to use(?)
2. **IcoStructFoam**
 - + easy to use do to better architecture(?)
 - only handles small structural deformations
 - only allows for a domain with 2 regions

Generally:

- * OpenFOAM structural equations only handle homogeneous structures
- * OpenFOAM's ability to handle large displacements for thin-shell structures is limited by small cell sizes and small timestep sizes hence long computation times

Second OpenFOAM Workshop in Zagreb, Croatia <http://bit.ly/a9JYr8>

http://www.openfoamworkshop.org/2007/index.php?title=Coupled_Simulations_and_Fluid-Structure_Interaction

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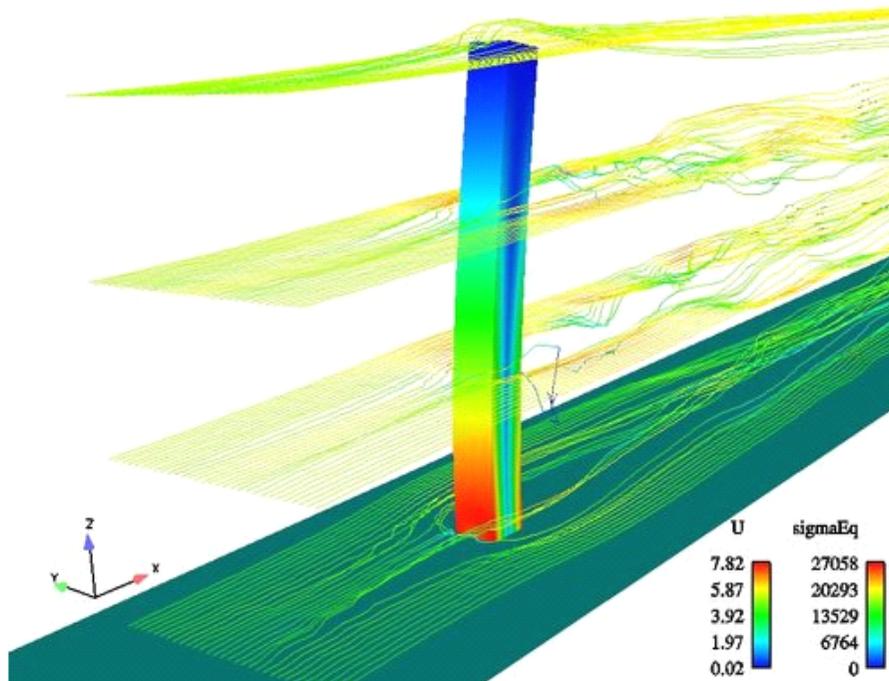
WIKI

Coupled Simulations and Fluid-Structure Interaction

A generic Computational Continuum Mechanics library like OpenFOAM is a natural platform for Fluid-Structure Interaction (FSI): both fluids and structural solvers already exist. Furthermore, doing a simulation in a single software simplifies the operation: there is no need for multi-threaded simulations of software to

FSI results

The FSI solver is tested on the flow past a cantilevered elastic square beam. The frequency of the inlet flow velocity pulsation is equal to the first natural frequency of the beam. The picture below shows streamlines pattern and equivalent Cauchy stress at the beam boundary. This calculation is done for the solid-fluid density ratio 100:1. For lower density ratios loosely coupled algorithm becomes unstable.



solvers and discretisation methods share the base mesh mapping tools are already implemented further
ed at Imperial College in late 1990-s - but it wasn't easy.
esh-based field registration, FSI in the new version is
SI-relevant capabilities and examples of application.

[\[edit\]](#)

Engineering Applications: Fluid-Structure Interaction

dar Karac of [University College Dublin](#) [Abstract](#)

CO s.r.l. [Abstract](#) [Slides](#)

tructures by Thomas Gallinger of [Technical University](#)

ons of flapping wings at low Reynolds numbers by

Netherlands [Abstract](#) [Slides](#)

eljko Tukovic of [University of Zagreb](#), Croatia

edia by Marianne Mataln of ICE Strömungsforschung

gorithms by Vicente Diaz Casas of [Universidade da](#)

g by Valentine Kanyanta of [University College Dublin](#)

<http://www.cfd-online.com/Forums/openfoam-solving/58588-patch-end-points-mesh-motion-movingwallvelocity.html><http://bit.ly/bVzmIs>

March 22, 2008, 02:38
Hello Patrick, 1) You have
#2

hjasak
Senior Member

Hrvoje Jasak
Join Date: Mar 2009
Location: London, England
Posts: 1,580
Rep Power: 11

Hello Patrick,

1) You have a problem with consistency of a boundary condition in mesh motion: a "lower" (eg. slip), will be over-ridden by the "higher" (eg. fixed value).

2) No need: moving wall velocity is an absolutely consistent version of a fixed value velocity. It is done because the code can calculate the wall-normal motion flux better than anything else.

Have a look at the flux field for the boundary - do you have a non-zero flux for it?

3) Yes, we are writing some papers about it. This is the main reason I am reluctant to release the tutorial, 'cause the new code from Zeljko is so much better. This will definitely come out in SVN at some stage, but the Eccomas, Commodia and journal papers are not out yet.

This is what I propose to do: I will give you a tutorial for icoFsiFoam as it stands without checking it in. Please find `flappingConsoleSmall_HJ_21Mar2008.tgz` in

<http://powerlab.fsb.hr/ped/kturbo/OpenFOAM/run/>

It runs fo

Enjoy,

Hrv

Hrvoje Ja

powerlab.fsb.hr - /ped/kturbo/OpenFOAM/run/

[\[To Parent Directory\]](#)

20. ožujak 2008	23:53	5835	dropletSplash_HJ_22Nov2007.tgz
21. ožujak 2008	19:32	2233668	flappingConsoleSmall_HJ_21Mar2008.
10. veljača 2006	1:21	81753739	kivaTest_HJ_9Feb2006.tgz
8. srpanj 2006	16:10	12334045	mixer3D_HJ_8Jul2006.tgz
19. veljača 2008	17:43	849490	mixerGgi_HJ_19Feb2008.tgz
30. svibanj 2006	22:55	12021687	pipeInTank.tgz
27. lipanj 2006	15:47	3151504	simpleEngineTutorial.tgz

<http://bit.ly/dkDvKS>

<http://powerlab.fsb.hr/ped/kturbo/OpenFOAM/run/>



page discussion view source history

Contrib icoStructFoam

Valid versions: **OF**
v1.3

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1 Description

This solver is a hybrid of `icoFoam` and `solidFoam`. The pressure of the fluid is solved with `icoFoam` and the solid is solved with `solidFoam`.

This solver is only a demo. It is not intended for production use.

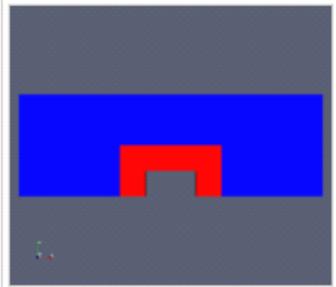
Ah. And by the way: it does not work on Linux.

2 Algorithm

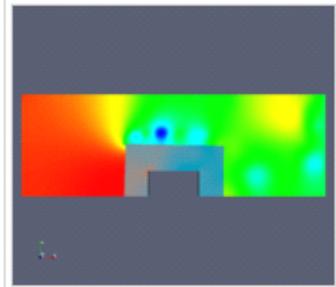
At each time-step the following things are solved:

- the equations in the fluid region
- fluid pressures at the fluid region
- the equations for the solid region
- displacements for the interface between the solid and fluid region
- the grid of the fluid region

4.2 Soft thing on a stick



The two regions



Pressure and strain

This case simulates the flow through a channel with an obstacle that consists of two parts: a solid, fixed part around which a deformable material is wrapped.

The two regions are shown in the picture on the left:

Blue: the fluid. On the left-side a velocity inlet, on the right side a pressure outlet. Top is a wall, bottom, a symmetry boundary.

- Red: the solid. The bottom edges are symmetry boundaries. The inner edges are fixed (the stick in the title)

The picture on the left is the undeformed geometry at the beginning. The picture on the right is the geometry at the end of the simulation. The solid is colored with the strain, the fluid with the pressure.

In certain parts of Austria this is also known as the Lentos-case.

5 Download

The solver

Case of the deformable channel

Case of the soft thing on a stick

6 History

Category: OpenFOAM Version 1.3

10 Nov 2006: Changed version number to 1.3

--Bgschaid 13:34, 11 Nov 2005 (CET)

PhD course in CFD with OpenSource software, 2007

Syllabus

The course gives an introduction to the use of OpenSource software for CFD applications. A major project work in OpenFOAM (see the short description below) forms a large part of the course. The project may be defined according to the student's special interests. The result of the project should be a detailed tutorial for a specific application of OpenFOAM. The tutorials will be peer-reviewed and graded by the students, and the tutorials thus form a part of the course. The tutorials will be made available as OpenSource, as a contribution to the OpenFOAM community. To pass the course the student must do the project and peer-review the tutorials from the other projects.

The course homepage is http://www.tfd.chalmers.se/~hani/kurser/OS_CFD_2007

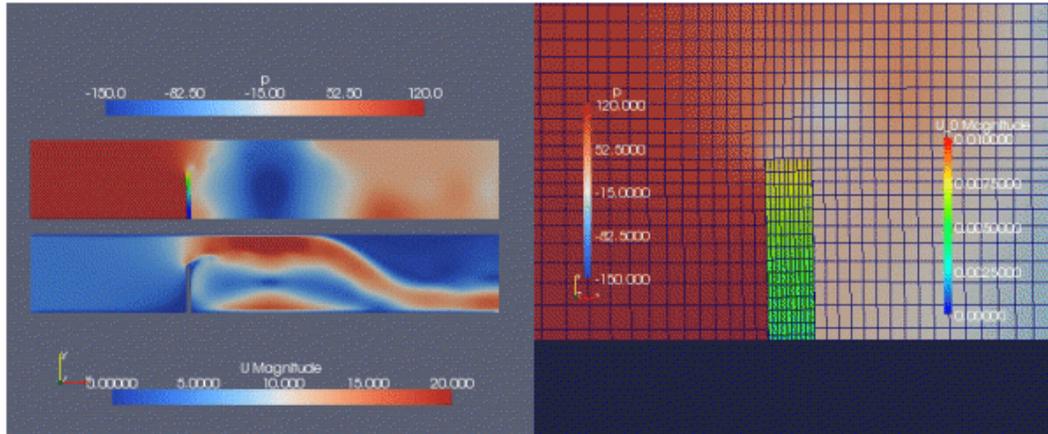
Final, peer-reviewed, student-contributed tutorials

These files should at least work for OF-1.4.1 or OF-1.4.1-dev at the student computers in the Mechanical Engineering building at Chalmers, at the time of the third occasion of this course.

- A tutorial on how to use Dynamic Mesh solver IcoDyMFoam, by Pirooz Moradnia:
[Report](#), [Presentation](#), [Case](#)
- Implementing third order compressible flow solver for hexahedral meshes in OpenFoam, by Martin Olausson:
[Report](#), [g3dFoam.tar](#), [shockTube.tar](#)
- icoStructFoam, a Fluid-Structure Interaction Solver, by Philip Evegren:
[Report](#), [Presentation](#), [IcoStructFoam_Rev561.tgz](#) (From openfoam-extend at SourceForge, Revision 561: /trunk/Breeder/solvers/other/IcoStructFoam)
- Different ways to treat rotating geometries, by Olivier Petit:
[Report](#)
- reactingFoam tutorial (simple gas phase reaction), by Andreas Lundstr*:
[Report](#), [Test case](#)
- Free surface tutorial using interFoam and rasInterFoam, by Hassan Hemida:
[Report](#), [Test case](#), [Movie](#)
- Large Eddy Simulation of a Tilt-rotor wing with Active Flow Control, by Mohammad El-Ali:

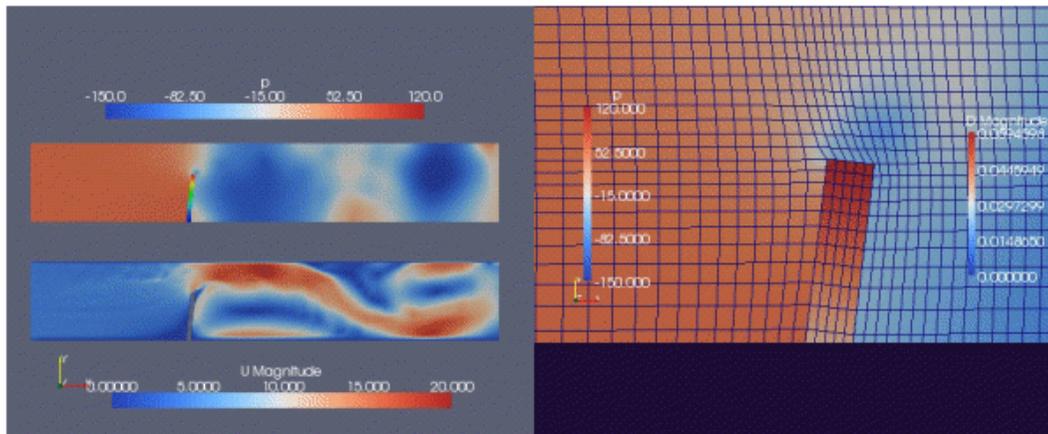
FD
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AM

FSI(Fluid Structure Interface) の、お次のレッスンは、OF-1.5-dev 用のチュートリアル。
まずは、OF-1.5-devで計算したもの。モデルは、
http://powerlab.fsb.hr/ped/kturbo/OpenFOAM/run/flappingConsoleSmall_HJ_21Mar2008.tgz より
入手したものをそのまま使用。



左の図は全体像で、上段が圧力コンタ図、下段が流速コンタ図。流入口から全体流路の1/3ほどの位置に、片持ち梁が設置してあり、これが流体の流れを受けて、変形・振動している。右側の図は、この片持ち梁の先端部分を拡大したものの。いずれもクリックすると動画で表示されるが、梁が振動している様子がよくわかる。これは、某原子力発電所のナトリウム漏洩事故の原因になった現象なんだろうな。。。と彷彿させるものがあります。

お次は、OF-1.5.xで、icoStructFoam で計算したもの。基本的には、上で使ったモデルをそのまま転用しましたが、そのままでは使えない部分を一部手直しました。

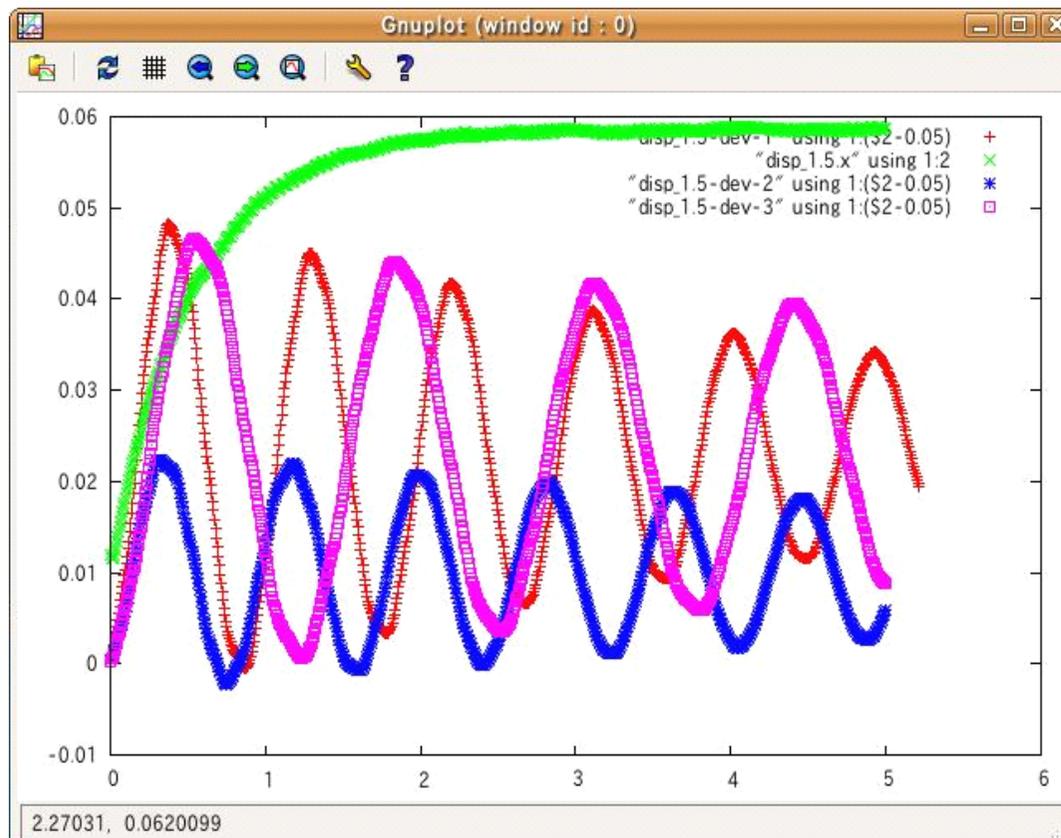


問題は、、、1.5-devのicoFsiFoam でやった結果とずいぶん異なるということです。

事前調査

<http://bit.ly/djScCr>

<http://mogura7.zenno.info/~et/wordpress/tag/fsi/>



赤のグラフがOpenFOAM-1.5-devのicoFsiFoam を使って計算したものであるのに対し、

緑は、OpenFOAM-1.5.xに追加したicoStructFoam を使って計算したもの。

アニメーションで見られた、振動の有無の違いがよくわかる。

今回、追加して計算したものが2つ。

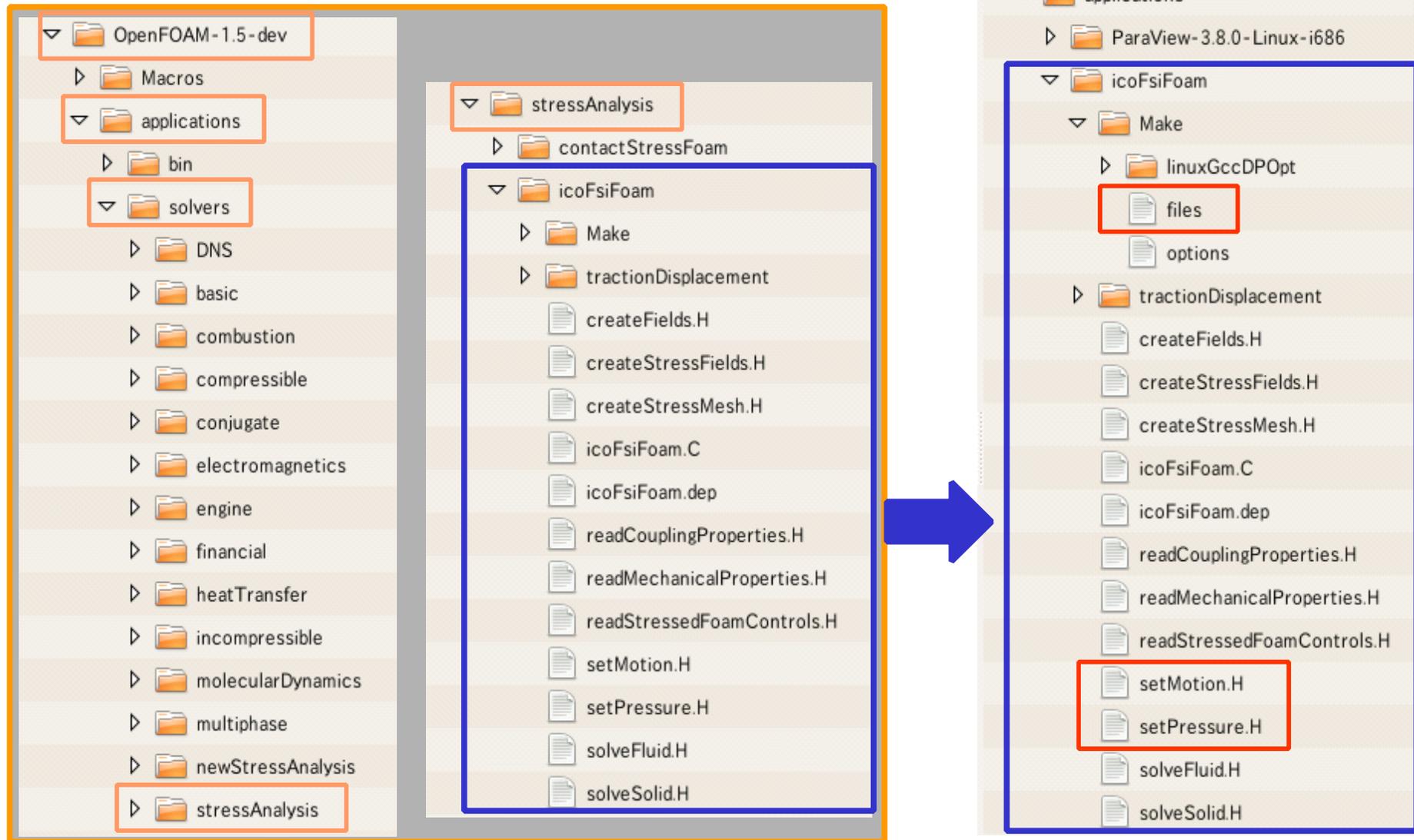
濃青・・・固体部分のメッシュを、icoStructFoamで使ったものと同等にして、icoFsiFoamにて計算

オレンジ・・・icoFsiFoam(赤)に対し固体の密度を2倍にして計算

これらの挙動変化は、およそ予想通りの結果になってくれたので、、、結論は、**FSIIには、OpenFOAM-1.5-devのicoFsiFoamを使いなさい**ということのようです。

プログラム (icoFsiFoam) の説明

プログラムの構成



DEXCS-FSI版では、一部 を改変

改変内容

<http://bit.ly/c7OMam>

<http://www.cfd-online.com/Forums/openfoam-solving/58513-fluid-structure-interaction-using-icofsiFoam-problems-3.html#post267620>

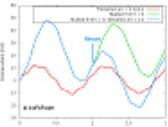
July 16, 2010, 18:25 **icoFsiFoam problem with restarted simulations** #55

7islands
Senior Member

Takuya OSHIMA
Join Date: Mar 2009
Location: Niigata City, Japan
Posts: 439
Blog Entries: 1
Rep Power: 5

Hi,
For future interests in doing FSI simulations, we are taking a look at icoFsiFoam in OF 1.5-dev in conjunction with the flappingConsole case ([flappingConsoleSmall_HJ_21Mar2008.tgz](#)), which includes several steps of saved field data up to $t = 0.024$ [s] and the simulation is setup to start from the latestTime. However, we are having problem in restarted simulations.

Here I attach a figure where the x-directional displacements at the top of the console are plotted for three cases: the red line is a restarted simulation from the saved data at $t = 0.024$ [s] (which is how one would usually run icoFsiFoam), the green line is a fresh simulation started from $t = 0$ by deleting the saved data, and the blue line is also a freshly started simulation but stopped at $t = 1$ [s] and restarted from there. There's no wonder in the difference between the red and the green/blue lines if the saved data and our data are calculated by e.g. different solvers, but what was problem to us was the discrepancy between the green and the red lines after $t = 1$ [s].



The main cause of the discrepancy, besides other insignificant ones, was sorted out to be the patch-to-patch interpolation weights between the fluid and the solid moving meshes not being updated per time step basis, hence the interpolation weights calculated at the time of simulation (re)start were constantly used during the simulation run regardless of the mesh movements. So here is what we tried to correct the issue:

Code:

```
Index: applications/solvers/stressAnalysis/icoFsiFoam/setMotion.H
=====
--- applications/solvers/stressAnalysis/icoFsiFoam/setMotion.H (revision 1790)
+++ applications/solvers/stressAnalysis/icoFsiFoam/setMotion.H (working copy)
@@ -11,6 +11,7 @@
     stressMesh.movePoints(newPoints);

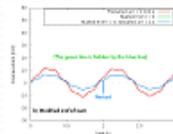
+   interpolatorSolidFluid.movePoints();
+   vectorField fluidPatchPointsDispl =
+       interpolatorSolidFluid.pointInterpolate
+       (
Index: applications/solvers/stressAnalysis/icoFsiFoam/setPressure.H
```

変更内容(つづき)

```
-----  
--- applications/solvers/stressAnalysis/icoFsiFoam/setPressure.H (revision 1790)  
+++ applications/solvers/stressAnalysis/icoFsiFoam/setPressure.H (working copy)  
@@ -2,6 +2,7 @@  
    // Setting pressure on solid patch  
    Info << "Setting pressure" << endl;  
  
+   interpolatorFluidSolid.movePoints();  
   scalarField solidPatchPressure =  
       interpolatorFluidSolid.faceInterpolate  
       (  

```

And the results with the patched icoFsiFoam are:



This time the green and the blue line agrees perfectly (up to around four significant digits) and the oscillating frequencies of all cases as well. Besides, combined with the results of other runs we have a general impression that the stability is also better. However, the displacements changed too drastically, to around an order of a magnitude smaller compared to those with the unpatched icoFsiFoam. Thus we are unsure if the omission of `movePoints()` as shown in the patch is a bug or intended for some reasons.

We'd appreciate any inputs, thoughts, comments. Thanks!

Takuya



プログラムの概要

```
1 tractionDisplacement/tractionDisplacementFvPatchVectorField.C
2 icoFsiFoam.C
3
4 EXE = $(FOAM_USER_APPBIN)/icoFsiFoam|
```

連成計算用境界条件

メインプログラム

メインプログラムの概要(1)

```
34 #include "fvCFD.H"
35 #include "dynamicFvMesh.H"
36 #include "patchToPatchInterpolation.H"
37 #include "tractionDisplacement/tractionDisplacementFvPatchVectorField.H"
38 #include "tetFemMatrices.H"
39 #include "tetPointFields.H"
40 #include "faceTetPolyPatch.H"
41 #include "tetPolyPatchInterpolation.H"
42 #include "fixedValueTetPolyPatchFields.H"
43
44 #include "pointMesh.H"
45 #include "pointFields.H"
46 #include "volPointInterpolation.H"
47
48 // *****
49
50 int main(int argc, char *argv[])
51 {
52 #   include "setRootCase.H"
53 #   include "createTime.H"
54 #   include "createDynamicFvMesh.H"
55 #   include "createStressMesh.H"
56 #   include "createFields.H"
57 #   include "createStressFields.H"
58 #   include "readMechanicalProperties.H"
59 #   include "readCouplingProperties.H"
60 #   include "readTimeControls.H"
61
62 #   include "initContinuityErrs.H"
63
64 // *****
```

FSI用境界条件
tractionDisplacement

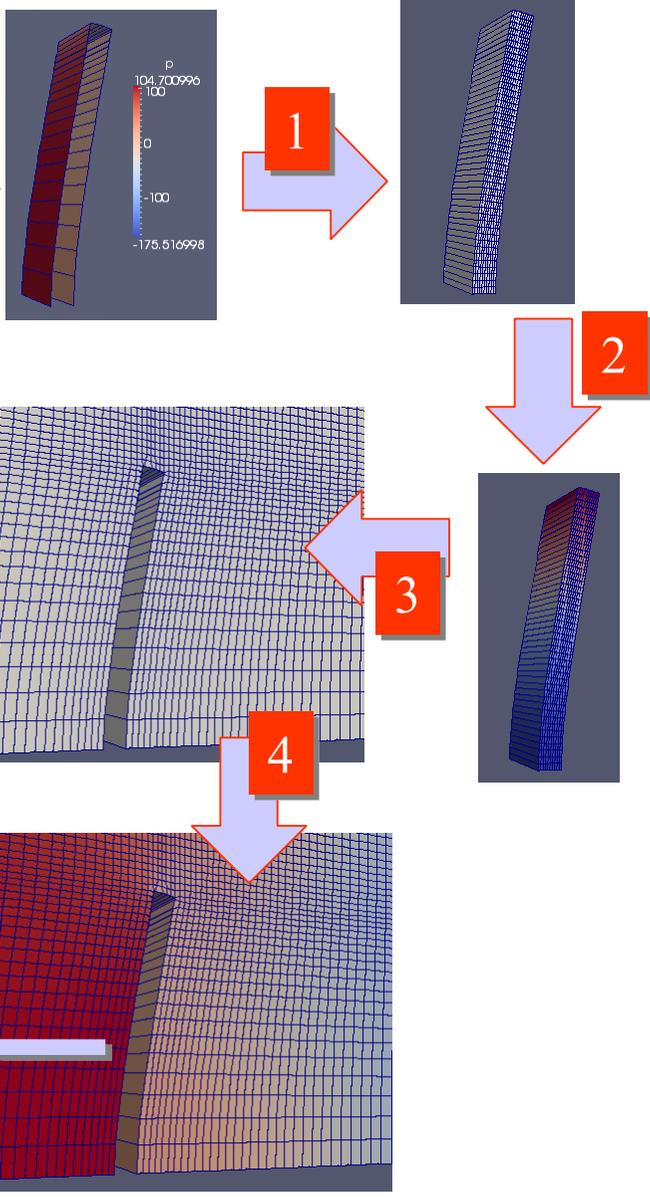


icoFsiFoam用
カスタマイズ部分

流体、固体部で、
各々メッシュ作成
初期場設定

メインプログラムの概要(2)

```
66 Info<< "¥nStarting time loop¥n" << endl;  
67  
68 while (runTime.run())  
69 {  
70 #   include "readPISOControls.H"  
71 #   include "readTimeControls.H"  
72 #   include "CourantNo.H"  
73 #   include "setDeltaT.H"  
74  
75   runTime++;  
76  
77   Info<< "Time = " << runTime.timeName() << nl << endl;  
78  
79 #   include "setPressure.H" ← 1  
80 #   include "solveSolid.H" ← 2  
81  
82 #   include "setMotion.H" ← 3  
83 #   include "solveFluid.H" ← 3  
84  
85   runTime.write();  
86  
87   Info<< "ExecutionTime = "  
88     << runTime.elapsedCpuTime() << "  
89     << " s¥n¥n" << endl;  
90 }  
91 Info<< "End¥n" << endl;  
92  
93 return(0);  
94 }  
95 }
```



setPressure

```
1 {  
2 // Setting pressure on solid patch  
3 Info << "Setting pressure" << endl;  
4  
5 interpolatorFluidSolid.movePoints();  
6 scalarField solidPatchPressure =  
7     interpolatorFluidSolid.faceInterpolate  
8     (  
9         p.boundaryField()[fluidPatchID]  
10    );  
11  
12    solidPatchPressure *= rhoFluid.value();  
13  
14    tForce.pressure() = solidPatchPressure;  
15  
16  
17    vector totalPressureForce =  
18        sum  
19        (  
20            p.boundaryField()[fluidPatchID]*  
21            mesh.Sf().boundaryField()[fluidPatchID]  
22        );  
23  
24  
25    Info << "Total pressure force = " << totalPressureForce << endl;  
26 }
```



オリジナル
改変(追加)部分

solveSolid

```
2 # include "readStressedFoamControls.H"
3
4 int iCorr = 0;
5 scalar initialResidual = 0;
6
7 do
8 {
9     volTensorField gradU = fvc::grad(Usolid);
10
11     fvVectorMatrix UEqn
12     (
13         fvm::d2dt2(Usolid)
14         ==
15         fvm::laplacian(2*mu + lambda, Usolid, "laplacian(DU,U)")
16         + fvc::div
17         (
18             mu*gradU.T() + lambda*(I*tr(gradU)) - (mu + lambda)*gradU,
19             "div(sigma)"
20         )
21     );
22
23     initialResidual = UEqn.solve().initialResidual();
24
25 } while (initialResidual > convergenceTolerance && ++iCorr < nCorr);
26 }
```

solidDisplacementFoam.C とほぼ同じ

setMotion

```

2 // Setting mesh motion
3
4 pointVectorField solidPointsDispl =
5     cpi.interpolate(Usolid - Usolid.oldTime());
6
7 vectorField newPoints =
8     stressMesh.points()
9     + solidPointsDispl.internalField();
10
11 stressMesh.movePoints(newPoints);
12
13 interpolatorSolidFluid.movePoints();
14
15 vectorField fluidPatchPointsDispl =
16     interpolatorSolidFluid.pointInterpolate
17     (
18         solidPointsDispl.boundaryField()[solidPatchID].
19         patchInternalField()
20     );
21
22 motionUFluidPatch ==
23     tppi.pointToPointInterpolate
24     (
25         fluidPatchPointsDispl/runTime.deltaT().value()
26     );
27
28 mesh.update();
29
30 # include "volContinuity.H"
31
32 Info << "Motion magnitude: mean = "
33     << average(mag(Usolid.boundaryField()[solidPatchID]))
34     << " max = "
35     << max(mag(Usolid.boundaryField()[solidPatchID])) << endl;
36 }

```



オリジナル
 改変(追加)部分

solveFluid

```

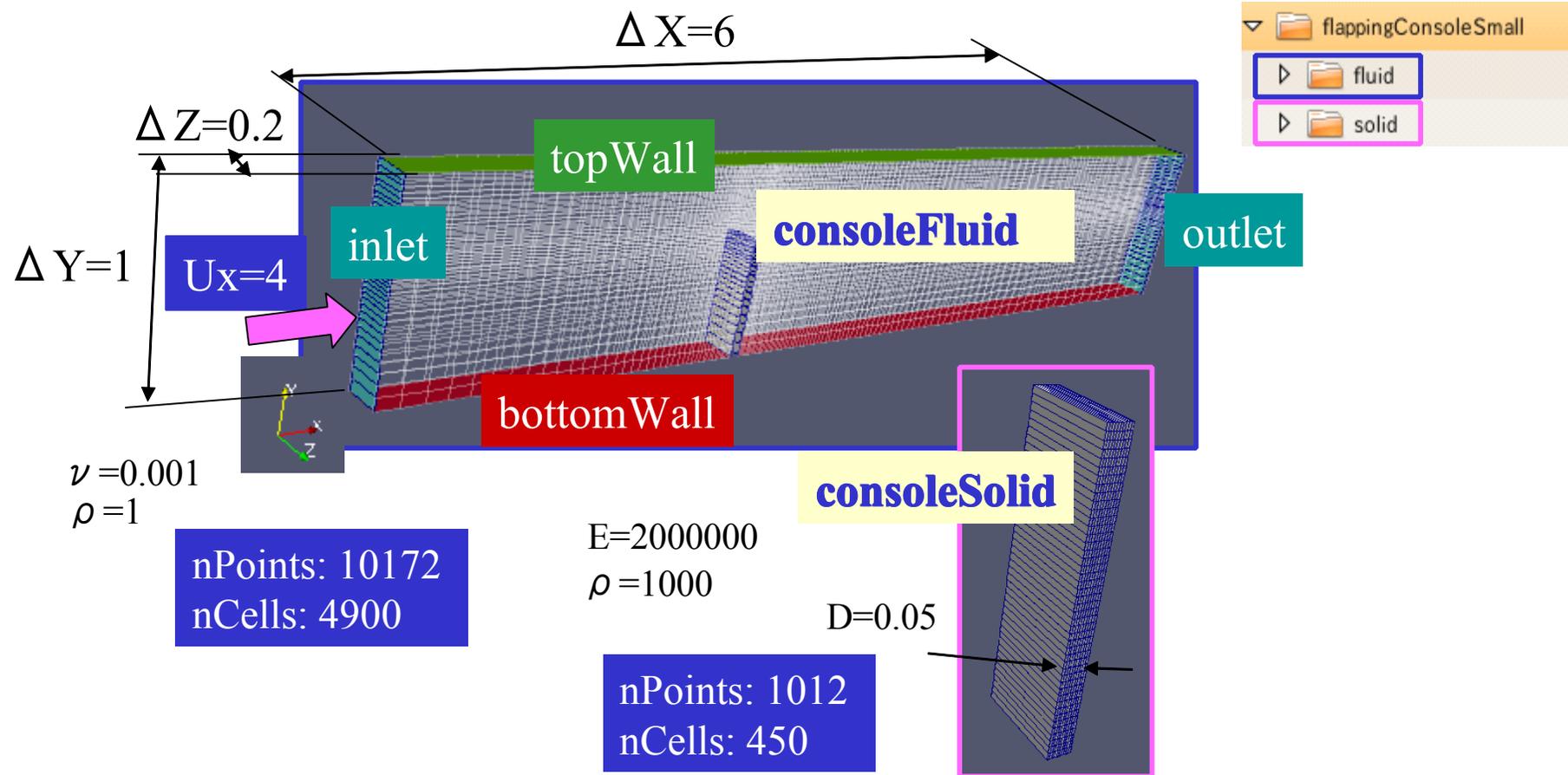
2 // SIMPLE loop
3
4 for (int corr=0; corr<nCorr; corr++)
5 {
6     fvVectorMatrix UEqn
7     (
8         fvm::ddt(U)
9         + fvm::div(phi, U)
10        - fvm::laplacian(nu, U)
11    );
12
13    UEqn.relax();
14
15    solve(UEqn == -fvc::grad(p));
16
17    U = UEqn.H()/UEqn.A();
18    U.correctBoundaryConditions();
19
20    adjustPhi(phi, U, p);
21
22    phi = fvc::interpolate(U) & mesh.Sf();
23
24    p.storePrevIter();
25
26    for (int nonOrth=0; nonOrth<=nNonOrthCorr; nonOrth++)
27    {
28        fvScalarMatrix pEqn
29        (
30            fvm::laplacian(1.0/UEqn.A(), p) == fvc::div(phi)
31        );
32
33        pEqn.setReference(pRefCell, pRefValue);
34        pEqn.solve();
35
36        if (nonOrth == nNonOrthCorr)
37        {
38            phi -= pEqn.flux();
39        }
40    }
41
42    p.relax();
43
44 #    include "movingMeshContinuityErrs.H"
45
46    U -= fvc::grad(p)/UEqn.A();
47    U.correctBoundaryConditions();
48
49    // Make the fluxes relative
50    phi -= fvc::meshPhi(U);
51 }

```

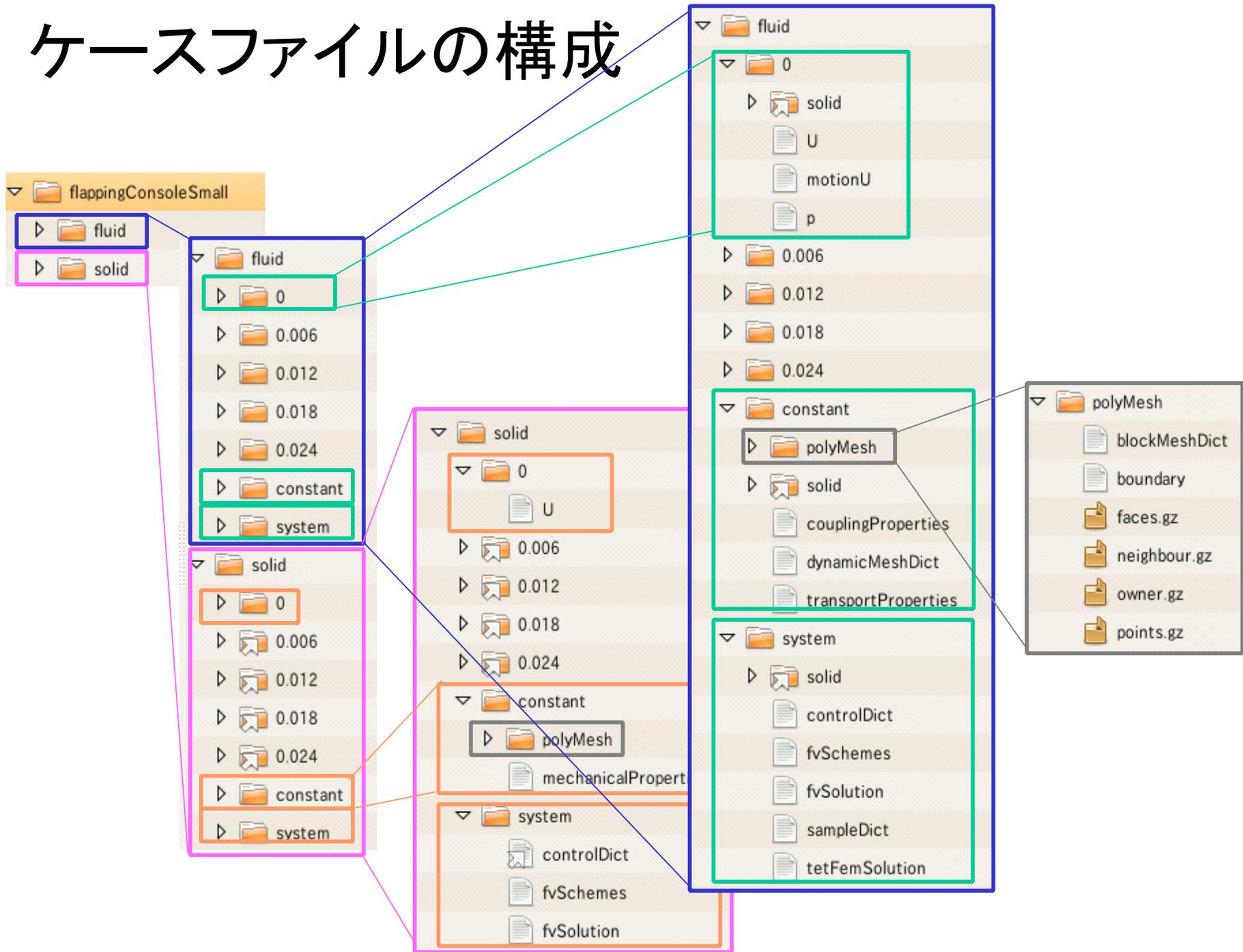
icoFoam.C
(PISO loop)
↓ (?)
SIMPLE loop

公開ケースの説明

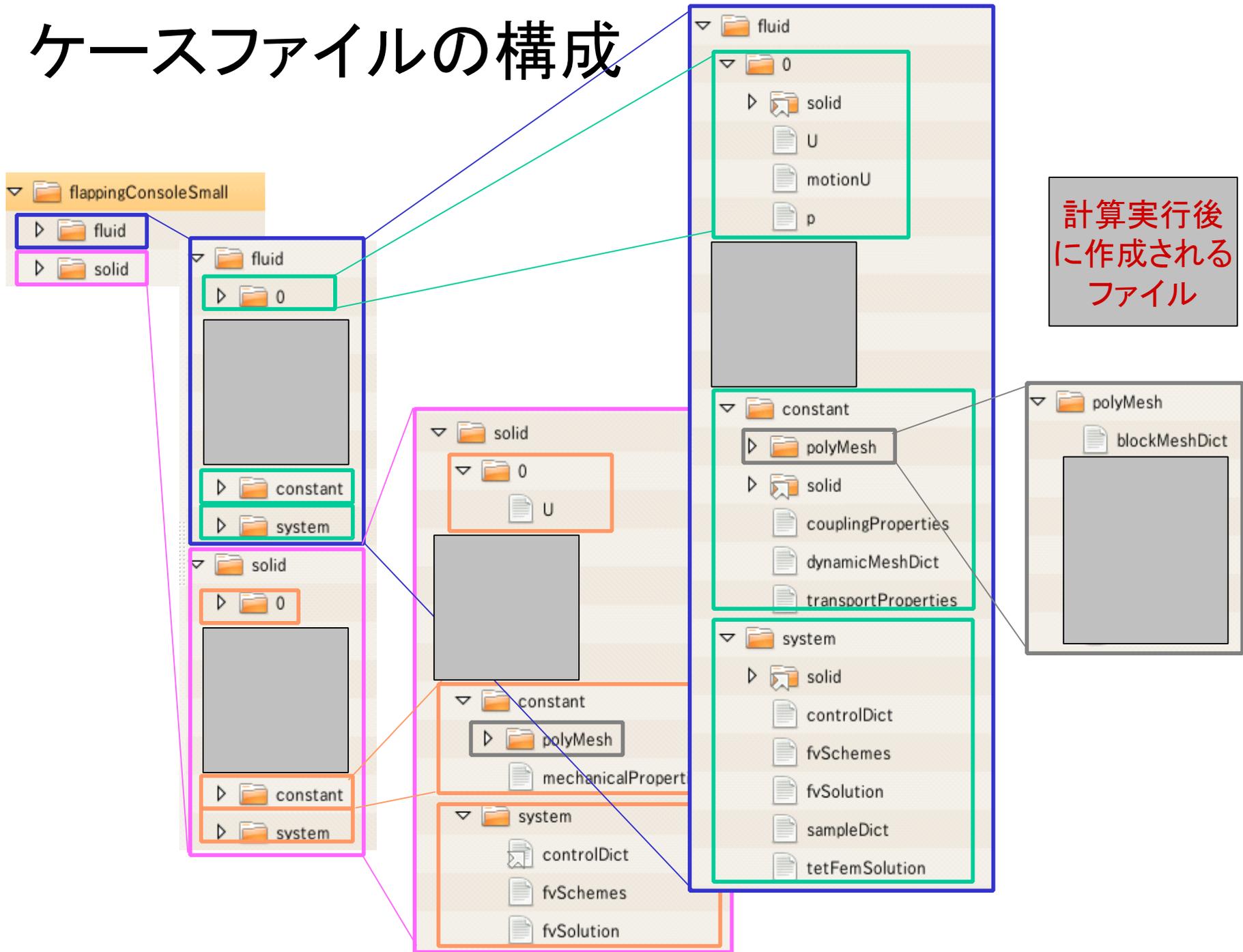
http://powerlab.fsb.hr/ped/kturbo/OpenFOAM/run/flappingConsoleSmall_HJ_21Mar2008.tgz



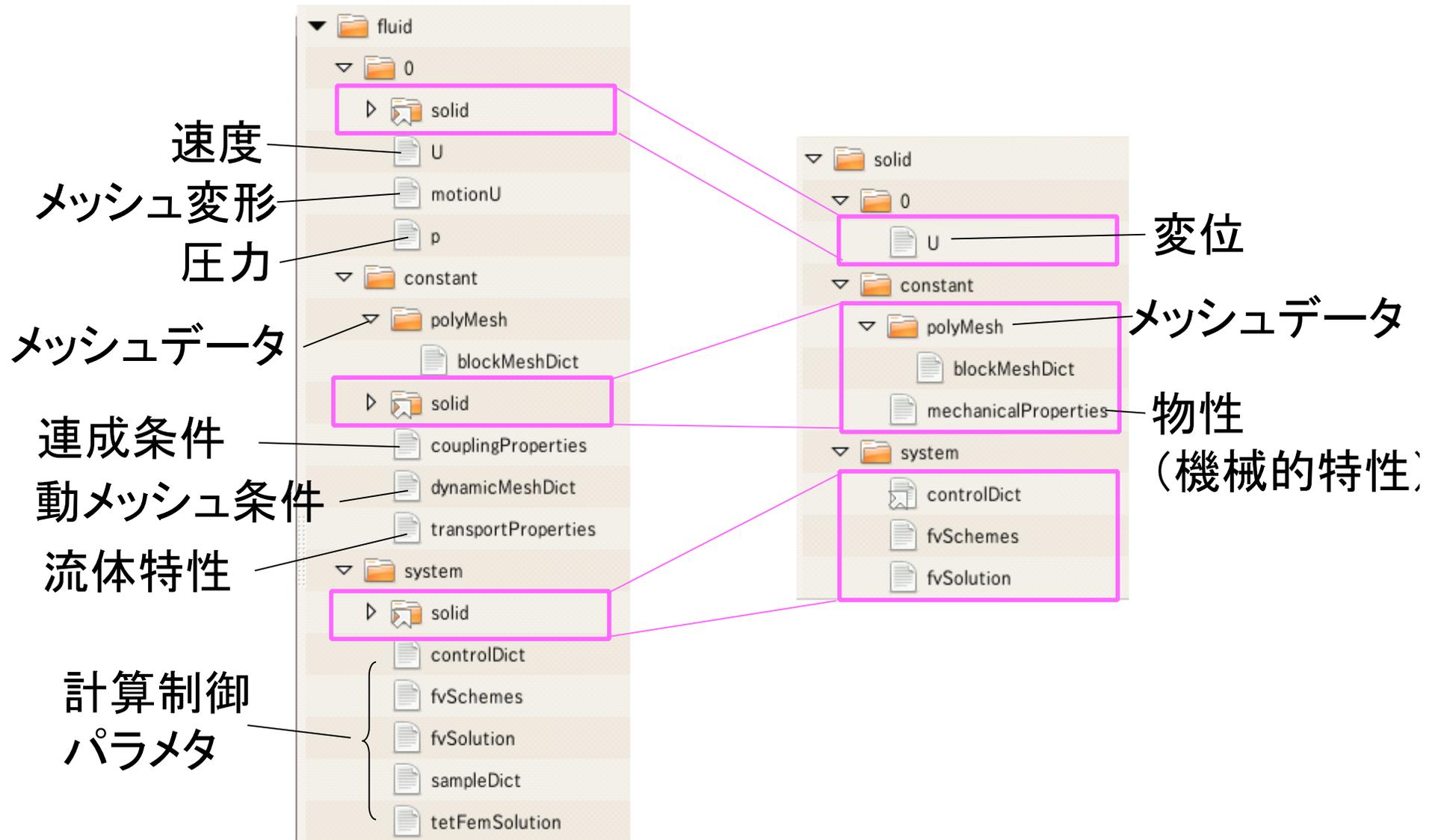
ケースファイルの構成



ケースファイルの構成

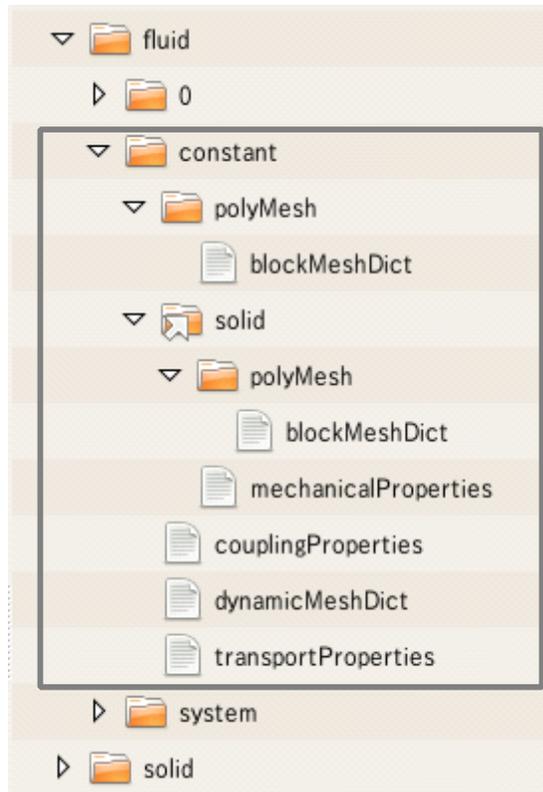


ケースファイルの構成(計算に必要なデータ)

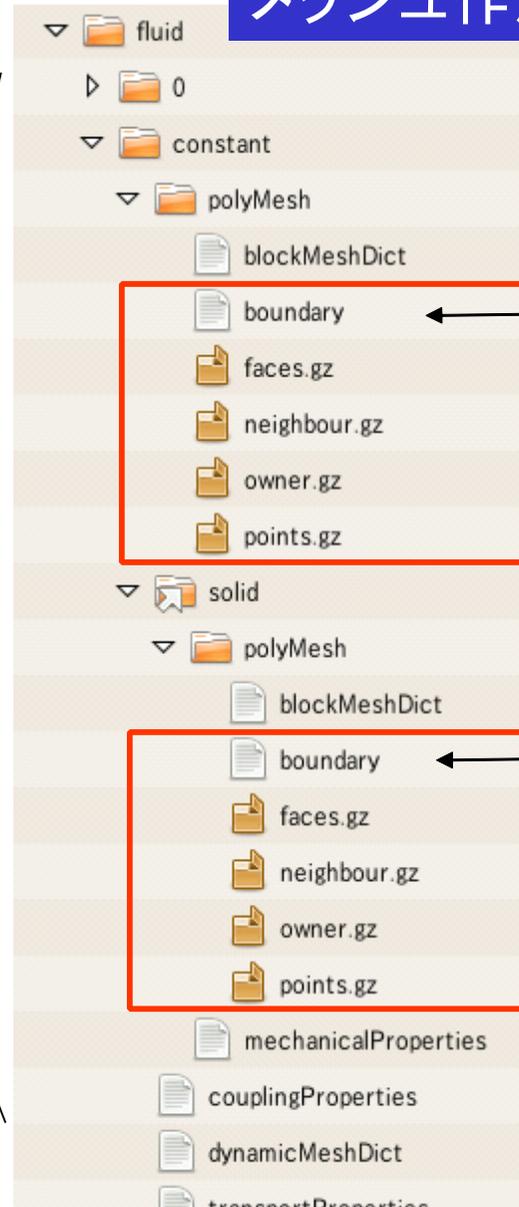


ケースファイルの構成 (メッシュ作成時点)

メッシュ作成前



メッシュ作成後



流体部

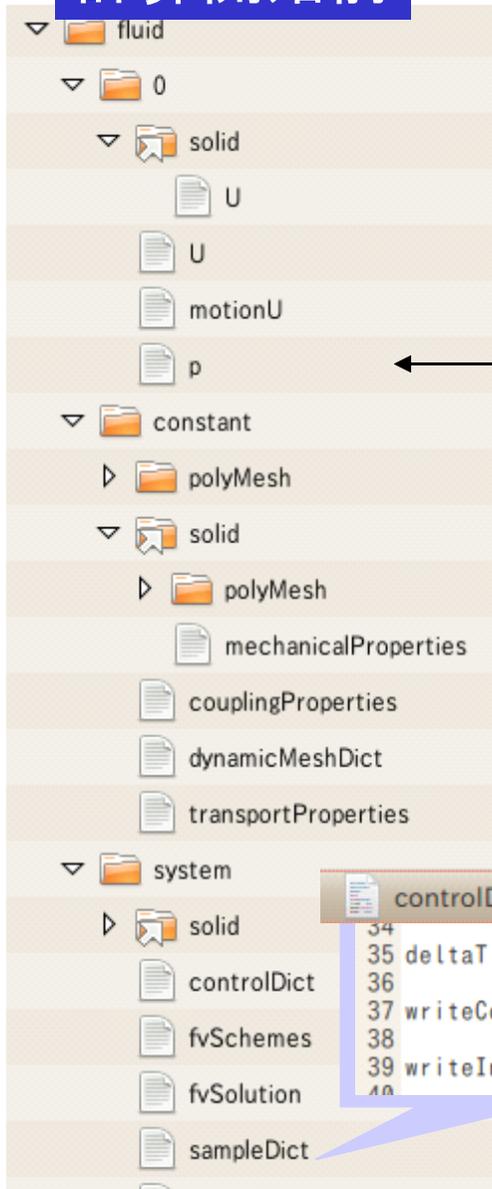
境界名定義ファイル
メッシュ定義データ

固体部

境界名定義ファイル
メッシュ定義データ

ケースファイルの構成(計算開始後)

計算開始前



計算開始後



流体部メッシュ座標

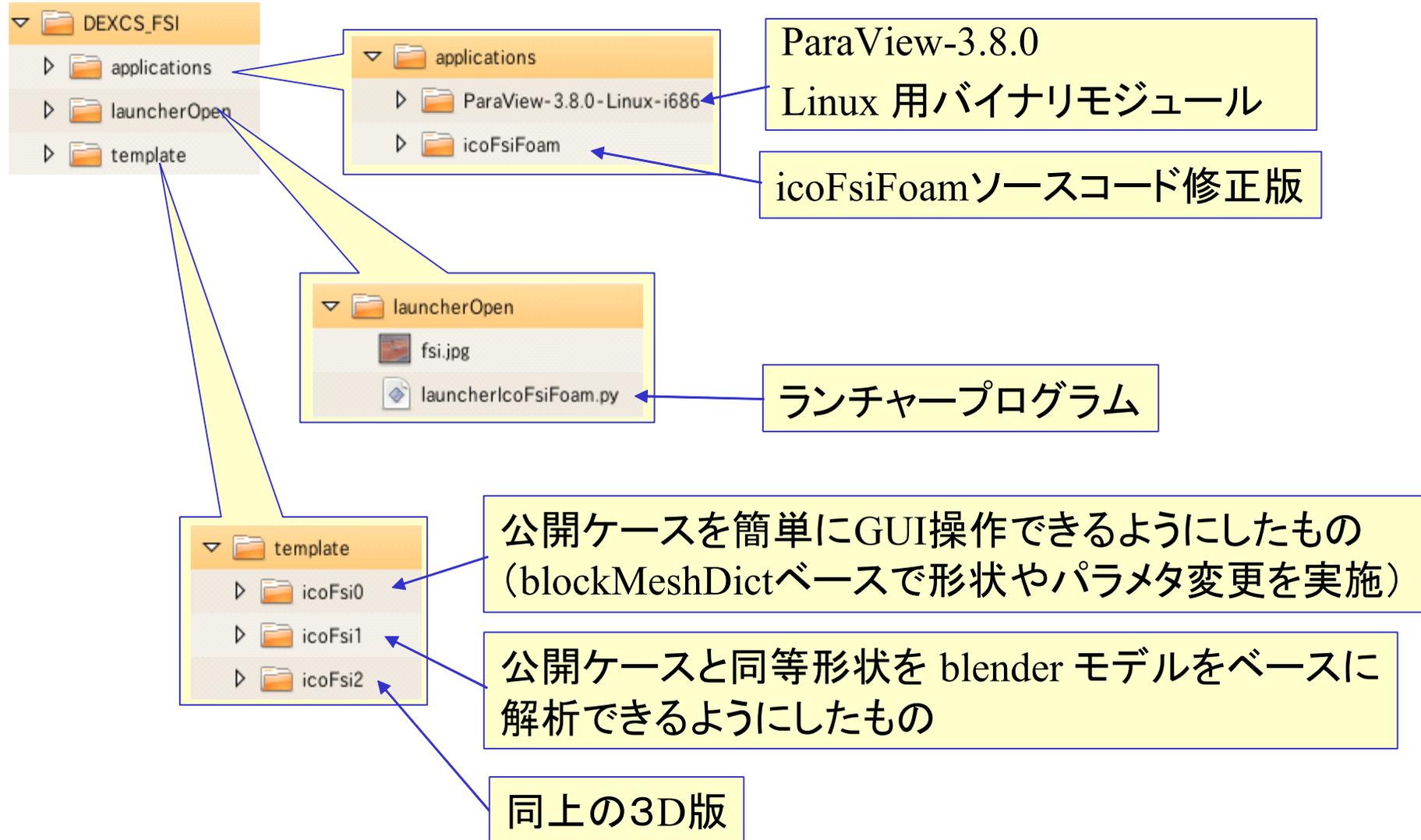
固体部メッシュ座標

0.006 sec
毎に出力

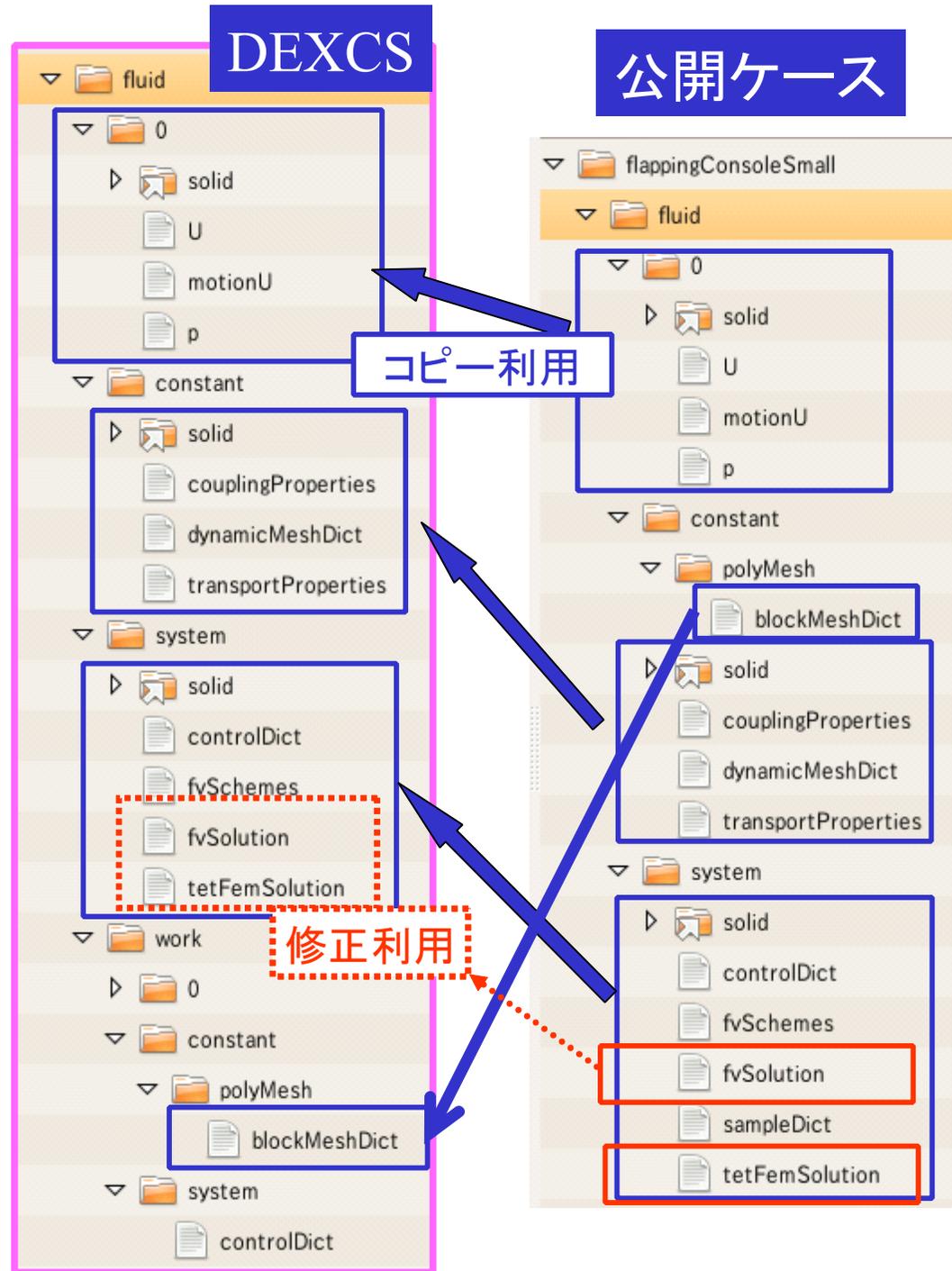
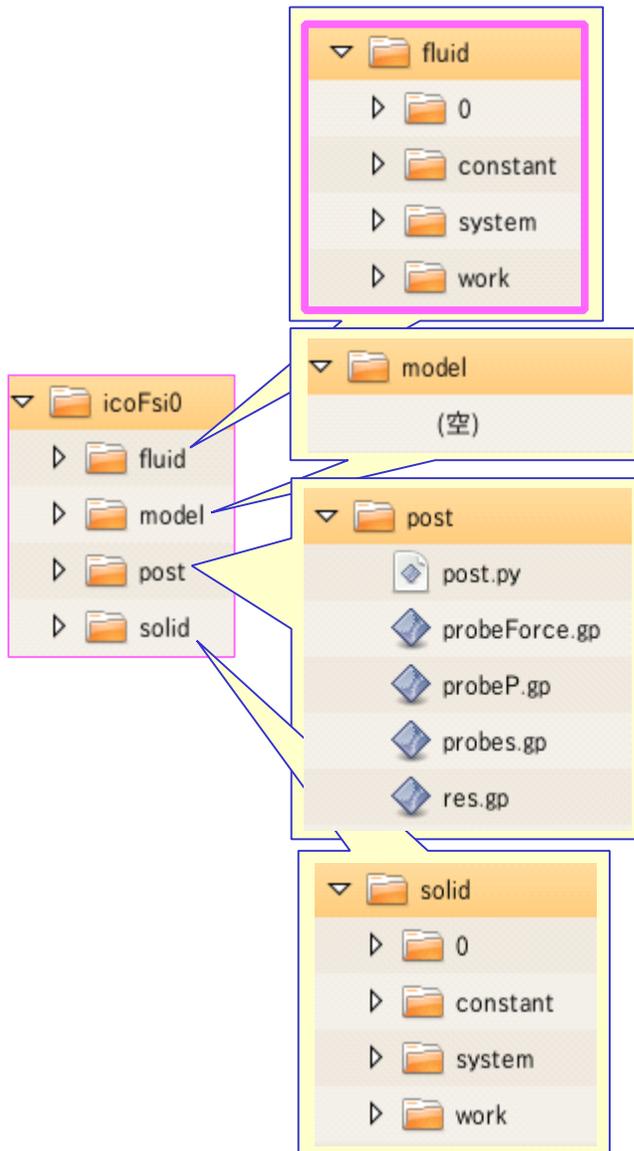
```
controlDict
34
35 deltaT      0.0003;
36
37 writeControl  timeStep;
38
39 writeInterval 20;
```

DEXCS_FSI ランチャーの説明

DEXCS-FSI のファイル構成



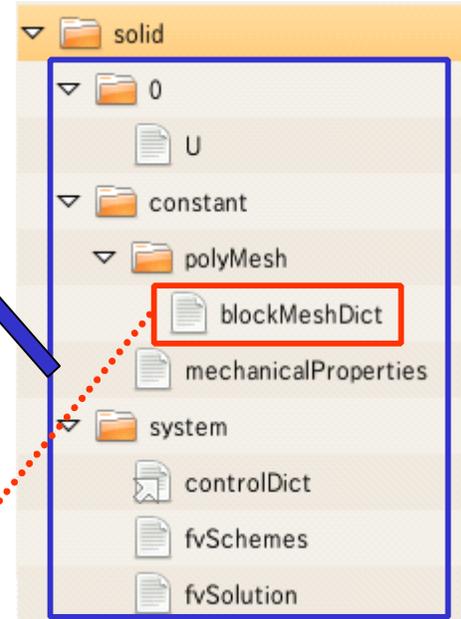
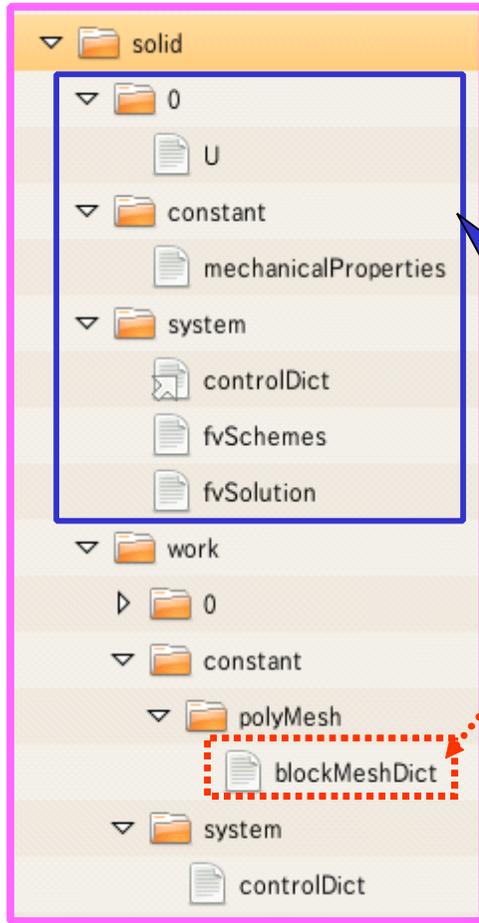
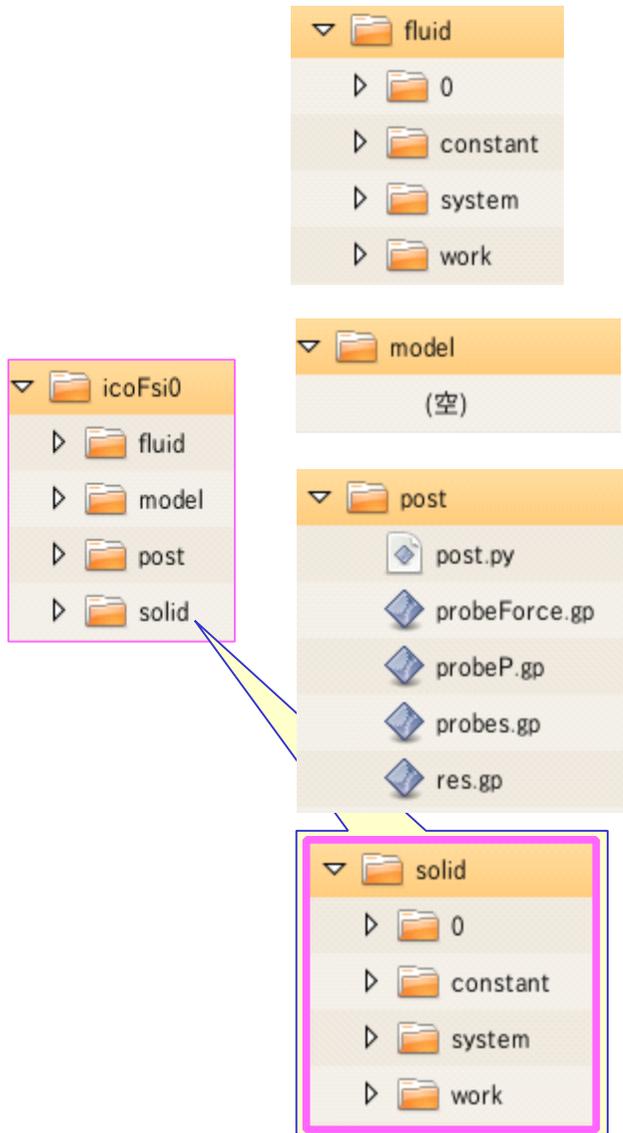
DEXCS template (icoFsi0)



DEXCS template (icoFsi0)

DEXCS

公開ケース



公開ケースのファイル構造を基本的に踏襲
但し、正しく動作しない部分(赤枠部)は修正を実施
workフォルダ下にてメッシュ作成

DEXCS_FSIランチャーによる解析実行 (標準モデルの場合)

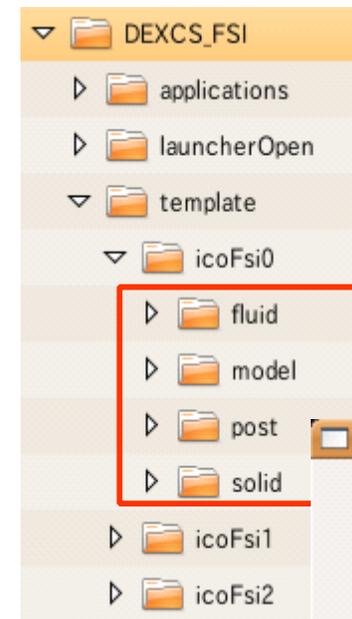
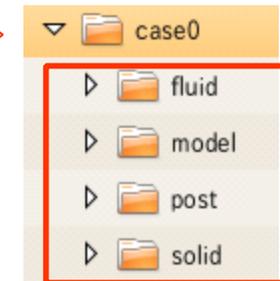
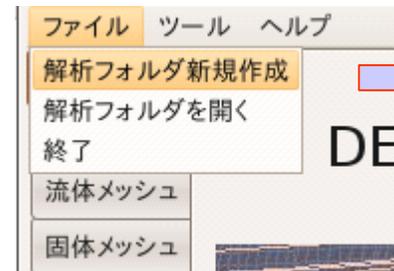
公開ケースで使用しているパラメタ	
そのままでは使えず、変更した	
そのまま使うしかなさそう	
他にも選択の余地がありそう	
ケーススタディ、検証対象になる	
DEXCS固有のカスタマイズパラメタ	

(パラメタ説明図の例)



```
dynamicMeshDict
23 // *****
24
25 dynamicFvMesh dynamicMotionSolverFvMesh;
26
27 twoDMotion yes;
28
29 solver laplaceFaceDecomposition;
30
31 diffusivity quadratic;
32
33 frozenDiffusion on;
34
35 distancePatches
36 (
37     consoleFluid
38 );
39
```

解析フォルダの設定



新規作成すると、
テンプレートファイルが
自動でコピーされる



流体メッシュ

blockMeshDictの確認と編集

The image shows a workflow for editing and displaying a block mesh in ANSYS Fluent. The main window is titled "現在の解析フォルダ: /home/et/Desktop/case1L".

- EditBlockMeshDictFluid**: A dialog box with the text "blockMeshDict を編集します" and buttons for "OK" and "Cancel / End".
- RunDisplayBlockMeshFluid**: A dialog box with the text "DisplayBlockMesh を実行します" and buttons for "OK" and "Cancel / End".
- blockMeshDict**: A text editor showing the mesh definition. A dashed purple box highlights the first four lines of the "hex" block definitions. An orange arrow points from this box to the text below.
- blockMesh-Viewer**: A 3D visualization of the mesh. A green rectangular block is shown with red node numbers (e.g., 820, 416, 922, 118, 112, 7, 19, 3, 15, 214, 012). An orange arrow points from the text below to this viewer.

形状やメッシュ分割方案を変更したい場合には blockMeshDictを直接変更する

変更の際には、ブロックや節点番号表示を見ながら作業すると良い

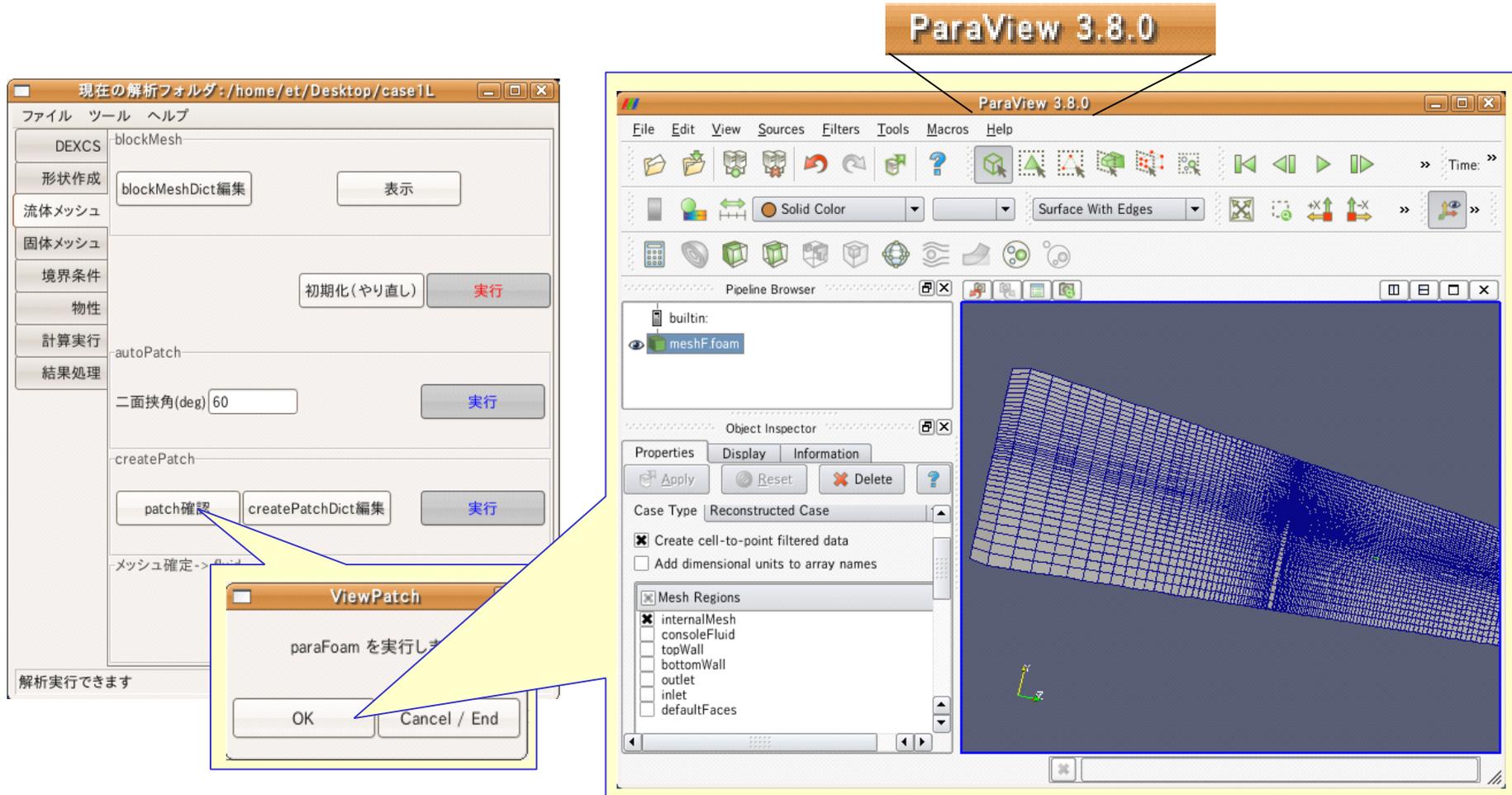
流体メッシュ

メッシュの作成 (blockMeshの実行)

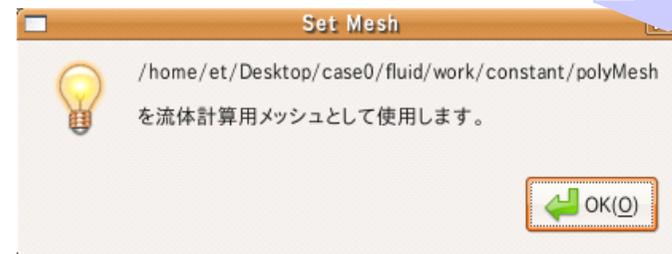
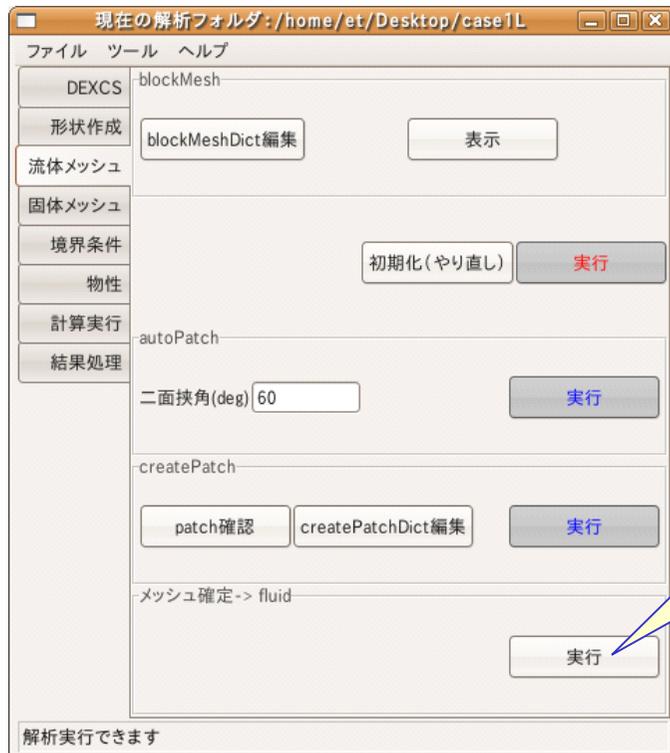


流体メッシュ

メッシュの確認



流体メッシュ -メッシュ確定



固体メッシュの作成

```
blockMeshDict
22
23 // *****
24
25 convertToMeters 1;
26
27 vertices
28 (
29   (0 0 -0.1)
30   (0.05 0 -0.1)
31   (0.05 0.6 -0.1)
32   (0 0.6 -0.1)
33   (0 0 0.1)
34   (0.05 0 0.1)
35   (0.05 0.6 0.1)
36   (0 0.6 0.1)
37 );
38
39 blocks
40 (
41   hex (0 1 2 3 4 5 6 7) (10 45 1)
42 );
43
44 edges
45 (
46 );
47
48 patches
49 (
50   patch consoleSolid
51   (
52     (3 7 6 2)
53     (0 4 7 3)
54     (2 6 5 1)
55   )
56   patch consoleFixed
57   (
58     (1 5 4 0)
59   )
60 )
```

現在の解析フォルダ: /home/et/Desktop/case1L

ファイル ツール ヘルプ

DEXCS blockMesh

形状作成 blockMeshDict編集 表示

流体メッシュ

固体メッシュ

境界条件

物性

計算実行

結果処理

初期化(やり直し) 実行

二面挟角(deg) 60 実行

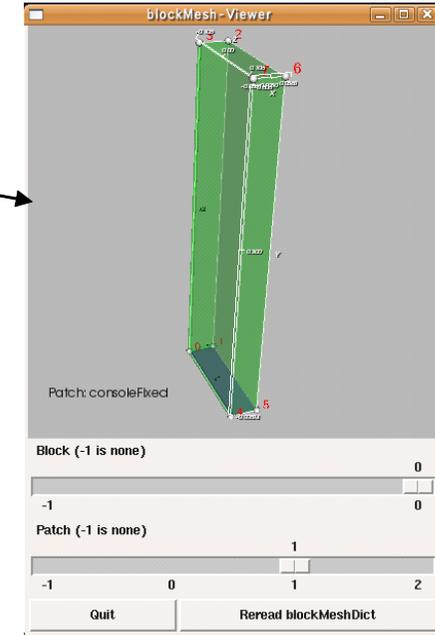
createPatch

patch確認 createPatchDict編集 実行

-メッシュ確定-> solid

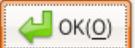
実行

解析実行できます



Set Mesh

 /home/et/Desktop/case0/solid/work/constant/polyMesh
を個体計算用メッシュとして使用します。

 OK(O)

境界条件

現在の解析フォルダ: /home/et/Desktop/case0

ファイル ツール ヘルプ

DEXCS 流体

形状作成

流体メッシュ 初期化 patch名取得 編集

固体メッシュ

境界条件

物性 固体

計算実行

結果処理

初期化 patch名取得 編集

EditAll

p, U, motionU, [boundary] を編集します

OK Cancel / End

U (~ /Desktop/case2/fluid/0) - gedit

ファイル(E) 編集(E) 表示(V) 検索(S) ツール(T) ドキュメント(D) ヘルプ(H)

新規 開く 保存 印刷... 元に戻す やり直す 切り取り

p U motionU boundary

```
27 internalField uniform (0 0 0);
28
29 boundaryField
30 {
31   consoleFluid
32   {
33     type          movingWallVelocity;
34     value         uniform (0 0 0);
35   }
36   topWall
37   {
38     type          value
39     value         uniform (0 0 0);
40   }
41 }
42 consoleFixed
43 {
44   type          fixedValue;
45   value         uniform (0 0 0);
```

U (~ /Desktop/case2/fluid/0/solid) - gedit

ファイル(E) 編集(E) 表示(V) 検索(S) ツール(T) ドキュメント(D) ヘルプ(H)

新規 開く 保存 印刷... 元に戻す やり直す 切り取り

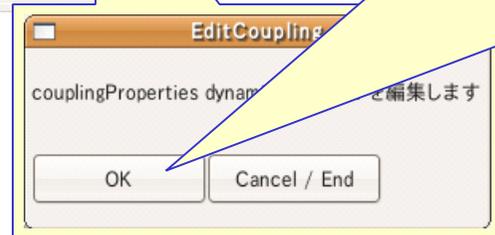
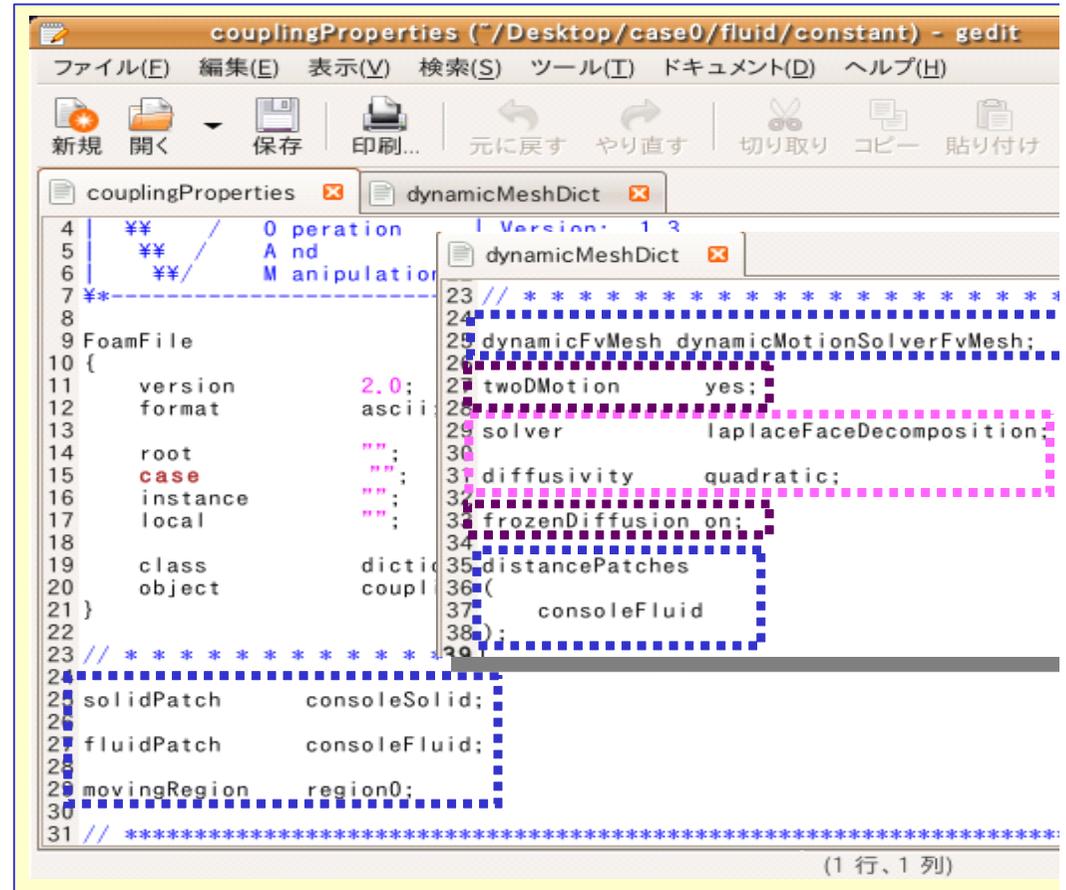
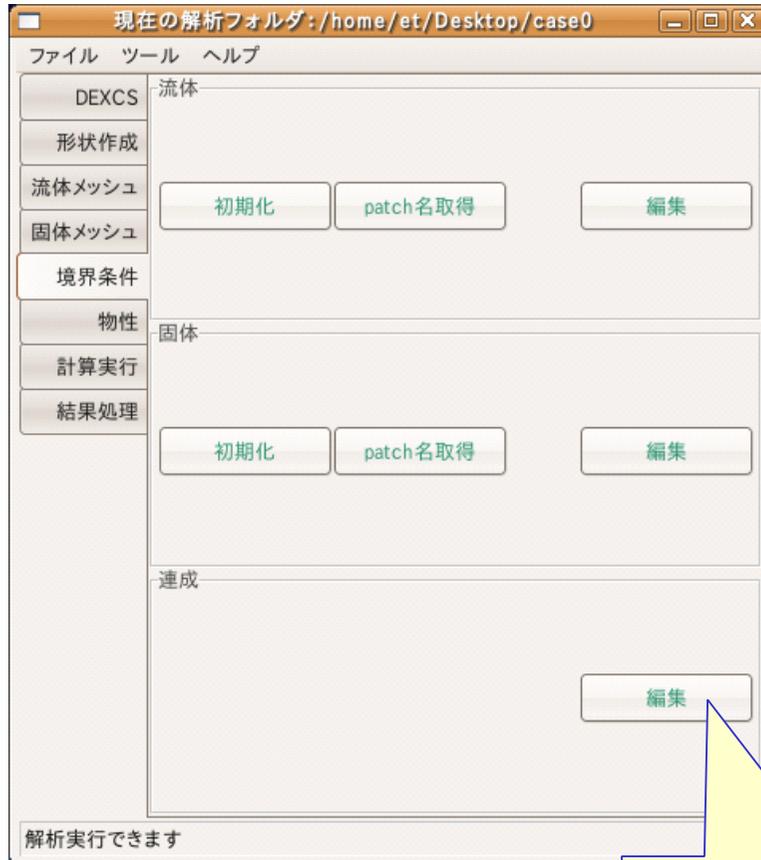
U boundary

```
33 {
34 consoleSolid
35 {
36   type          tractionDisplacement;
37   traction      uniform (0 0 0);
38   pressure      uniform 0;
39   value         uniform (0 0 0);
40 }
41 }
42 consoleFixed
43 {
44   type          fixedValue;
45   value         uniform (0 0 0);
```

p U motionU boundary

```
33 consoleFluid
34 {
35   type          fixedValue;
36   value         uniform (0 0 0);
37 }
38 }
```

境界条件(連成)



物性

```
transportProperties 流体特性
12 format      ascii;
13
14 root        "";
15 case       "";
16 instance   "";
17 local      "";
18
19 class       dictionary;
20 object     transportProperties;
21 }
22
23 // *****
24
25 nu          nu [0 2 -1 0 0 0 0] 0.001;
26
27 rho        rho [1 -3 0 0 0 0 0] 1;
28
29
```

動粘性係数

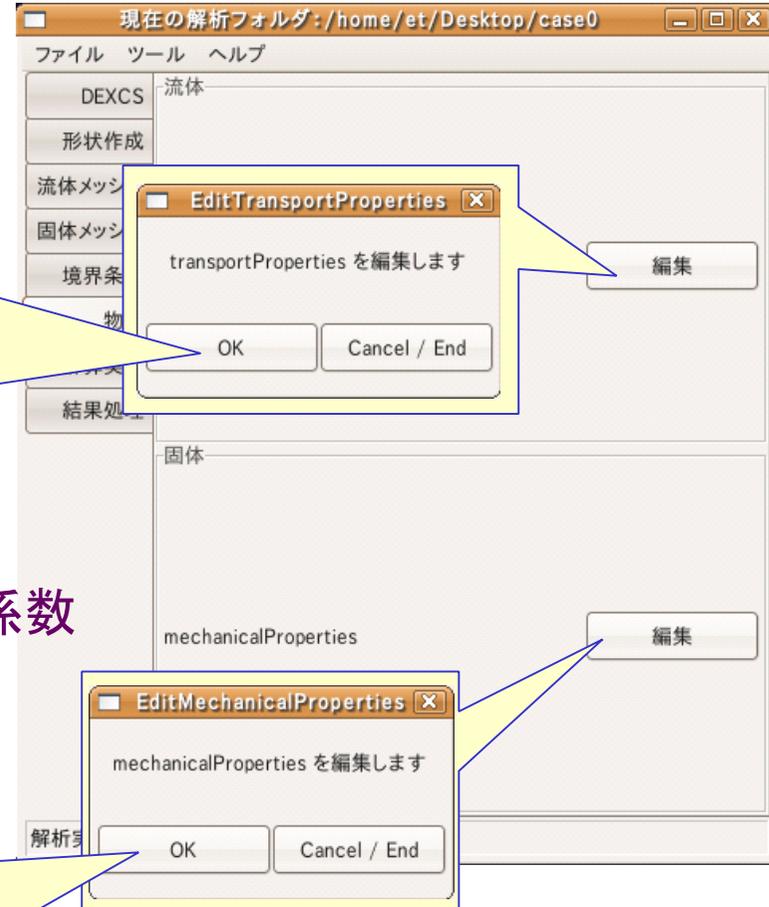
密度

```
mechanicalProperties 固体特性
(機械材料特性)
16 instance   "";
17 local      "";
18
19 class       dictionary;
20 object     mechanicalProperties;
21 }
22
23 // *****
24
25 rho        rho [1 -3 0 0 0 0 0] 1000;
26
27 nu         nu [0 0 0 0 0 0 0] 0.3;
28
29 E          E [1 -1 -2 0 0 0 0] 1.2e+6;
30
31 planeStress yes;
32
```

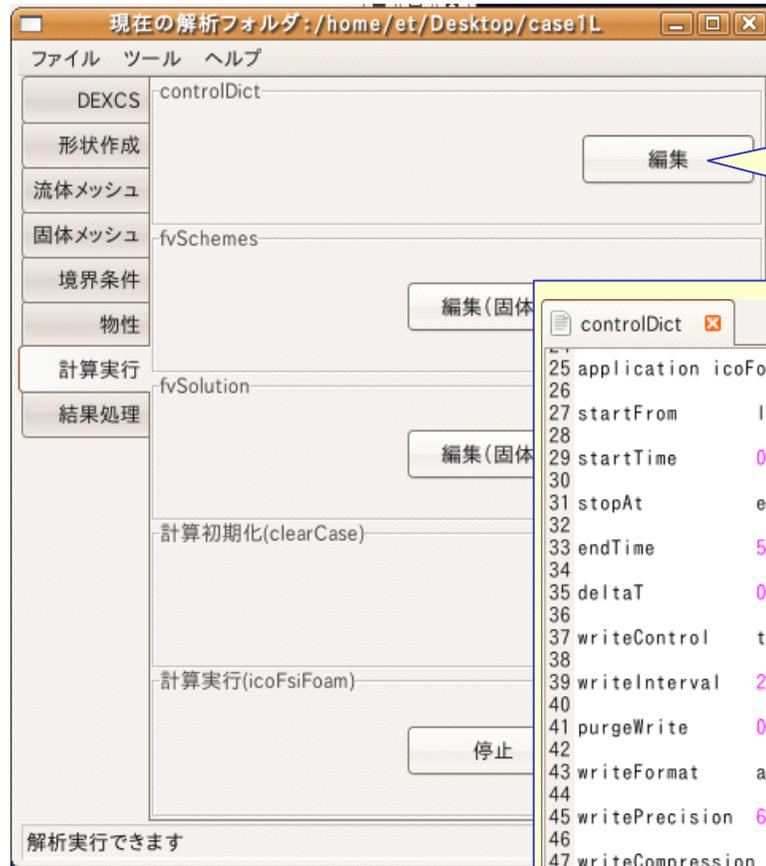
密度

ポアソン比

ヤング率



計算実行 (controlDict)

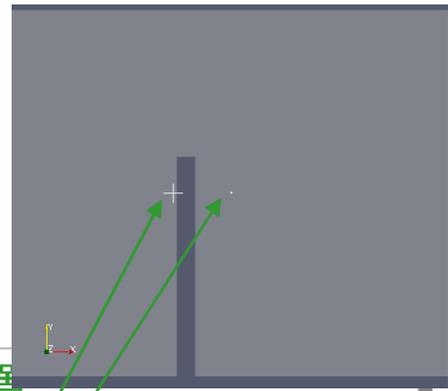


```
controlDict
25 application icoFoam;
26
27 startFrom latestTime;
28
29 startTime 0;
30
31 stopAt endTime;
32
33 endTime 50;
34
35 deltaT 0.0003;
36
37 writeControl timeStep;
38
39 writeInterval 20;
40
41 purgeWrite 0;
42
43 writeFormat ascii;
44
45 writePrecision 6;
46
47 writeCompression compressed;
48
49 timeFormat general;
50
51 timePrecision 6;
52
53 runTimeModifiable yes;
54
55 adjustTimeStep no;
56
57 maxCo 0.5;
58
```

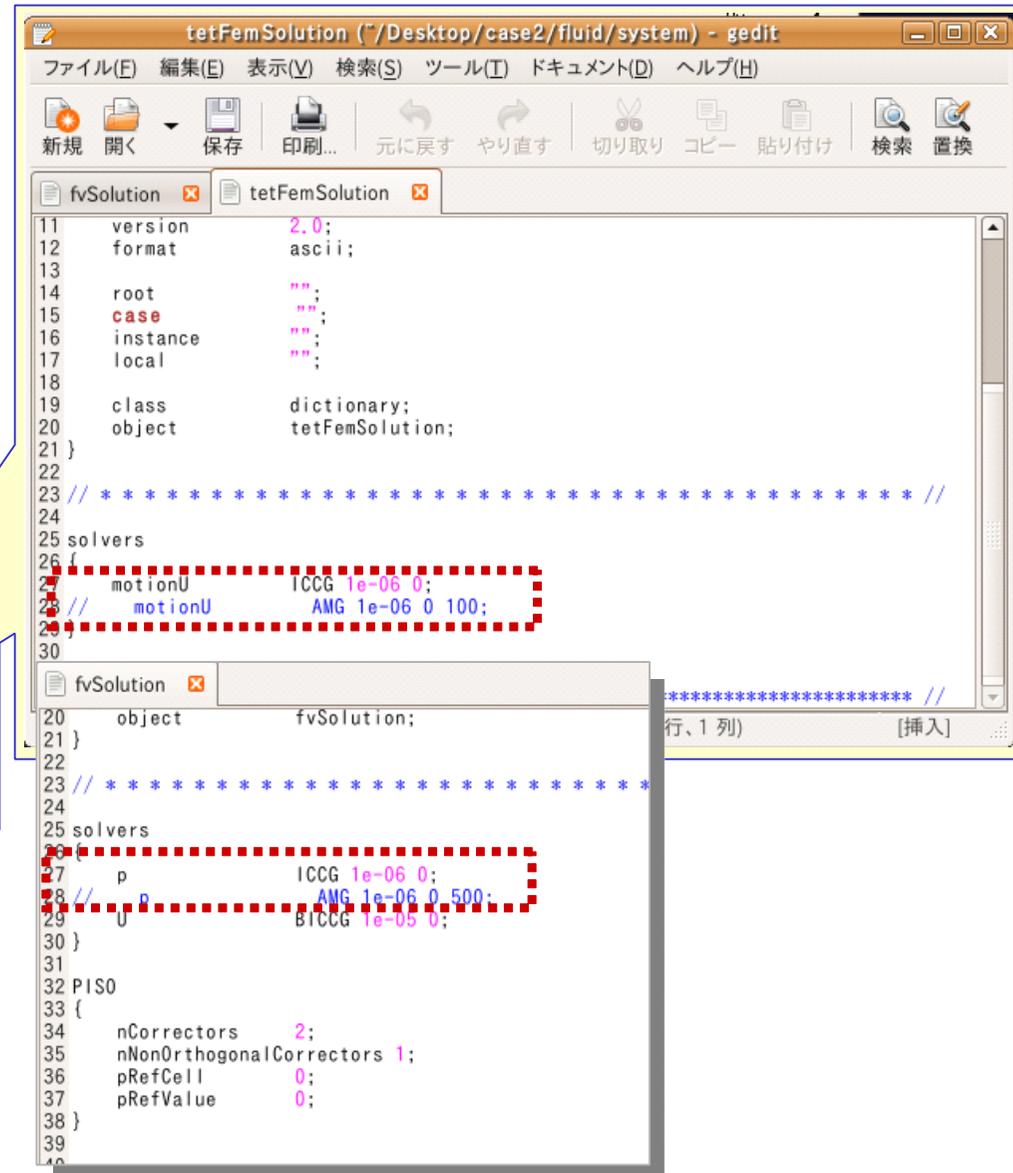
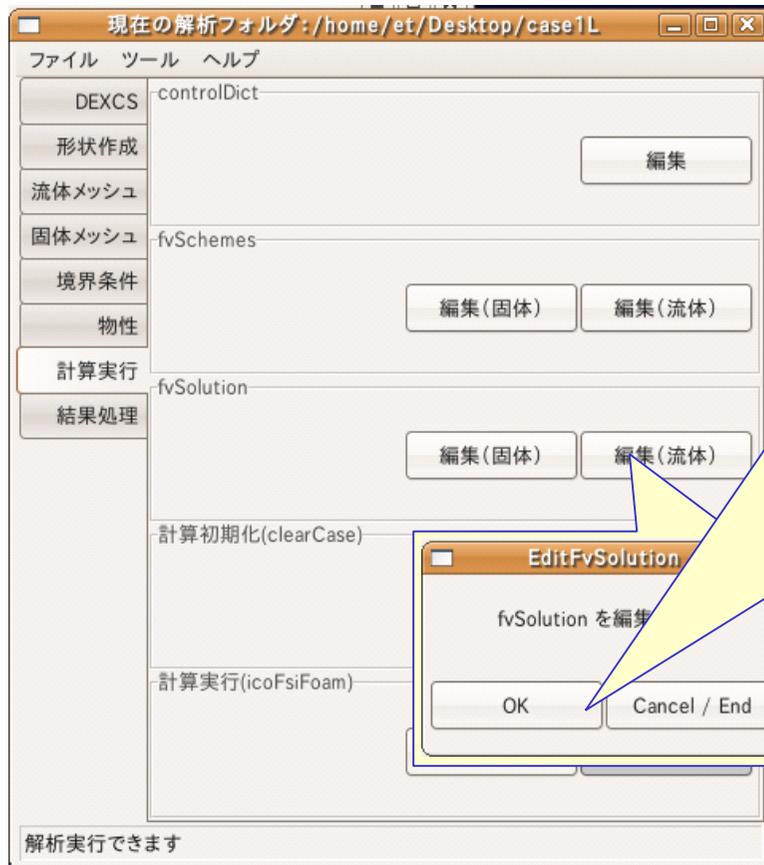
```
59 functions
60 (
61     probes1
62     {
63         type probes; // Type of functionObject
64         // Where to load it from (if not already in solver)
65         functionObjectLibs ("libsampling.so");
66
67         probeLocations // Locations to be probed. runTime modifiable!
68         (
69             (-0.01 0.5 0.0)
70             (0.15 0.5 0.0)
71         );
72         // Fields to be probed. runTime modifiable!
73         fields
74         (
75             p
76             U
77         );
78     }
79     forces
80     {
81         type forces;
82         functionObjectLibs ("libforces.so"); //Lib to load
83         patches (consoleFluid); // change to your patch name
84         rhoInf 1.225; //Reference density for fluid
85         CofR (0.15 0 0); //Origin for moment calculations
86     }
87 );
```

probe設置位置

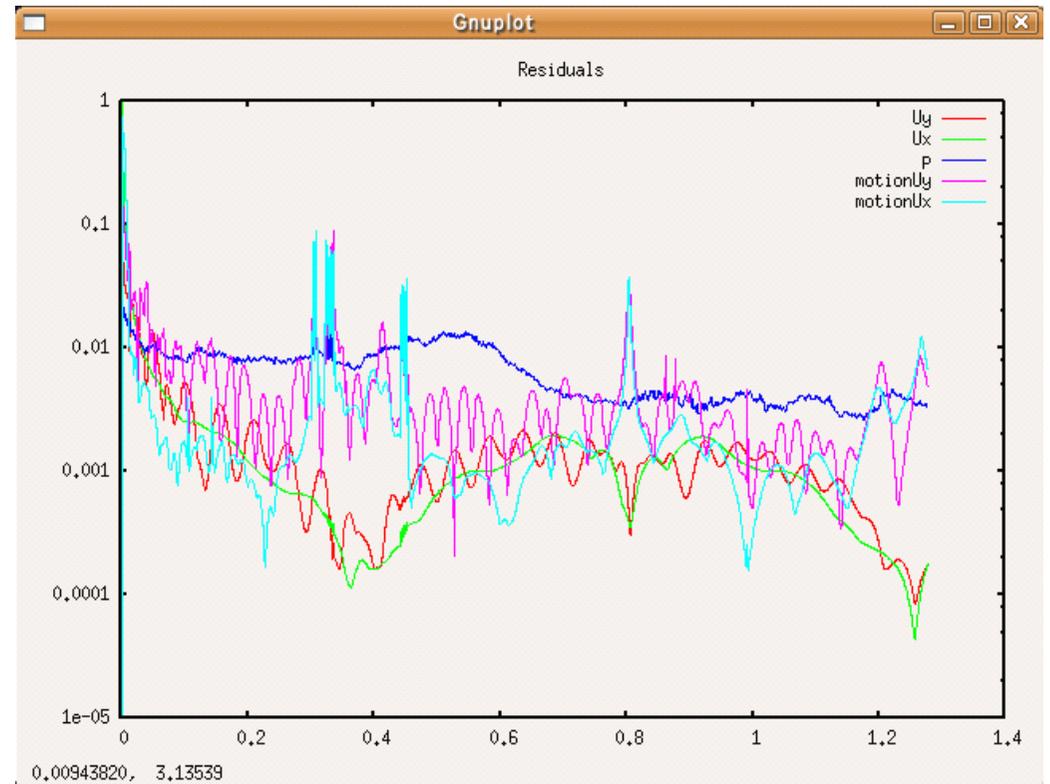
流体力を計算する
patch名を指定



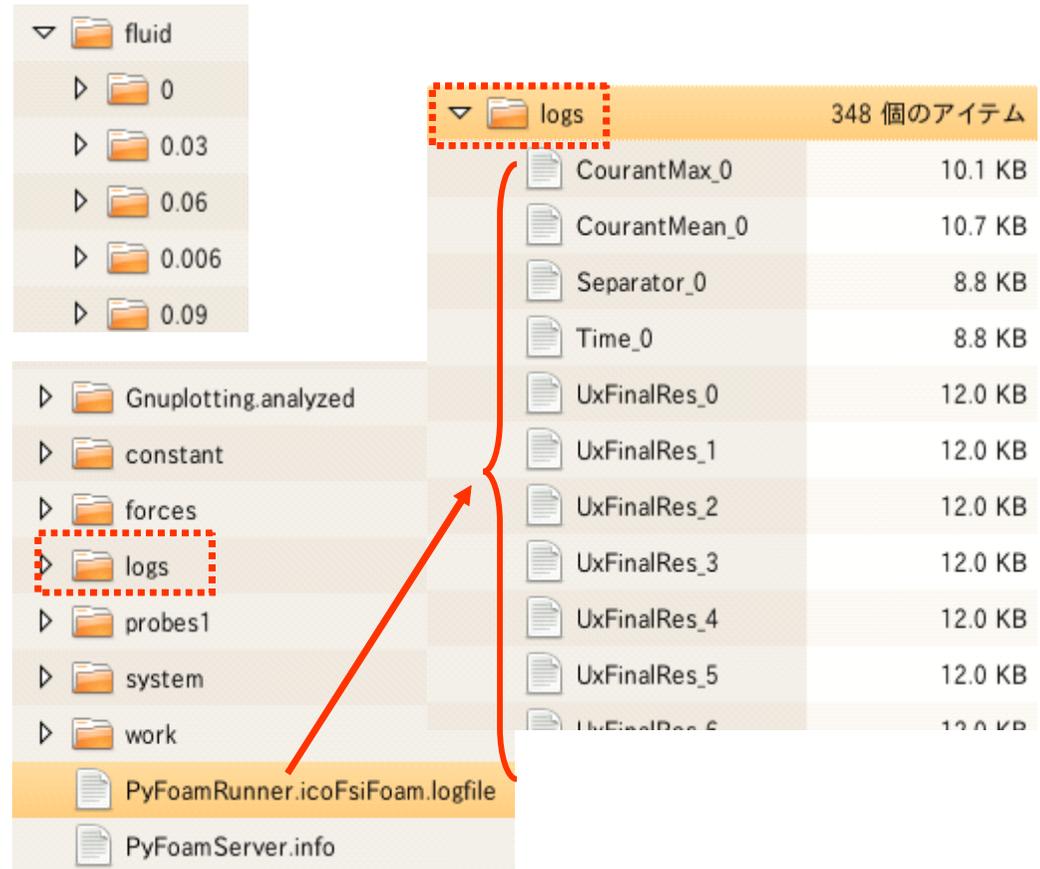
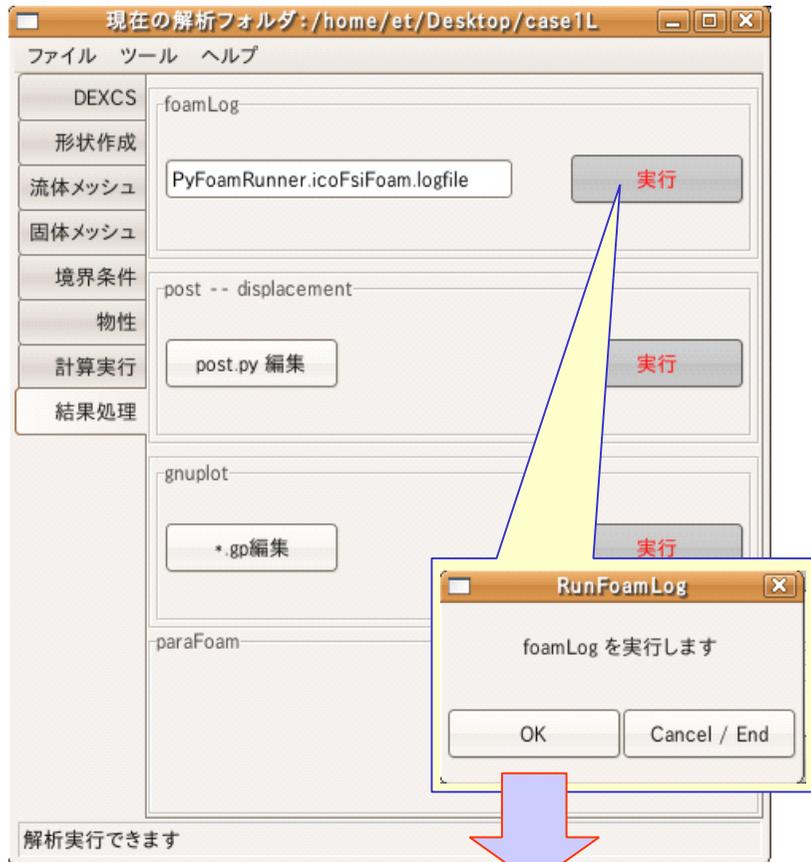
計算実行 (fvSolution)



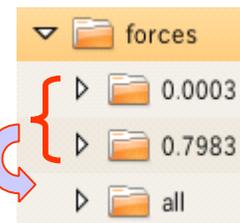
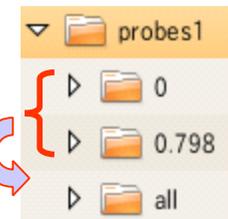
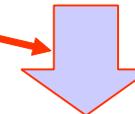
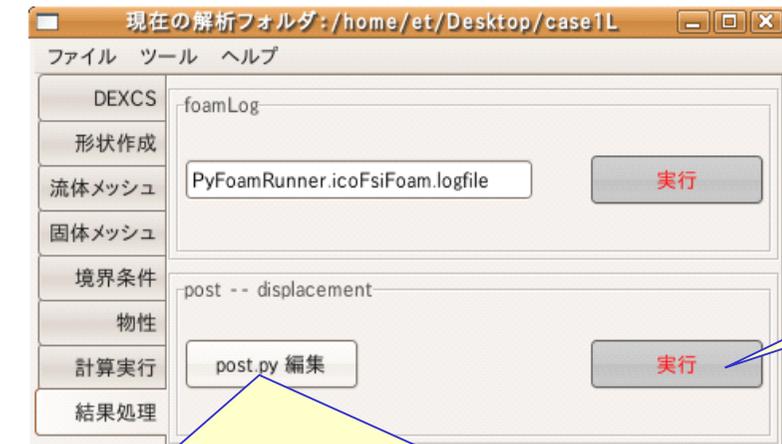
計算実行 (icoFsiFoam)



結果処理 (foamLog)



結果処理 (post -- displacement)



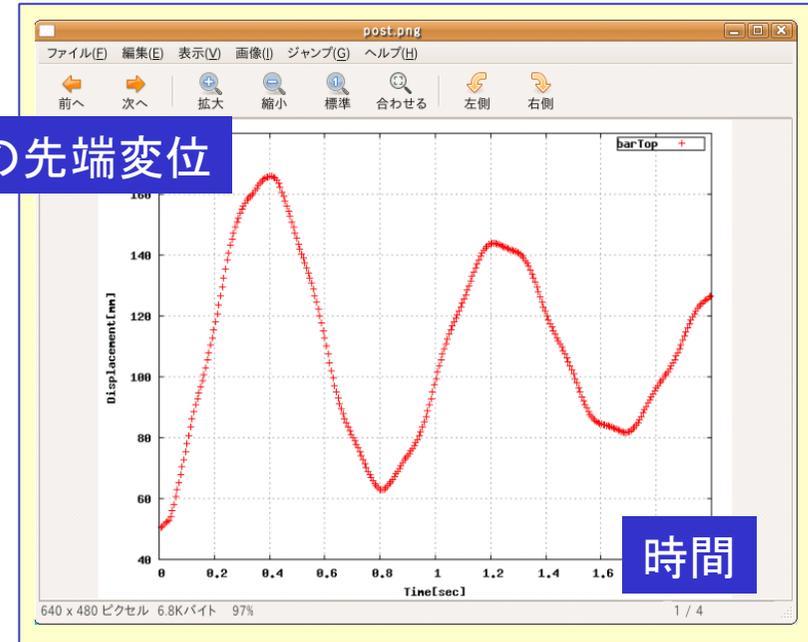
```
post.py
34
35 merge_probes( '../fluid/probes1', 'p', 'U' )
36 merge_probes( '../fluid/forces', 'forces.dat' )
37
38 g = open("test.x", 'w')
39 search_root = os.getcwd() + os.sep + "../fluid"
40 a = os.listdir(search_root)
41 a.sort()
42 npoints_line = 18
43 for f in a:
44     #print f
45     file = search_root + os.sep + f + "/solid/polyMesh/points.gz"
46     if (f != "constant" ) and (os.path.exists(file)):
47         print file
48         dat = gzip.open(file).read()
49         lines = dat.split('\n')
50         #print lines[25]
51         npoints = int(lines[npoints_line])
52         target =lines[npoints_line + npoints + 1]
53         target = string.replace(target,"(", "")
54         target = string.replace(target,")", "")
55         print npoints, target
56         g.write(f + ' ' + target + '\n' )
57 g.close
```

固体(梁)の
節点座標

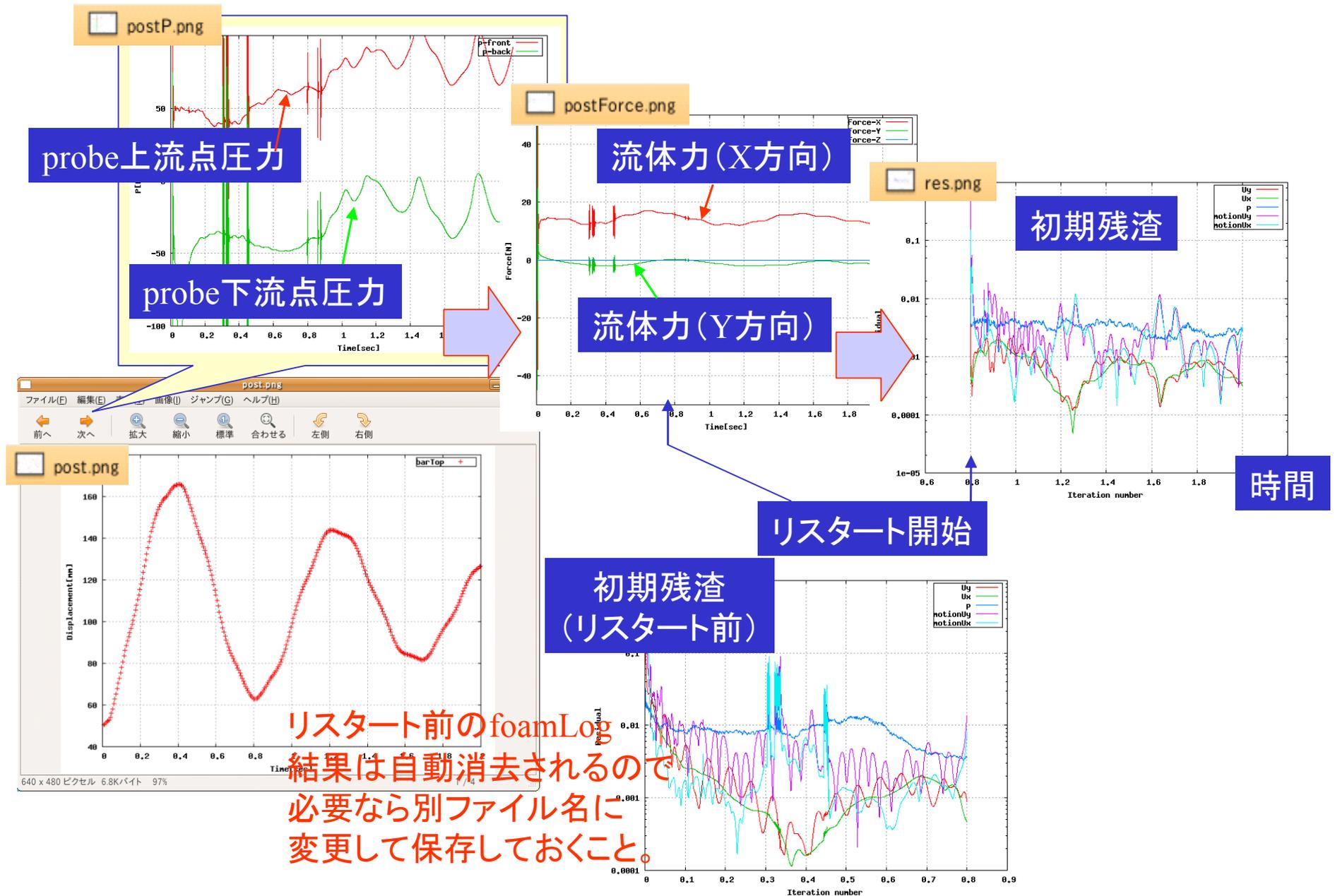
梁の先端位置



結果処理 (gnuplot)



結果処理 (gnuplot) 続き



結果処理(グラフ表示形式変更)

The screenshot displays a software interface for post-processing simulation results. The main window has a sidebar with various options, including '結果処理' (Result Processing). An 'EditGpFiles' dialog box is open, prompting the user to execute 'gedit res.gp probes.gp probeForce.gp probeP.gp'. Three script windows are shown, each containing Gnuplot commands for plotting different data series.

Script 1 (res.gp):

```
1 set terminal png
2 set output "res.png"
3 set logscale y 10
4 set xlabel "Iteration number"
5 set ylabel "Residual"
6 set grid
7 set key box
8 set style data line
9 plot "../fluid/logs/Uy_0" title "Uy",¥
10  "../fluid/logs/Ux_0" title "Ux",¥
11  "../fluid/logs/p_0" title "p",¥
12  "../fluid/logs/motionUy_0" title "motionUy",¥
13  "../fluid/logs/motionUx_0" title "motionUx",¥
14 # EOF
```

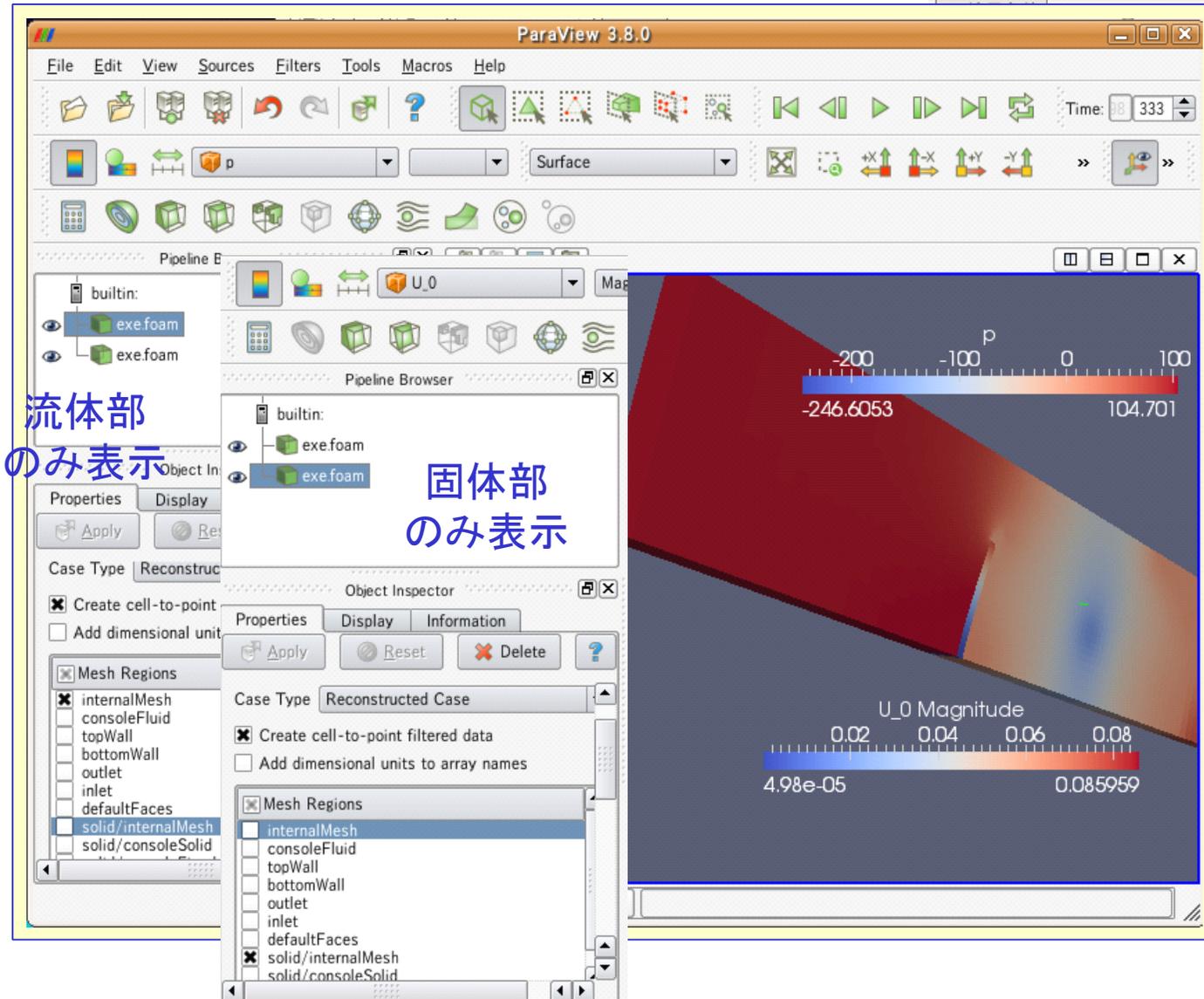
Script 2 (probeP.gp):

```
1 set terminal png
2 set output "postP.png"
3 set xlabel "Time[sec]"
4 set yrange [-100:100]
5 #set xrange [10:11]
6 set ylabel "P[Pa]"
7 set grid
8 set key box
9 set style data line
10 plot "../fluid/probes1/all/p" using 1:2 title "p-front",¥
11  "../fluid/probes1/all/p" using 1:3 title "p-back"
12 # EOF
13
```

Script 3 (probeForce.gp):

```
1 set terminal png
2 set output "postForce.png"
3 set xlabel "Time[sec]"
4 set yrange [-50:50]
5 #set xrange [10:11]
6 set ylabel "Force[N]"
7 set grid
8 set key box
9 set style data line
10 plot '<sed -e "s/(//g" -e "s)//g" ../fluid/forces/all/forces.dat' using 1:2 title "Force-X",¥
11  '<sed -e "s/(//g" -e "s)//g" ../fluid/forces/all/forces.dat' using 1:3 title "Force-Y",¥
12  '<sed -e "s/(//g" -e "s)//g" ../fluid/forces/all/forces.dat' using 1:4 title "Force-Z",¥
13 # EOF
14
```

結果 (paraFoam)



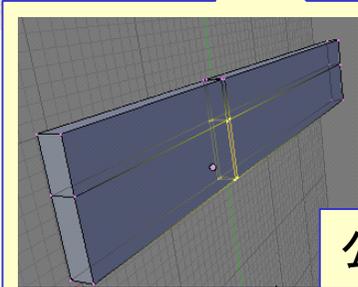
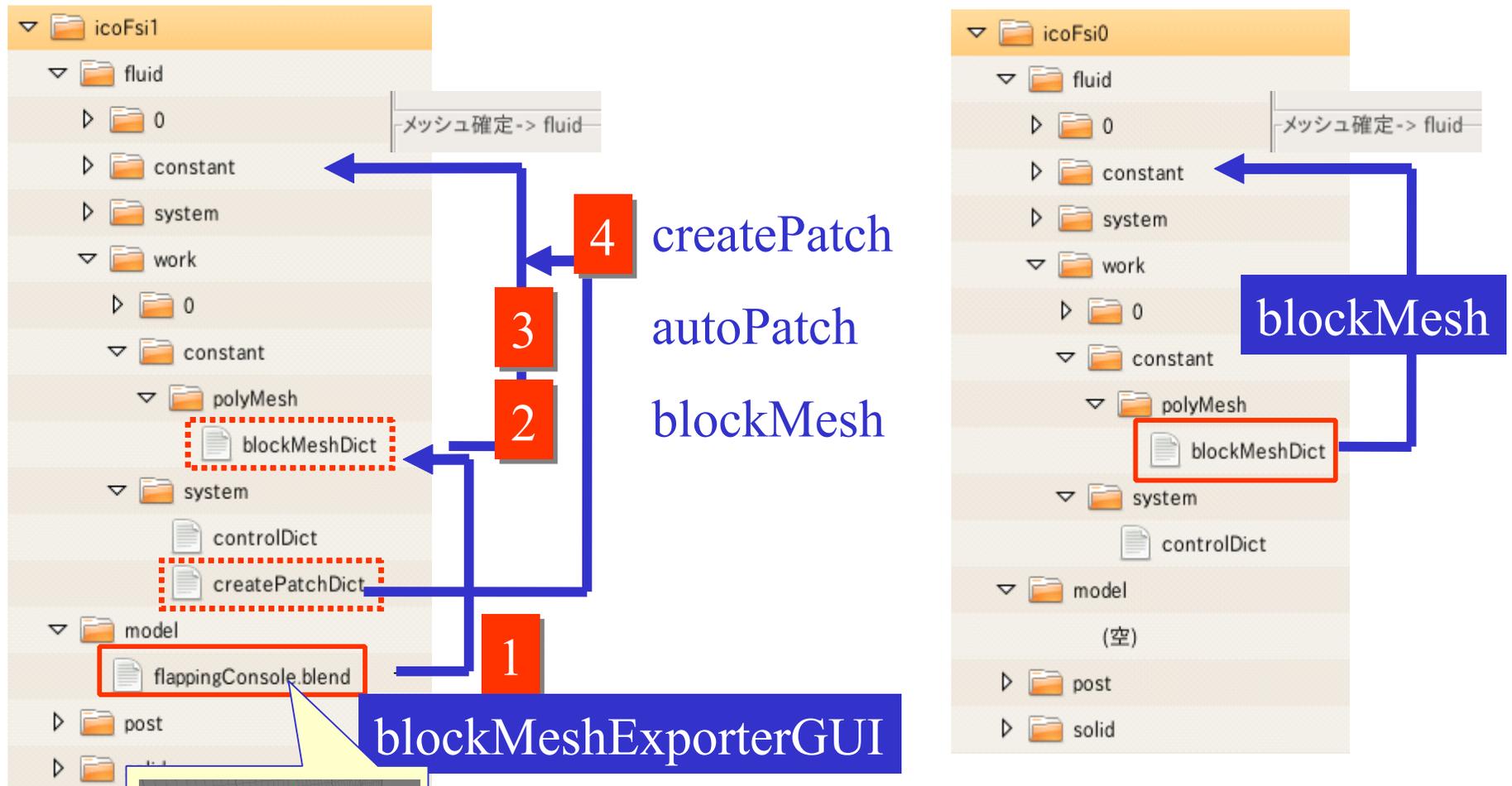
DEXCS_FSI ランチャーによる解析実行 (標準モデルの形状変更)

blender形状モデル



blockMeshExporter GUI

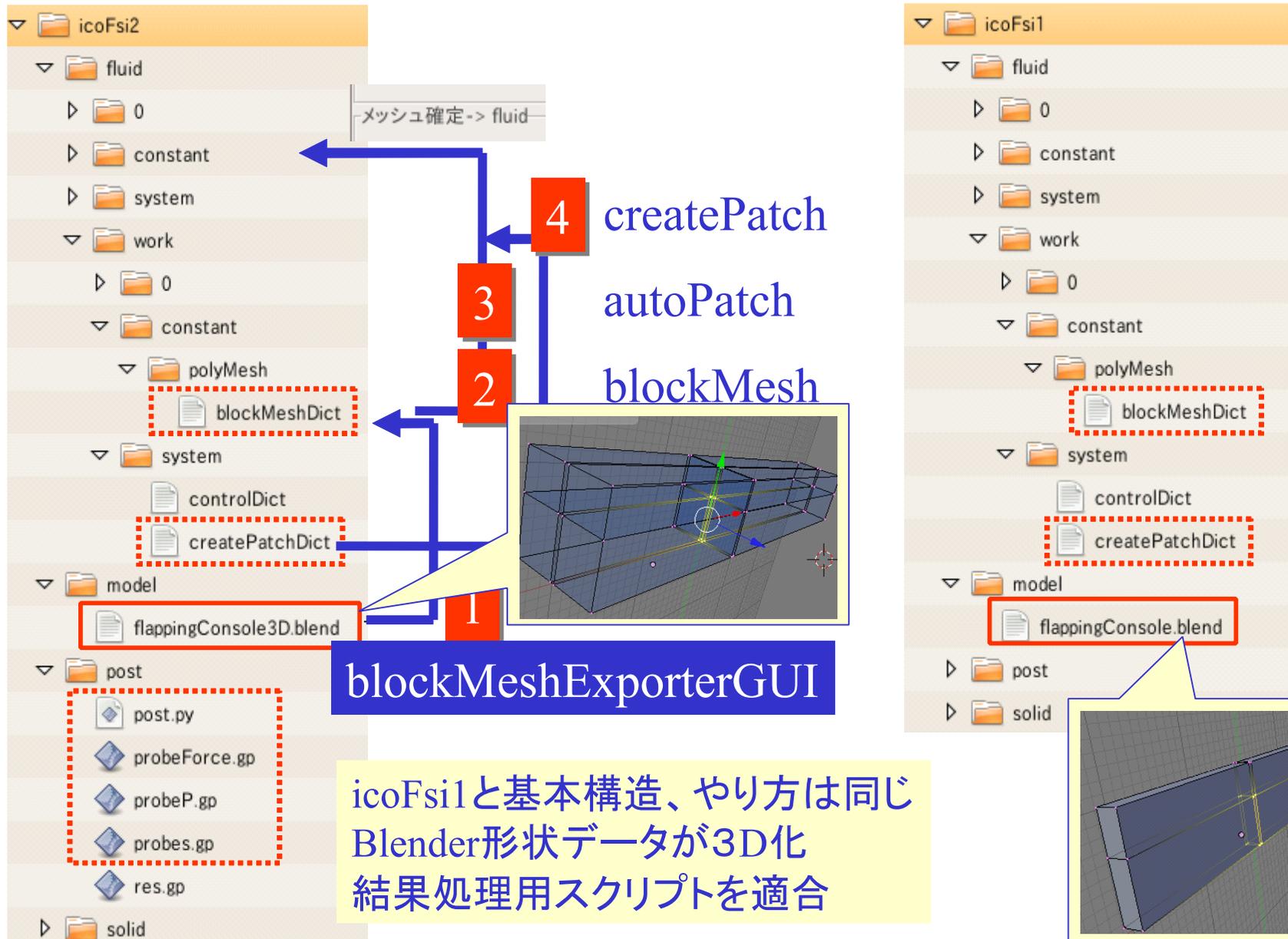
DEXCS template 2 (icoFsi1)



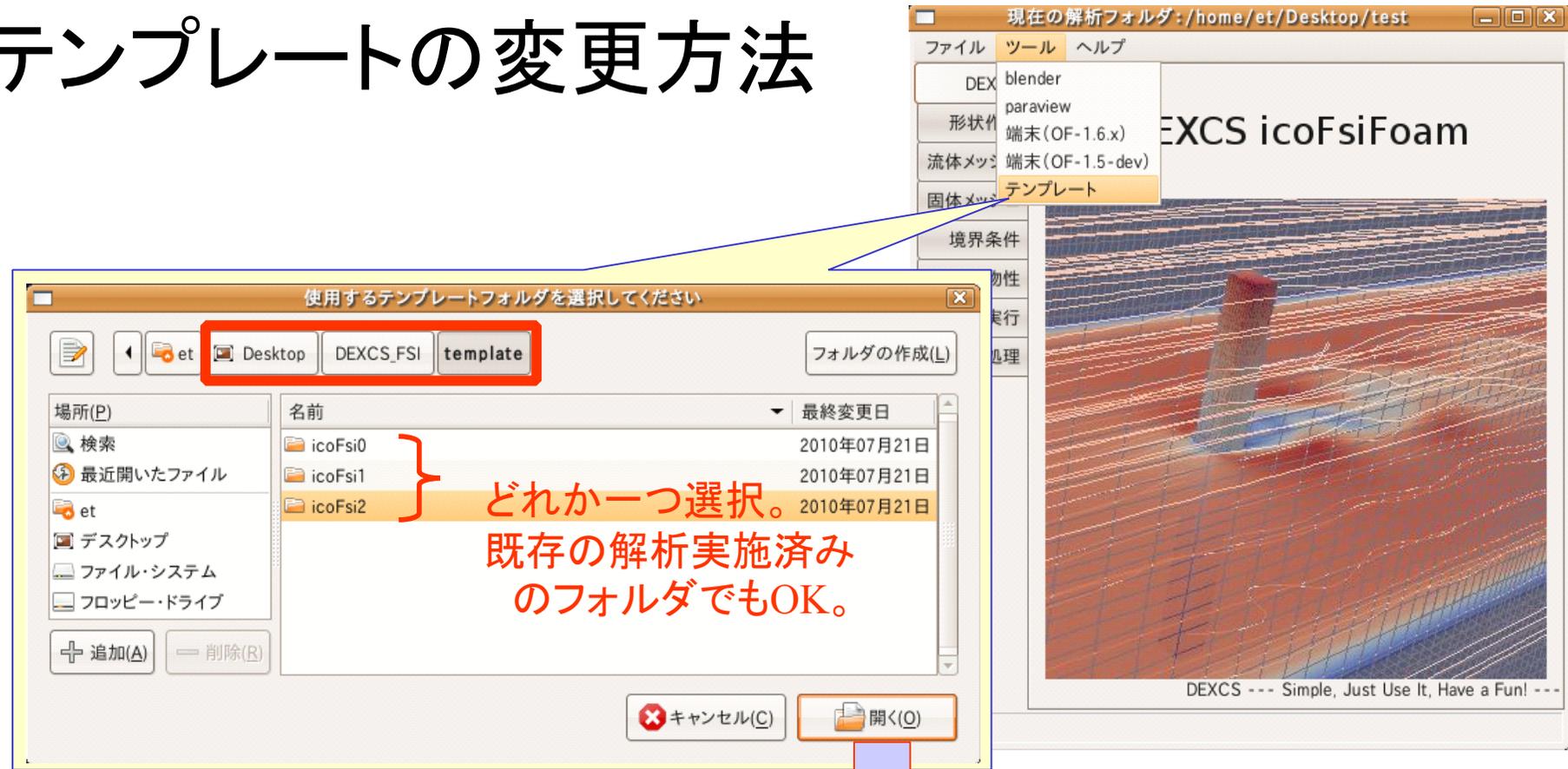
形状変更の際に、blockMeshDict、createPatchDictを都度、手修正変更にて使用できるようにしたもの

公開ケースと同等形状の blender モデル

DEXCS template 3 (icoFsi2)



テンプレートの変更方法



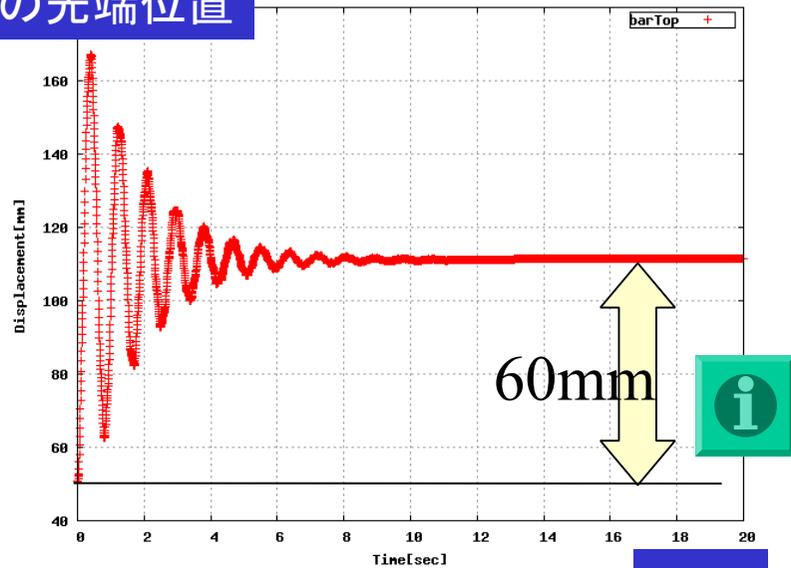
- この設定以降に作成される新規解析フォルダに適用される。
- 但し、ランチャーを終了すれば本設定変更はリセットされる。
- 作成済みの解析フォルダには影響しない。



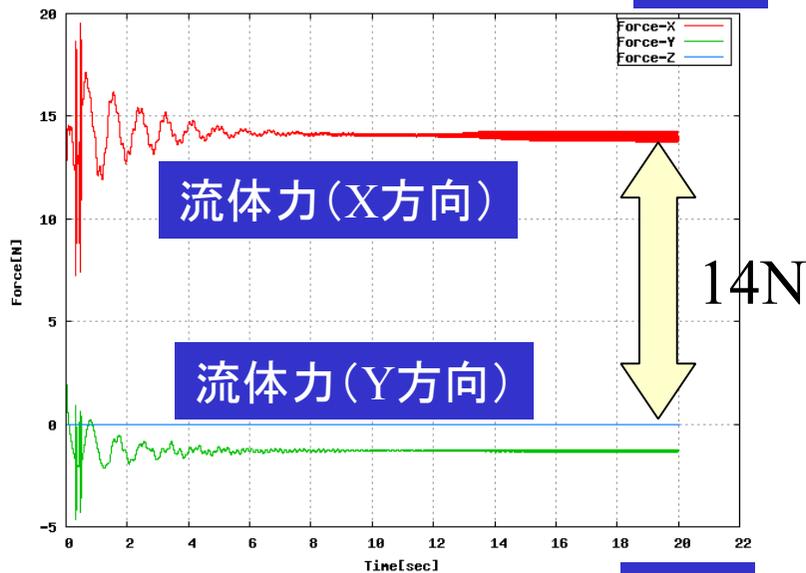
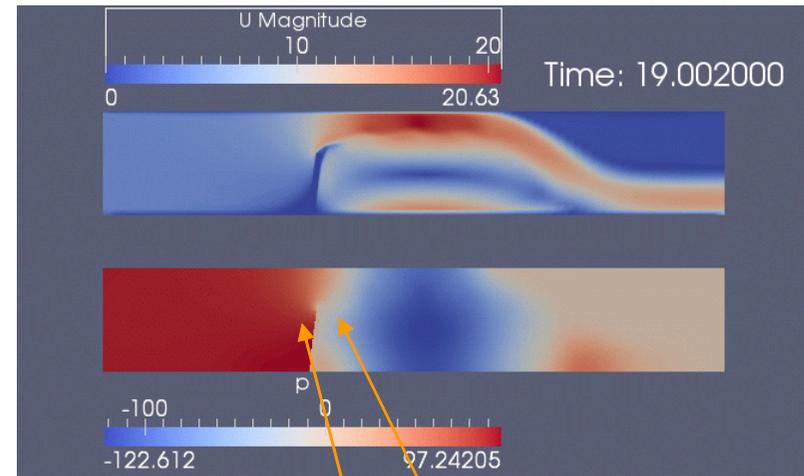
解析例の紹介

解析例1 (公開ケース)

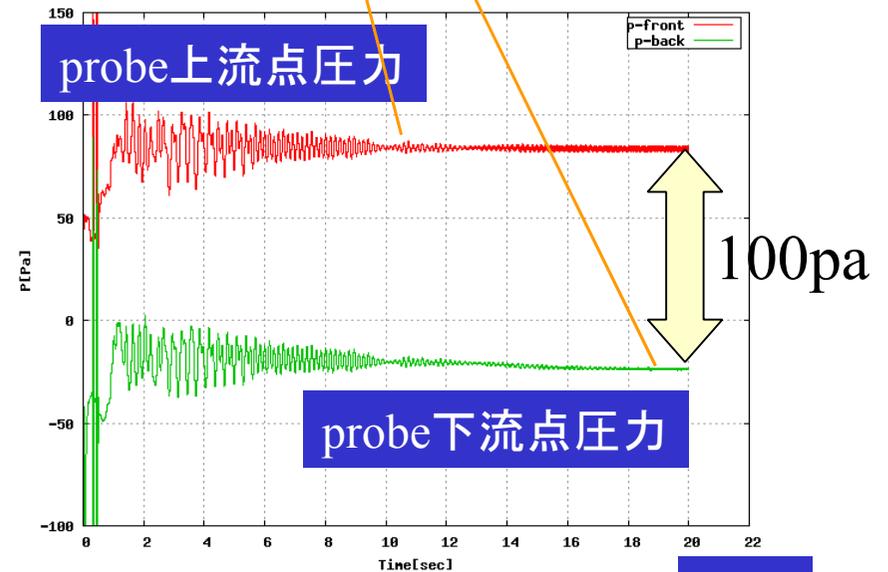
梁の先端位置



時間



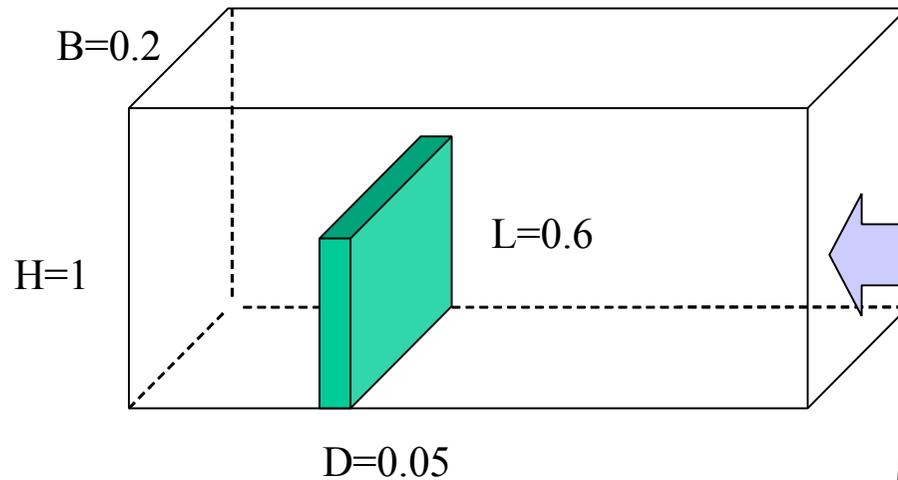
時間



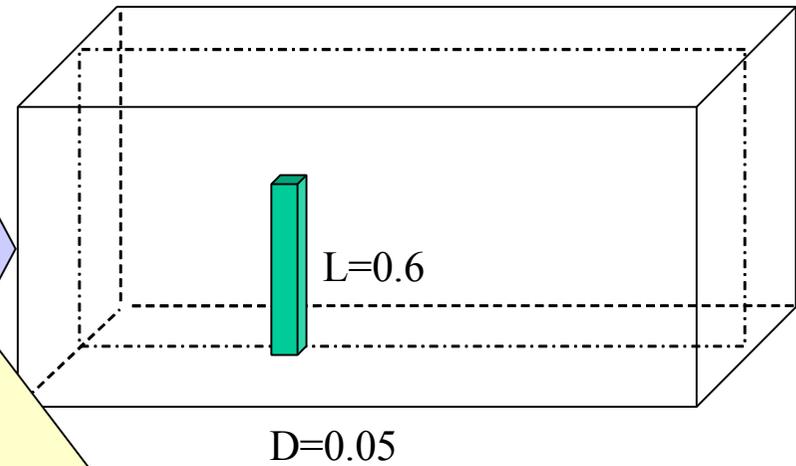
時間

考察1

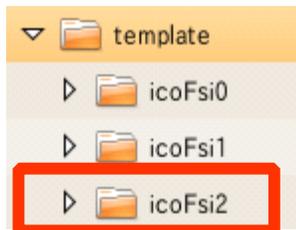
公開ケース(2D)



解析したい事象?(3D)



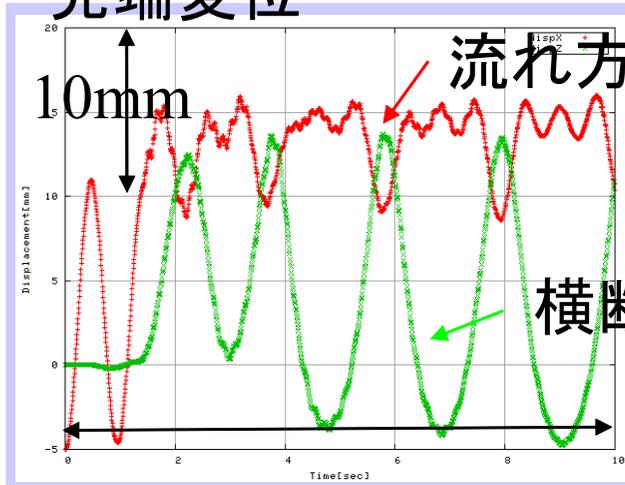
曲げの固有振動数は同一
しかし、流れ場が大きく異なる



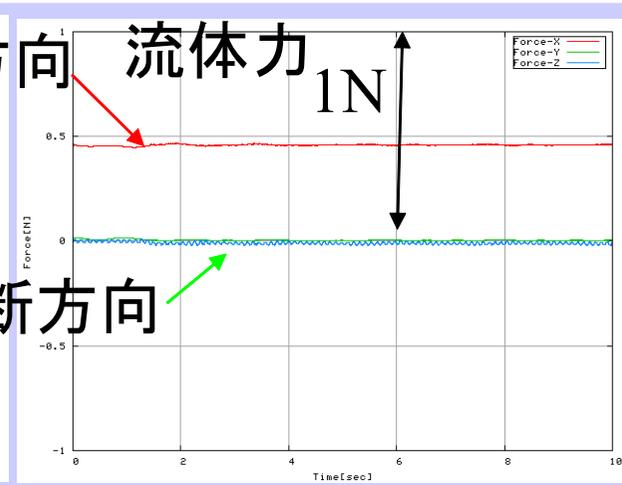
3Dで計算してみよう!

解析例2(3D)(参考)

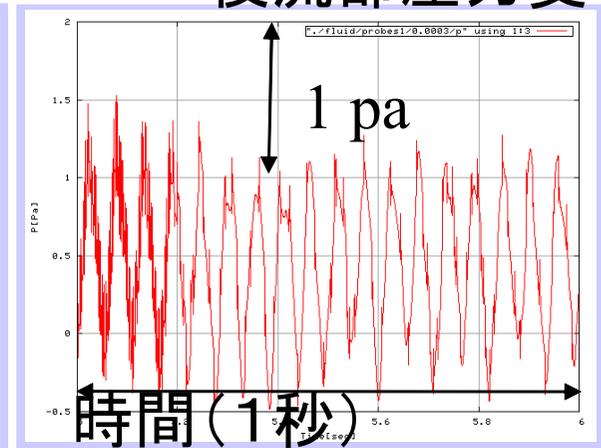
片持ち梁
先端変位



時間(10秒)

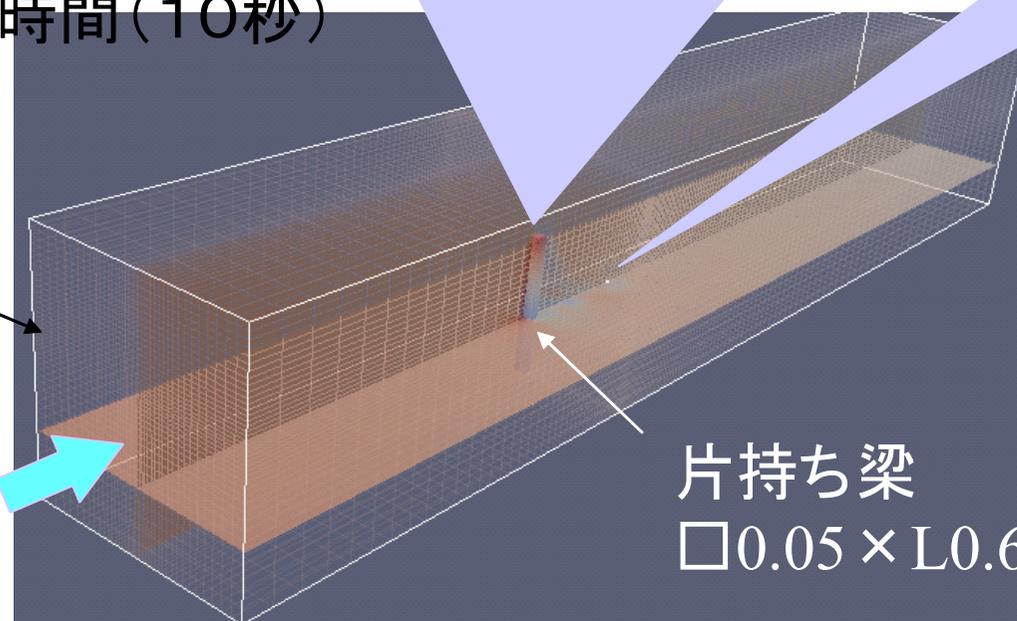


後流部圧力変化



ダクト
□1.0 × L6.0

U=4m/s



片持ち梁
□0.05 × L0.6

流体部メッシュ

Ncells=204,500
Npoints=216,652

固体部メッシュ

Ncells=4,500
Npoints=5,566

3D計算の補足

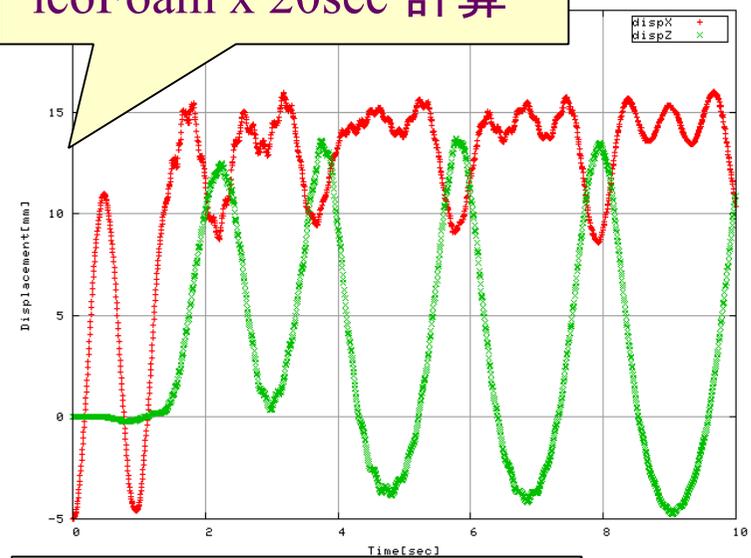
```
mechanicalProperties
16 instance "";
17 local "";
18
19 class dictionary;
20 object mechanicalProperties;
21 }
22
23 // *****
24
25 rho rho [1 -3 0 0 0 0] 1000;
26
27 nu nu [0 0 0 0 0 0] 0.3;
28
29 E E [1 -1 -2 0 0 0] 2e+6;
30
31 planeStress yes;
32
```

yes

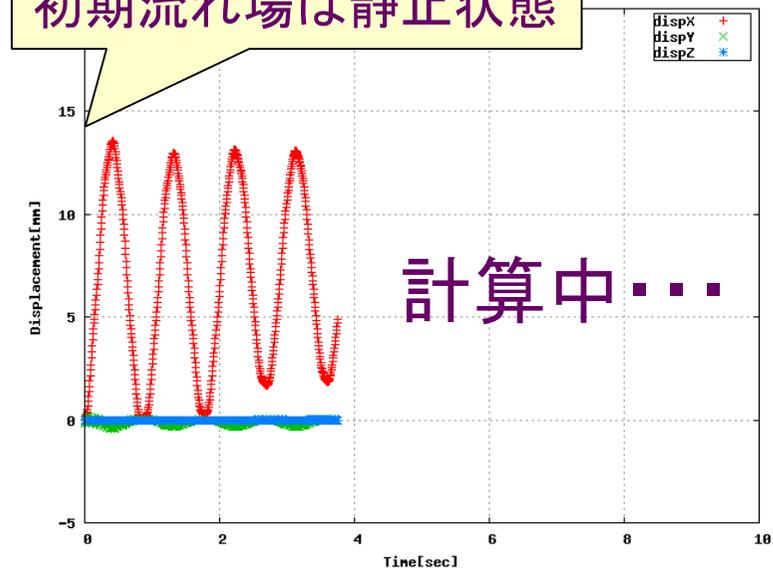
```
dynamicMeshDict
23 // *****
24
25 dynamicFvMesh dynamicMotionSolverFvMesh;
26
27 twoDMotion yes;
28
29 solver laplaceFaceDecomposition;
30
31 diffusivity quadratic;
32
33 frozenDiffusion on;
34
35 distancePatches
36 (
37 consoleFluid
38 );
39
```

no

初期流れ場は
icoFoam x 20sec 計算

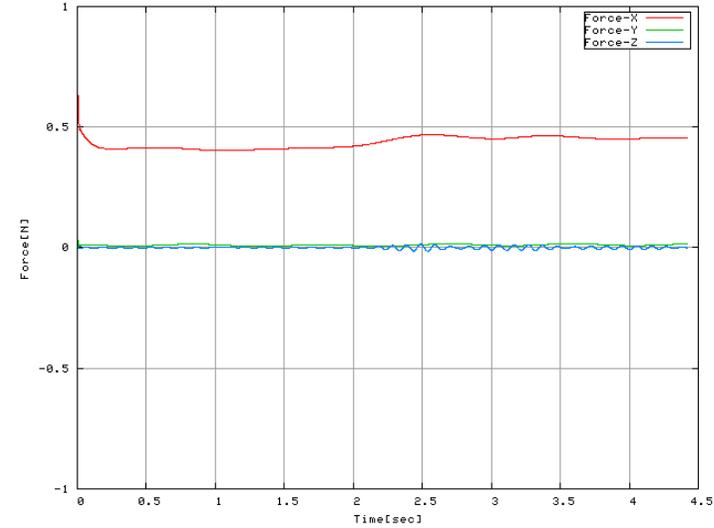
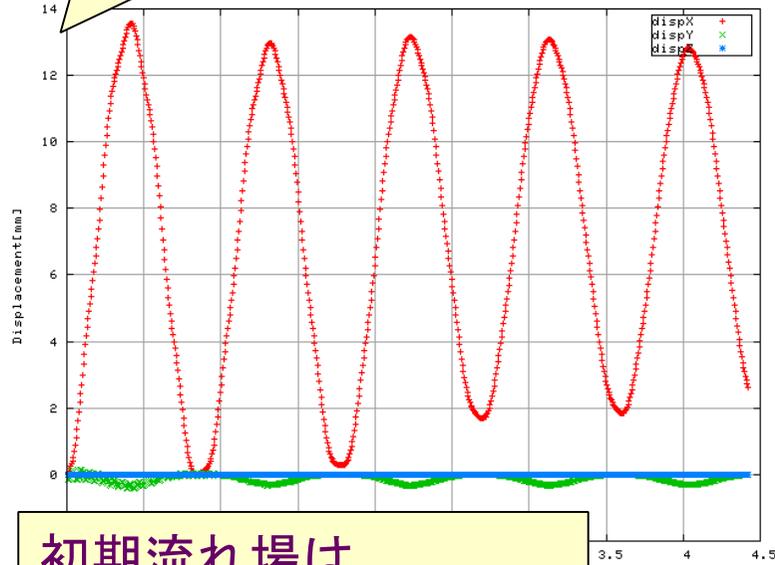


初期流れ場は静止状態

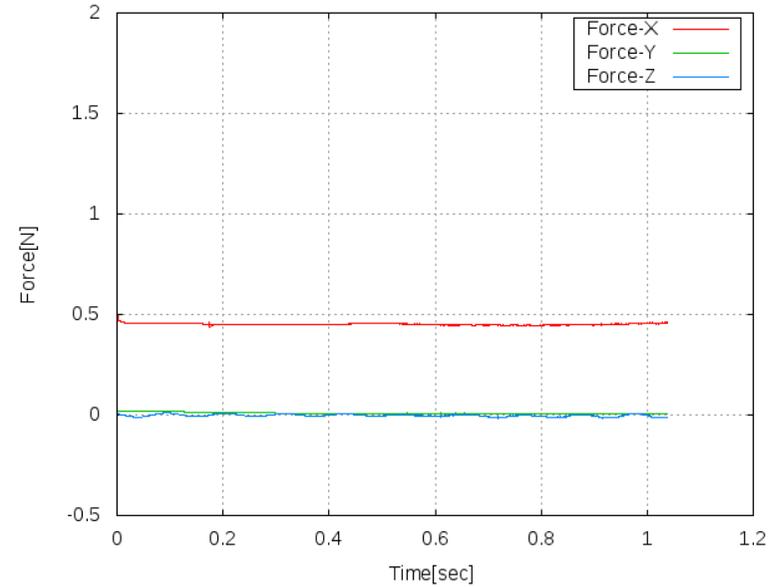
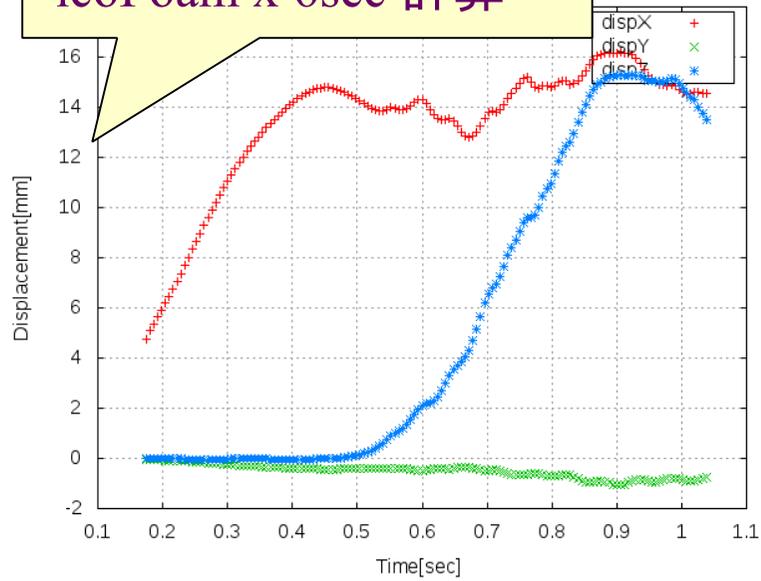


再計算の状況(3D)

初期流れ場は静止状態

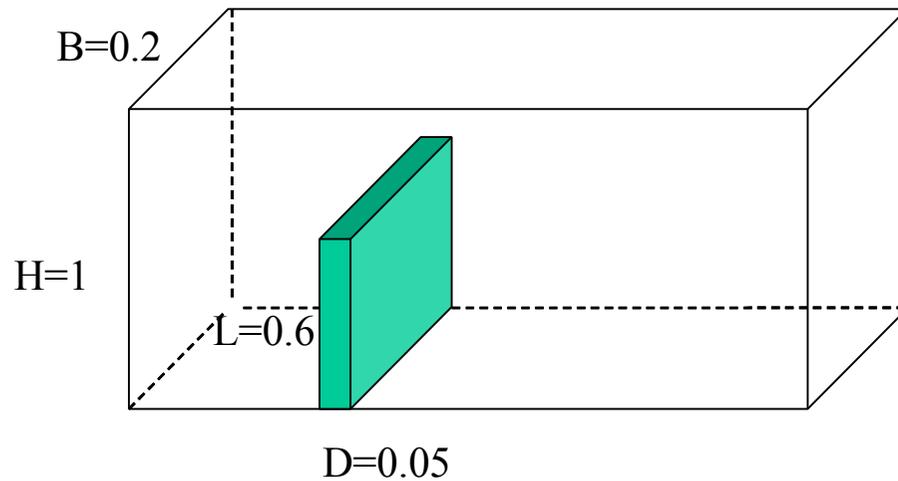


初期流れ場は
icoFoam x 6sec 計算

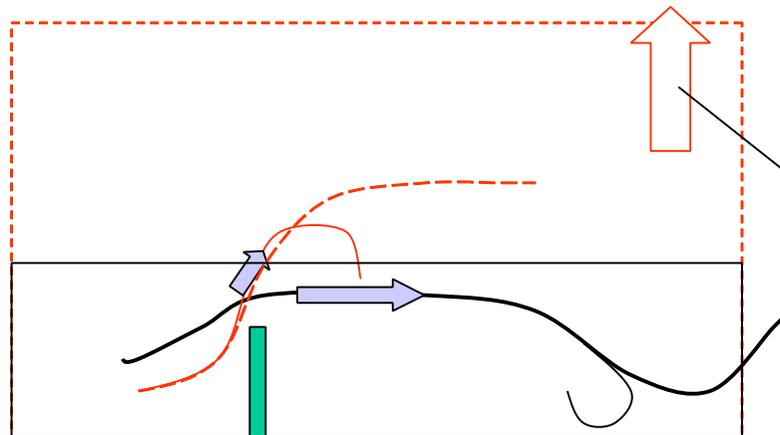
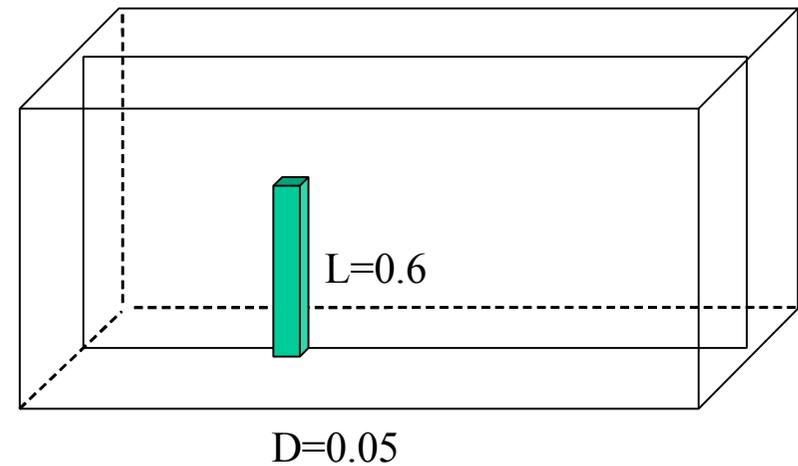


考察2 (2D計算で何とかできないか?)

公開ケース(2D)



解析したい事象?(3D)

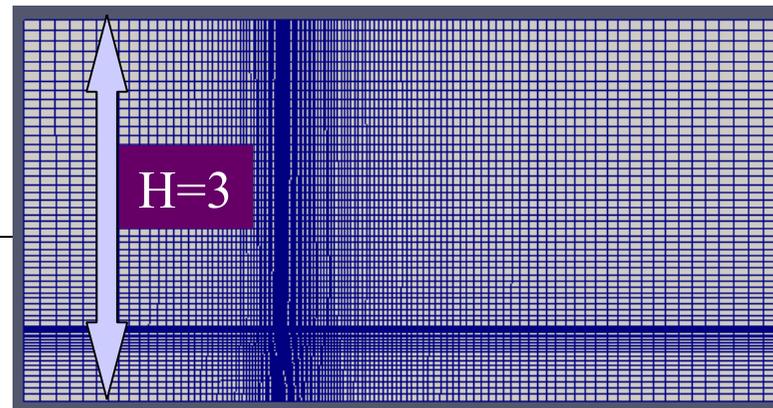


曲げの固有振動数は同一
しかし、流れ場が大きく異なる

解析領域の拡大はどうか?

解析例3 blockMesh

40分割



```

blockMeshDict
28 vertices
29 (
30 (-2 0 -0.1)
31 (0 0 -0.1)
32 (0.05 0 -0.1)
33 (4 0 -0.1)
34 (-2 0.6 -0.1)
35 (0 0.6 -0.1)
36 (0.05 0.6 -0.1)
37 (4 0.6 -0.1)
38 (-2 3 -0.1)
39 (0 3 -0.1)
40 (0.05 3 -0.1)
41 (4 3 -0.1)
42
43 (-2 0 0.1)
44 (0 0 0.1)
45 (0.05 0 0.1)
46 (4 0 0.1)
47 (-2 0.6 0.1)
48 (0 0.6 0.1)
49 (0.05 0.6 0.1)
50 (4 0.6 0.1)
51 (-2 3 0.1)
52 (0 3 0.1)
53 (0.05 3 0.1)
54 (4 3 0.1)
55 );
    
```

```

57 blocks
58 (
59 hex (0 1 5 4 12 13 17 16) (40 20 1) simpleGrading (0.1 0.2 1)
60 hex (2 3 7 6 14 15 19 18) (80 20 1) simpleGrading (10 0.2 1)
61 hex (4 5 9 8 16 17 21 20) (40 40) simpleGrading (0.1 2 1)
62 hex (5 6 10 9 17 18 22 21) (5 40) simpleGrading (1 2 1)
63 hex (6 7 11 10 18 19 23 22) (80 40) simpleGrading (10 2 1)
64 );
    
```

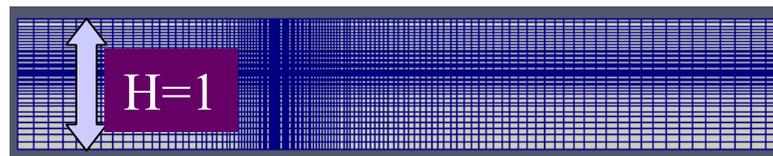
部を変更

```

blockMeshDict
28 vertices
29 (
30 (-2 0 -0.1)
31 (0 0 -0.1)
32 (0.05 0 -0.1)
33 (4 0 -0.1)
34 (-2 0.6 -0.1)
35 (0 0.6 -0.1)
36 (0.05 0.6 -0.1)
37 (4 0.6 -0.1)
38 (-2 1 -0.1)
39 (0 1 -0.1)
40 (0.05 1 -0.1)
41 (4 1 -0.1)
42
43 (-2 0 0.1)
44 (0 0 0.1)
45 (0.05 0 0.1)
46 (4 0 0.1)
47 (-2 0.6 0.1)
48 (0 0.6 0.1)
49 (0.05 0.6 0.1)
50 (4 0.6 0.1)
    
```

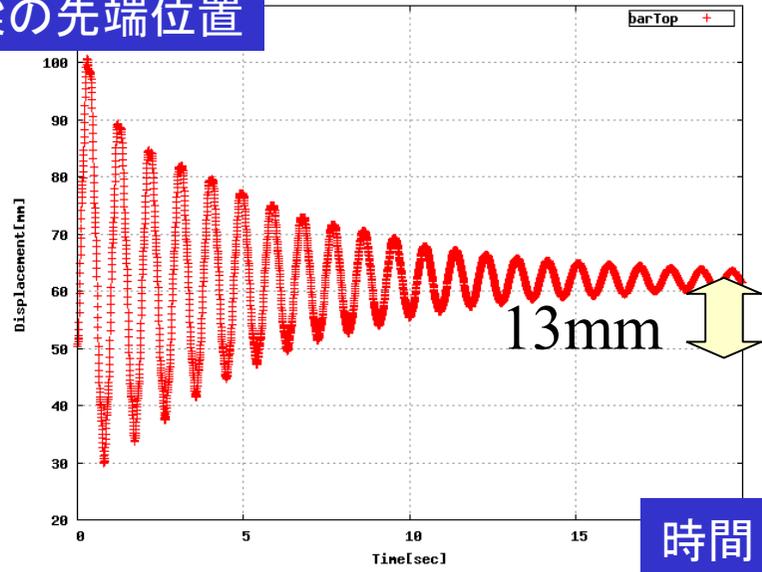
(解析例1)

20分割

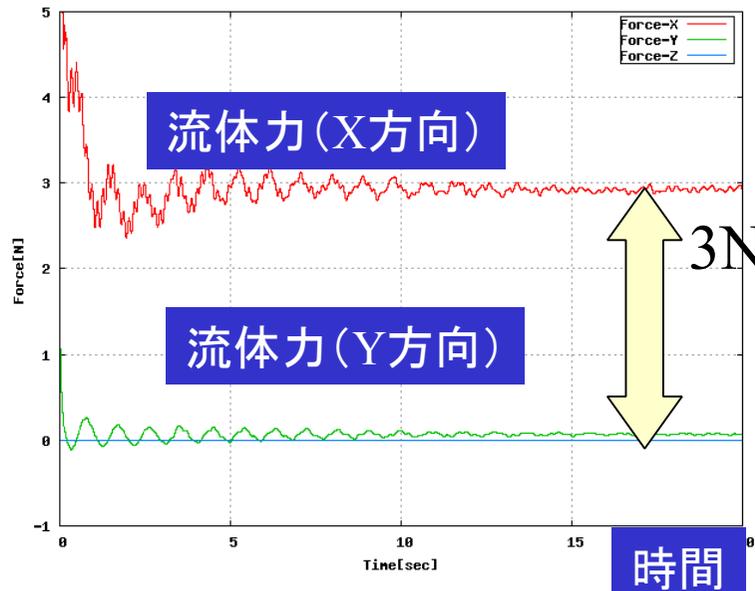


解析例3

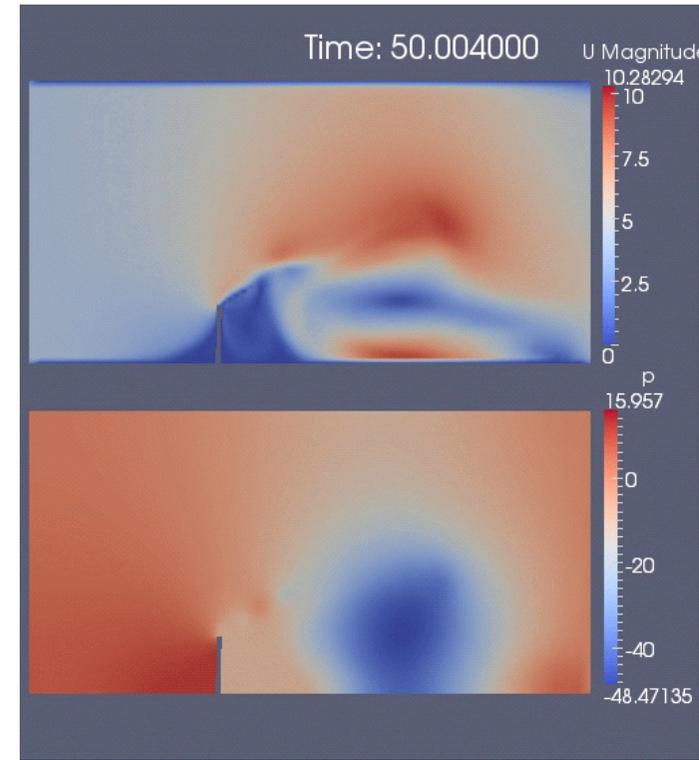
梁の先端位置



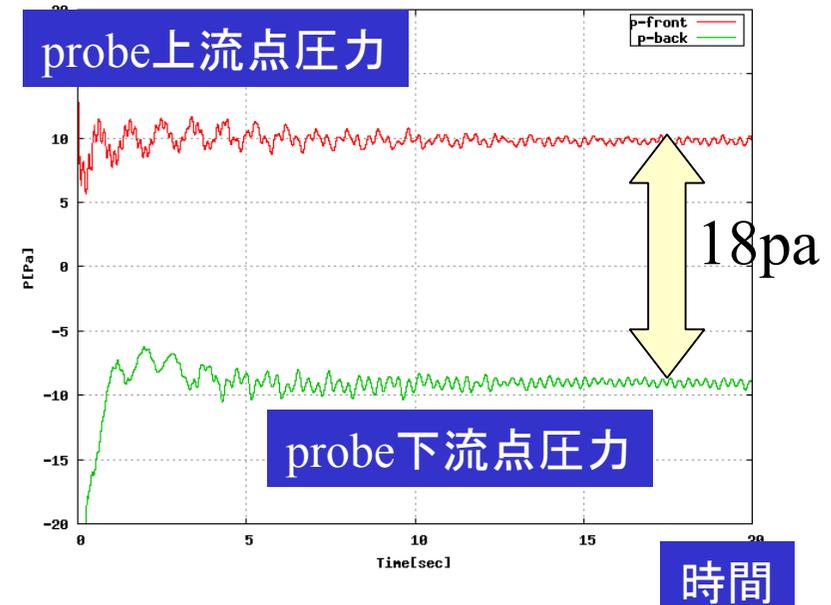
時間



時間



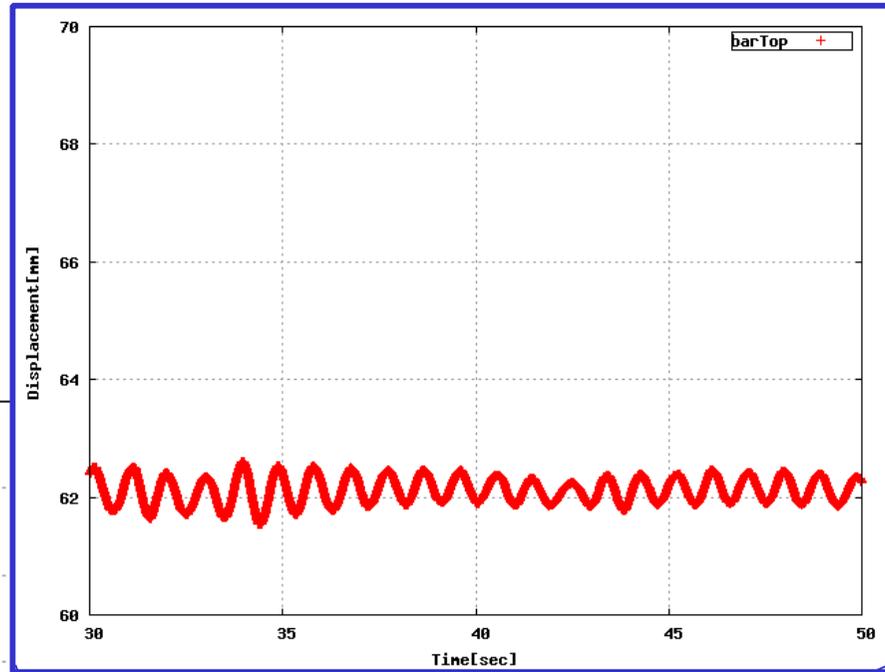
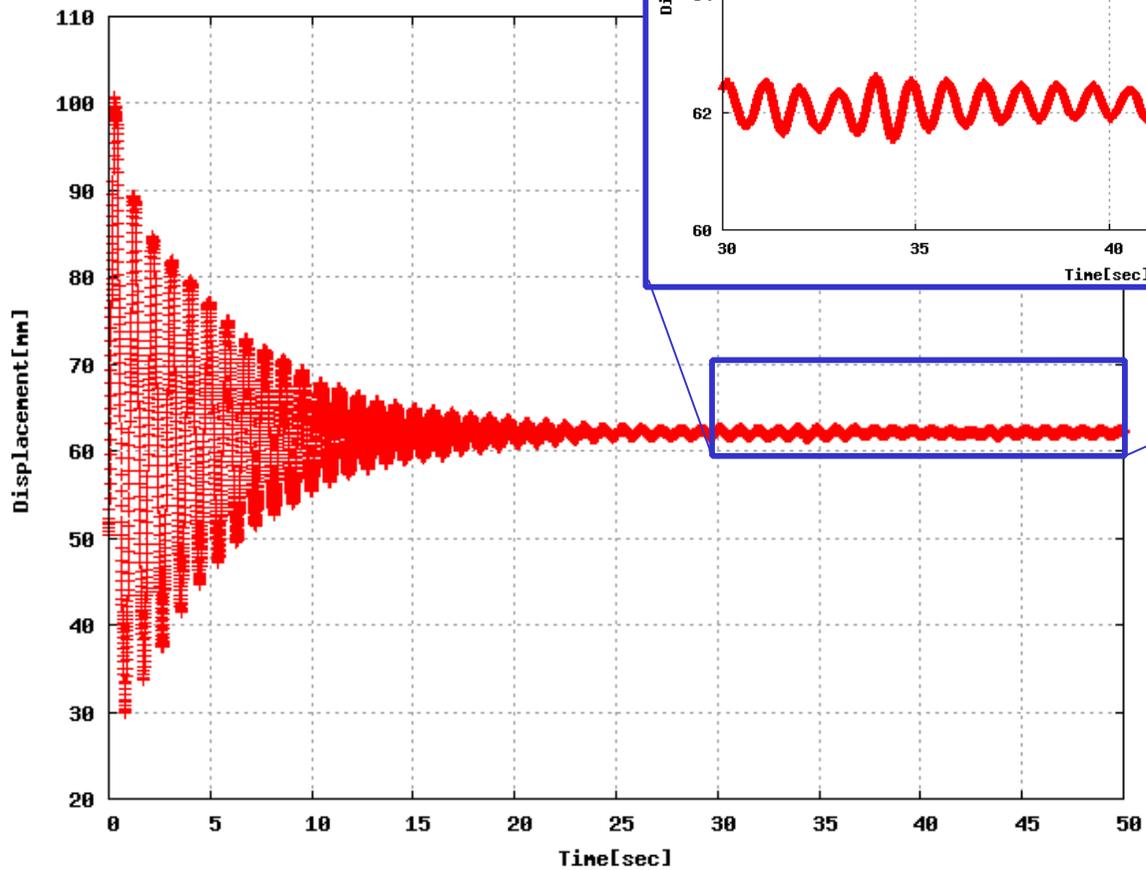
probe上流点圧力



時間

解析例3(続き)

梁の先端位置



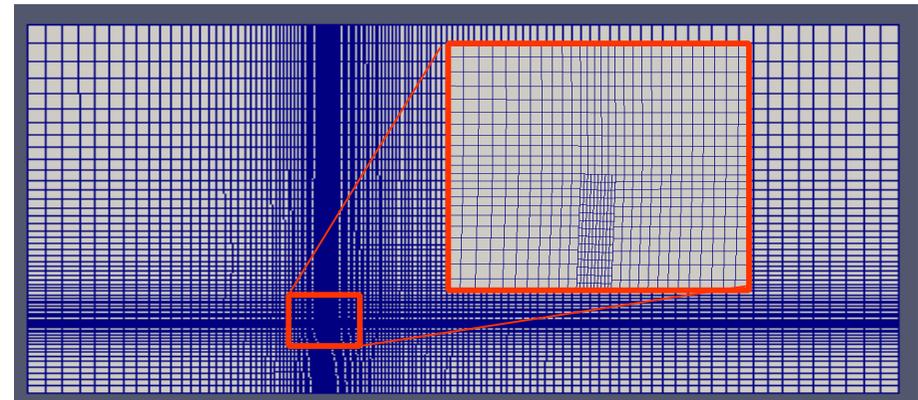
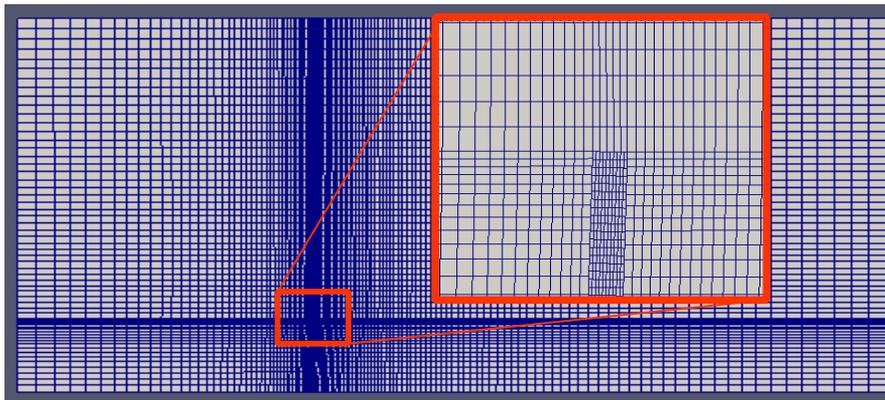
時間

解析例3

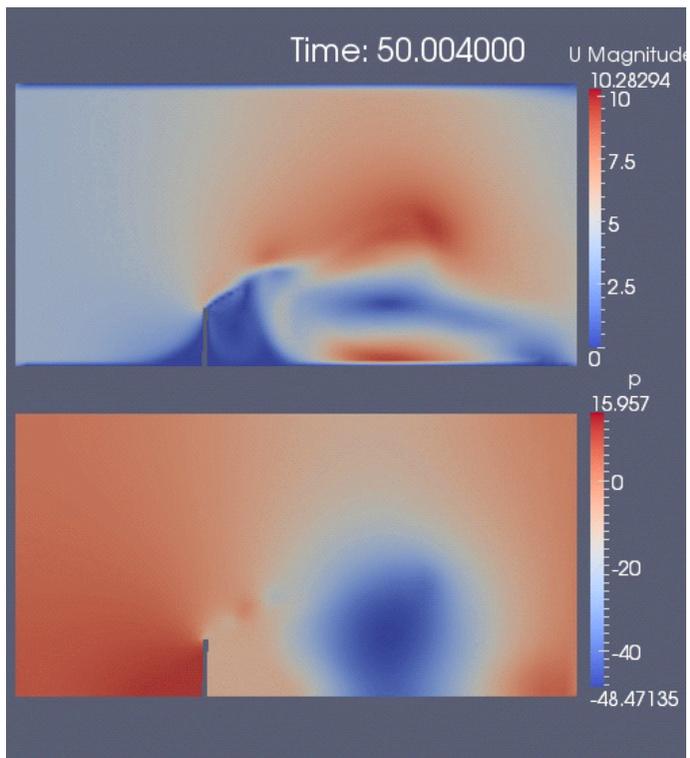
```
57 blocks
58 (
59   hex (0 1 5 4 12 13 17 16) (40 20 1) simpleGrading (0.1 0.2 1)
60   hex (2 3 7 6 14 15 19 18) (80 20 1) simpleGrading (10 0.2 1)
61   hex (4 5 9 8 16 17 21 20) (40 20 1) simpleGrading (0.1 2 1)
62   hex (5 6 10 9 17 18 22 21) (5 20 1) simpleGrading (1 2 1)
63   hex (6 7 11 10 18 19 23 22) (80 20 1) simpleGrading (10 2 1)
64 );
```

解析例3改

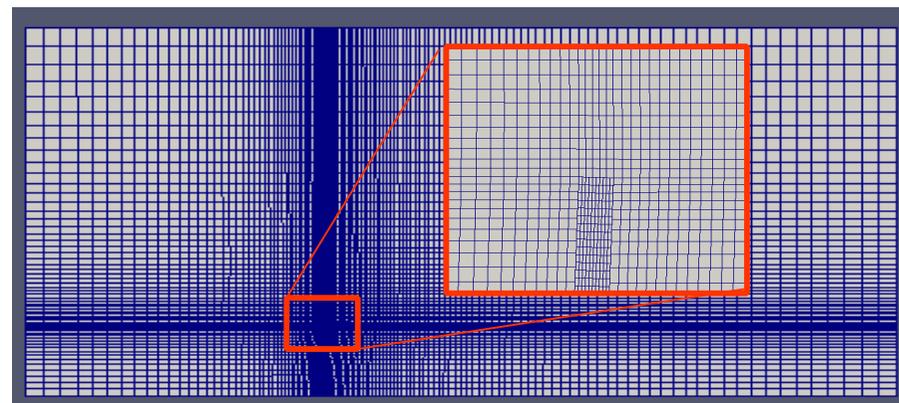
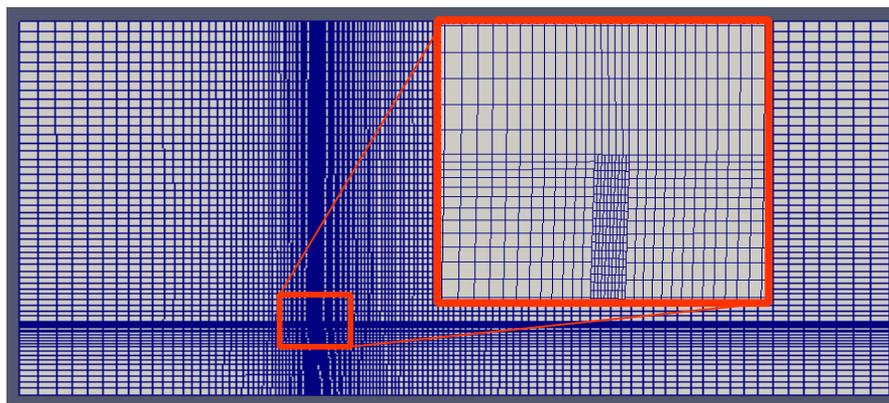
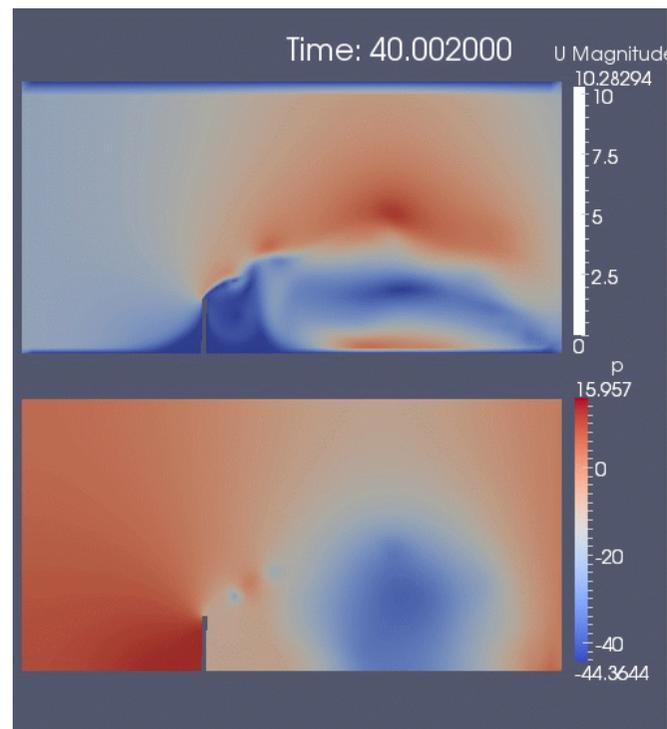
```
ts
hex (0 1 5 4 12 13 17 16) (40 20 1) simpleGrading (0.1 0.2 1)
hex (2 3 7 6 14 15 19 18) (80 20 1) simpleGrading (10 0.2 1)
hex (4 5 9 8 16 17 21 20) (40 40 1) simpleGrading (0.1 10 1)
hex (5 6 10 9 17 18 22 21) (5 40 1) simpleGrading (1 10 1)
hex (6 7 11 10 18 19 23 22) (80 40 1) simpleGrading (10 10 1)
```



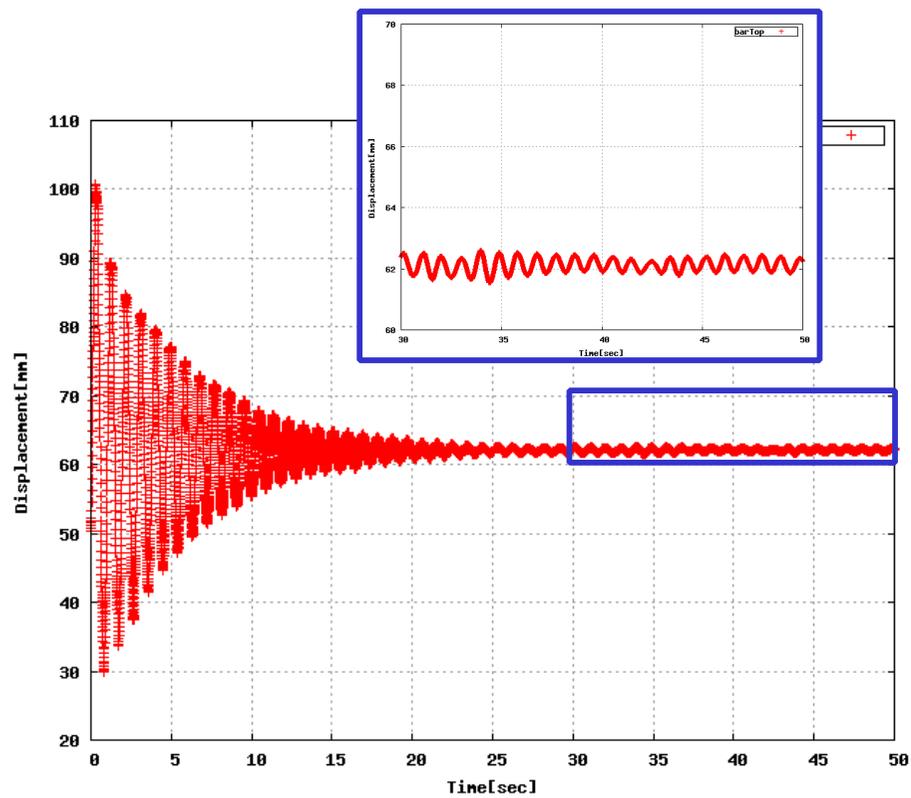
解析例3



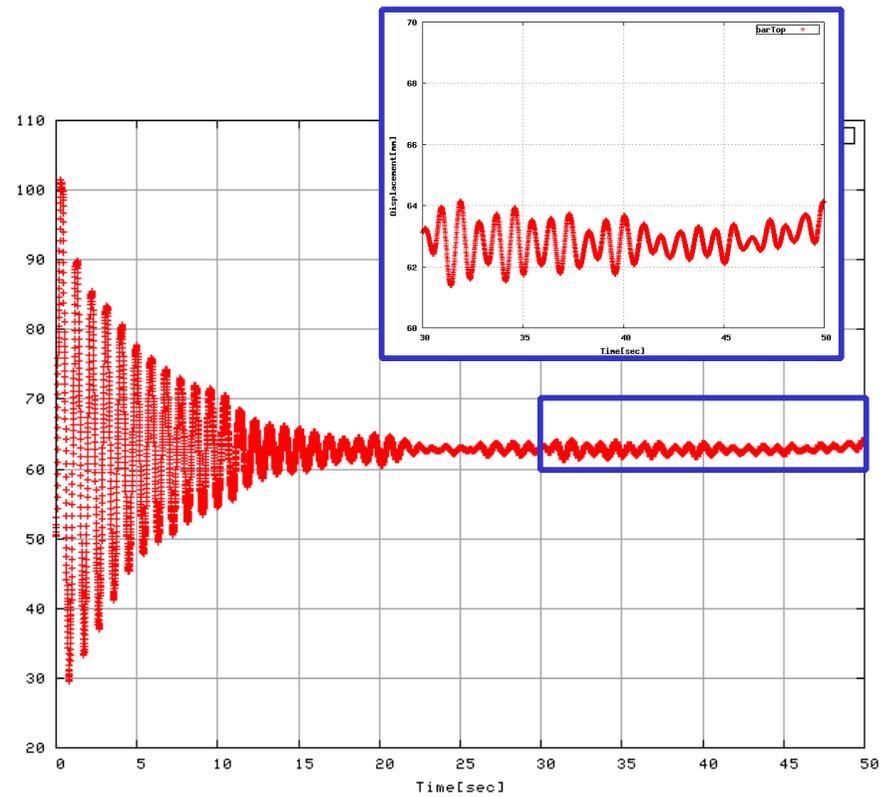
解析例3改



解析例3



解析例3改



まとめ

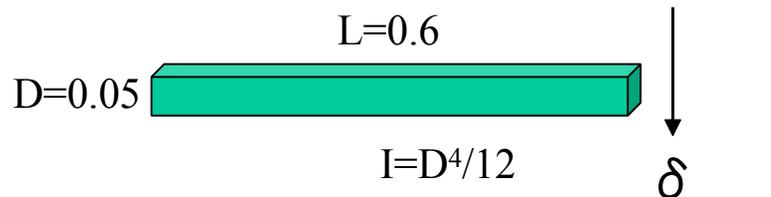
1. OpenFOAM-1.5-dev のicoFsiFoam を使って、流体構造連成解析を実施した
2. 一般公開情報をそのまま使った解析では問題があり、さらなる工夫が必要であった
3. これまでの実施例では、概ね合理的な計算結果が得られているが、十分な検証が出来ているとは言い難い
4. 非定常計算には長大な計算時間がかかるが、icoFsiFoamは並列計算に対応できておらず、実用面では問題になる
5. 今回取り上げなかった icoStructFoam (OF-1.6/1.7で動作OK) もソルバーの改変や使い方の工夫で適用可能性はありそう

參考資料

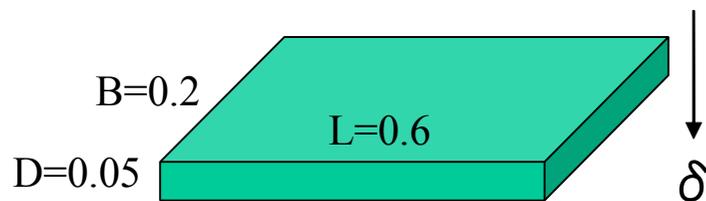
片持ちはりの変形

<http://bit.ly/aJ8aX4>

<http://kozo.milkcafe.to/rikigaku2/henkei.html>



$$\begin{aligned} \delta &= WL^4 / 8EI \\ &= \frac{0.6^4}{8 \times 2000000 \times 0.05^4 / 12} \times W \\ &= 0.0155 \times W \end{aligned}$$



$$\begin{aligned} \delta &= WL^4 / 8EI \\ &= \frac{0.6^4}{8 \times 2000000 \times 0.2 \times 0.05^3 / 12} \times W \\ &= 0.0039 \times W \end{aligned}$$

梁	最大たわみ角θ	最大たわみδ
	$\frac{PL^2}{16EI}$	$\frac{PL^3}{48EI}$
	$\frac{WL^3}{24EI}$	$\frac{5WL^4}{384EI}$
	$-\frac{PL^2}{2EI}$	$\frac{PL^3}{3EI}$
	$-\frac{WL^3}{6EI}$	$\frac{WL^4}{8EI}$

<http://bit.ly/aOYWG2>

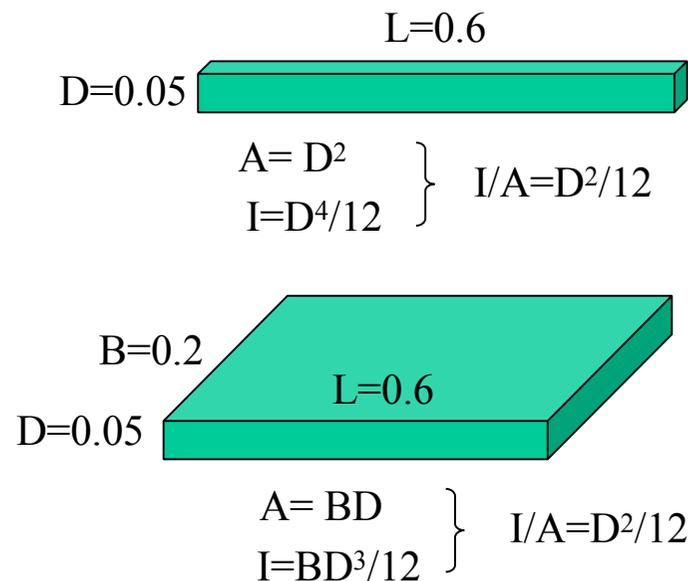
<http://kozo.milkcafe.to/rikigaku2/seinou.html>

断面形状	断面2次モーメント
	$I_x = \frac{bD^3}{12}$



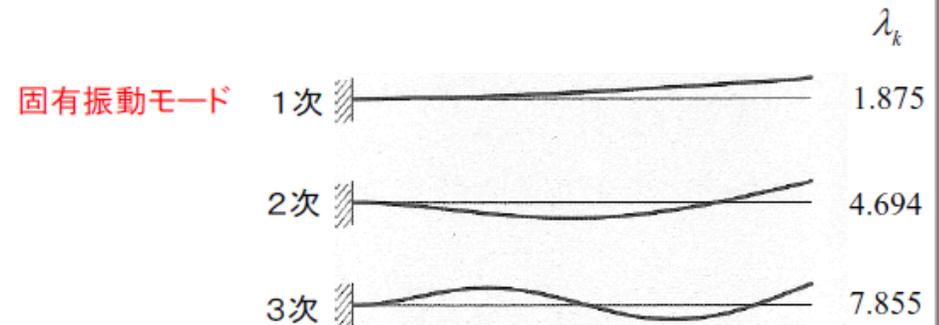
片持ちはりの曲げ振動

http://www.mech.usp.ac.jp/~hnw/model/kogi/2006/kiriki2_12.pdf



片持ちはりの曲げ振動

固有振動数 $\omega_k = \left(\frac{\lambda_k}{L}\right)^2 \sqrt{\frac{EI}{\rho A}}$



$$\omega = \left(\frac{\lambda}{L}\right)^2 \sqrt{\frac{EI}{\rho A}} = \left(\frac{\lambda}{L}\right)^2 \sqrt{\frac{ED^2}{12\rho}}$$
$$= \left(\frac{1.875}{0.6}\right)^2 \sqrt{\frac{2000000 \cdot 0.05^2}{12 \cdot 1000}} = 6.67 \text{ rad/sec}$$

$E=2000000$

$\rho=1000$



カルマン渦の放出周波数

この渦の放出周波数 f_s は U と D によって次式により無次元化され、ストローハル数 St と呼ぶ。

$$St = \frac{f_s D}{U} \quad (1)$$

St 数は一般に Re 数の関数として実験的に求められる。図2に実験値を示す。

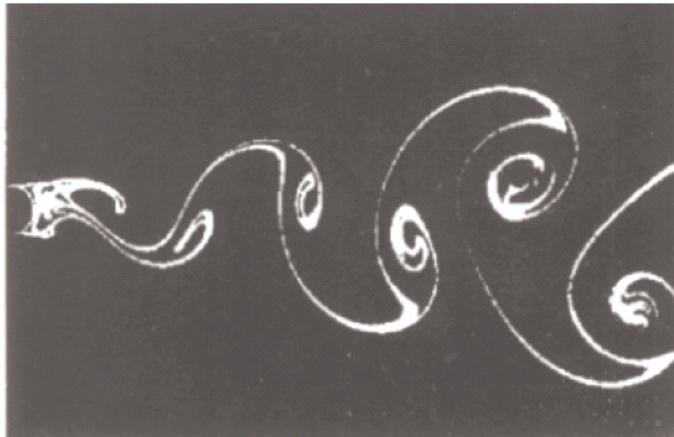


図1 カルマン渦⁽⁴⁾

(4) 種子田定俊：「画像から学ぶ流体力学」，朝倉書店（1988）。

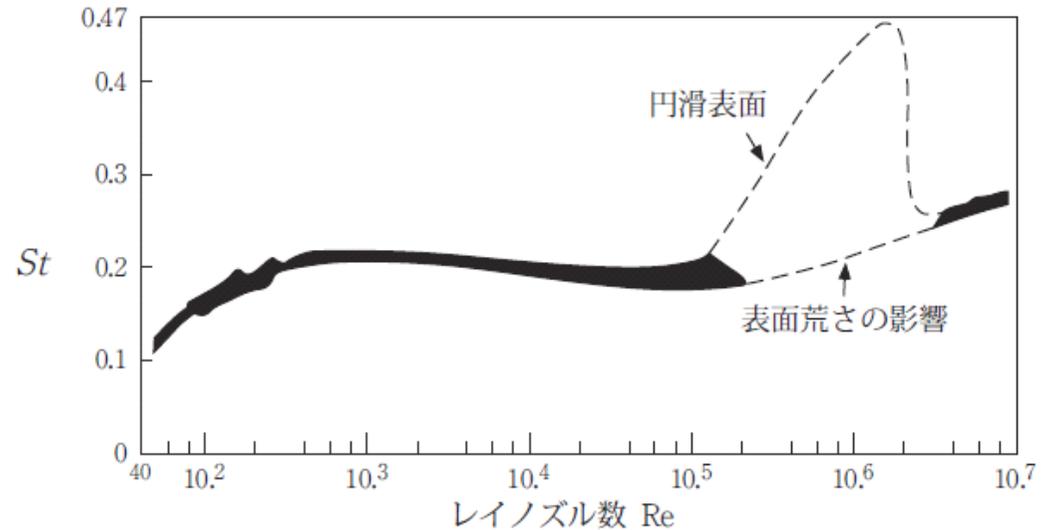


図2 レイノルズ数に対するストローハル数⁽⁵⁾

(5) R. D. Blevins: "Flow-induced vibration", Krieger publishing company (1990) .

$D=0.05$
 $\nu=0.001$
 $U=4$
 $Re=200$

$St=0.2$
 $f_s=St \cdot U/D=16$



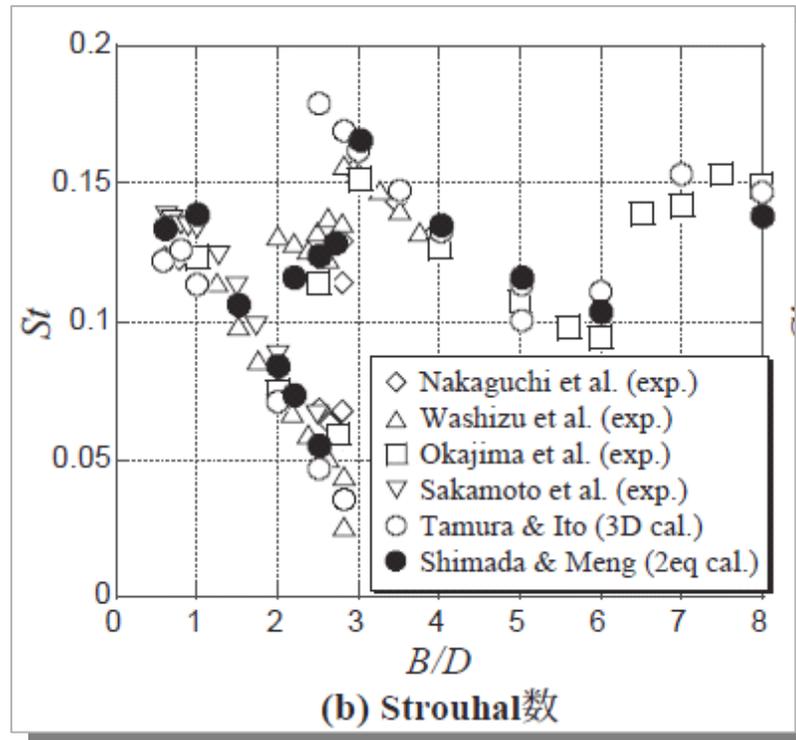
ストローハル数(角柱の場合)

<http://bit.ly/b86pJE>

http://ci.nii.ac.jp/els/110002399378.pdf?id=ART0002680678&type=pdf&lang=jp&host=cinii&order_no=&ppv_type=0&lang_sw=&no=1280810119&cp=

<http://bit.ly/bsNgzx>

<http://www.nagare.or.jp/download/noauth.html?d=22-1-t01.pdf&dir=36>



辺長比 B/D (B : 角柱の幅, D : 奥行き)

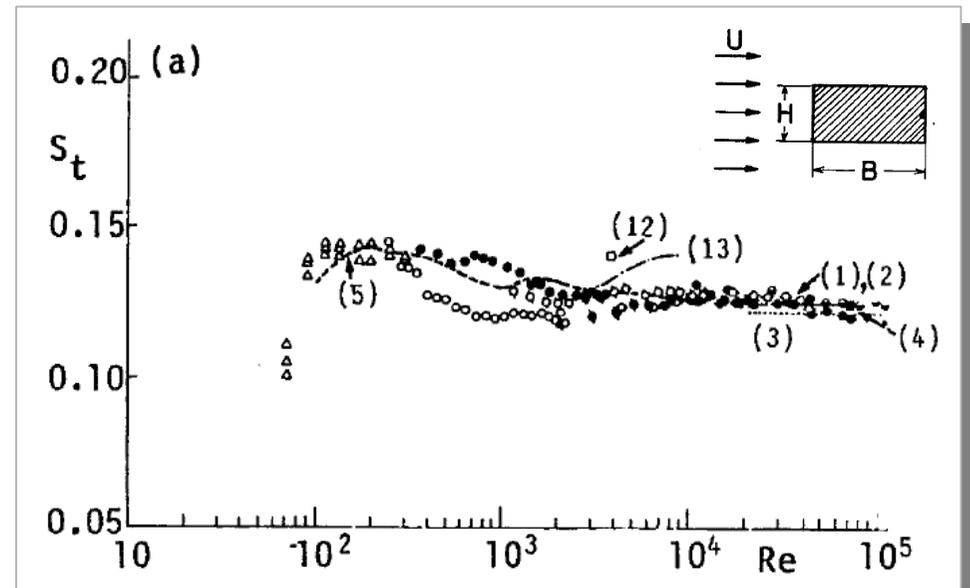


図 2 $B/H = 1.0$ 正方形断面柱の (a) S_t 数

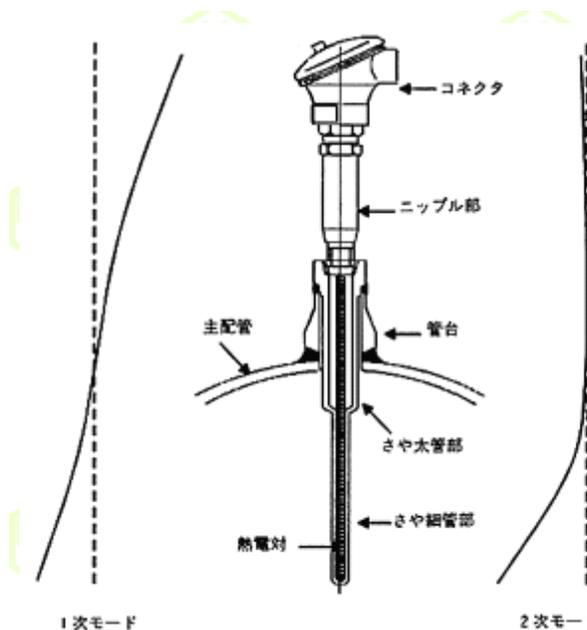
$D=0.05$
 $\nu=0.001$
 $U=4$
 $Re=200$

$St=0.13$
 $fs=St \cdot U/D=10.4$



「もんじゅ」事故と原因究明の現状・・・より

http://www.jaea.go.jp/04/monju/category05/mj_accirep/mj_accirep17.html



温度	1次固有振動数(Hz)		2次固有振動数(Hz)	
	流れ直角方向	流れ方向	流れ直角方向	流れ方向
200°C	163	173	257	257
325°C	160	170	251	251
485°C	157	164	241	241

表4-1 温度計の固有振動数

図4-2 温度計の固有振動モード(ナトリウム中、200度の例)

二次主冷却系の温度計は、主配管の横腹に設けられた管台に溶接され、温度計さやが配管内に約185mm突き出した構造となっている。このうち、さやの先端約150mmの部分は、直径が10mmと細くなっている(図4-2参照)。

http://www.jaea.go.jp/04/monju/category05/mj_accirep/mj_accirep18.html

		100%流量試験 (200°C等温)	100%流量試験 (325°C等温)	40%流量試験 (485°C)
Na流速	ν	5.2 m/s	5.2 m/s	2.2 m/s
Na密度	ρ	904 kg/m ³	874 kg/m ³	836 kg/m ³
レイノルズ数	Re	1.0×10^5	1.4×10^5	7.2×10^4
固有振動数 (流体 質量効果を考慮)	f	272Hz (257Hz)	265Hz (251Hz)	254Hz (241Hz)

表4-2 プラントの運転状態

http://www.jaea.go.jp/04/monju/category05/mj_accirep/mj_accirep19.html

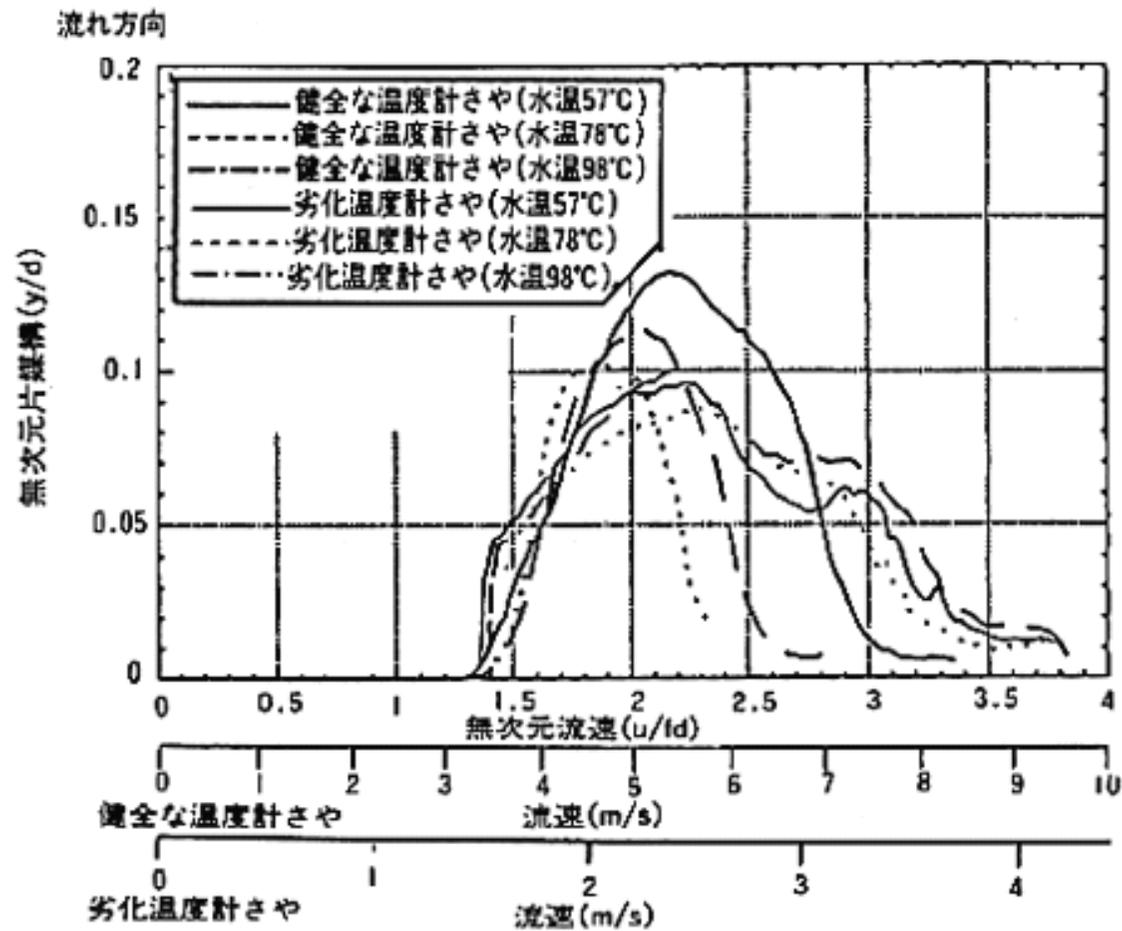
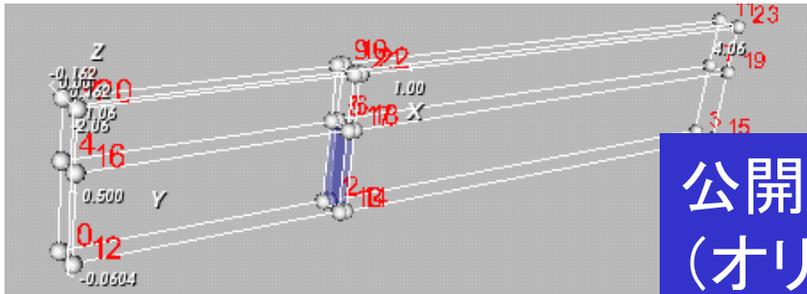


図4-9 温度計さや先端変位振幅と無次元流速の関係

FSI境界面定義方法の問題



公開ケース
(オリジナル)

```
patches
(
  patch consoleSolid
  (
    (3 7 6 2)
    (0 4 7 3)
    (2 6 5 1)
  )
)
```

DEXCS

```
patches
(
  patch consoleSolid
  (
    (0 4 7 3)
    (2 6 5 1)
    (3 7 6 2)
  )
)
```

autoPatch
⇒ createPatch

